

Double Crystal Monochromator Workshop
ESRF, Grenoble, 13 and 14 May 2014



| The European Synchrotron

Thermal, mechanical deformation and stability of Monochromator Crystals under high heat load

- **Cooling strategy**
 - Water or LN2, direct or indirect, crystal size and cooling scheme
- **Crystal material, properties**
 - Crystals, Silicon, doping, anisotropic elasticity, pure isotope
- **Thermal deformation**
 - Finite element analysis (FEA)
 - Measurement techniques
 - Comparison between measurements and simulations
 - Some extended FEA results
 - Power and power density, beam size, grazing angle, cooling coefficient, ...
 - Focusing effects
- **Initial deformation of the crystal**
 - Manufacturing, mounting, and cooling down to LN2 temperature
- **Stability and vibration**
 - Some measurement results

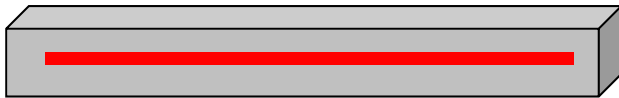
Cooling strategy: mirror and monochromator

Thermal deformation - comparison of mirror and monochromator

➤ For an incident beam at 30 m

- Power density $P_{a0}=200 \text{ W/mm}^2$
- Beam size $H \times V=2 \times 1 \text{ mm}^2$

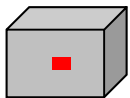
White beam mirror



typical length: 1000 mm

- typical **grazing angle**: 2 mrad
- footprint: 500 ~ 1000 mm
- Power density $P_a \sim 1 \text{ W/mm}^2$
- **Topside cooling by water**

Monochromator crystal

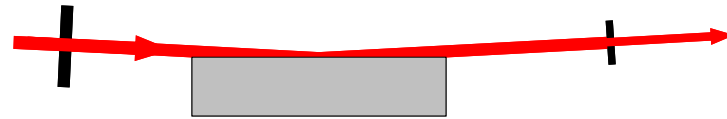
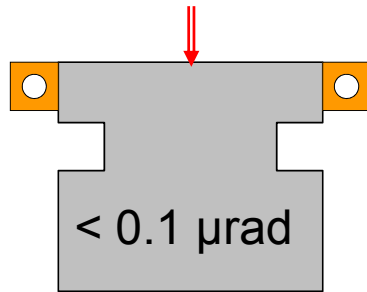


typical length: 100 mm

- typical **Bragg angle**: 12° (209 mrad)
- footprint $\sim 1\%$ as long as for mirror
- Power density $P_a \sim 50 \text{ W/mm}^2$
- **Cooling scheme ?**

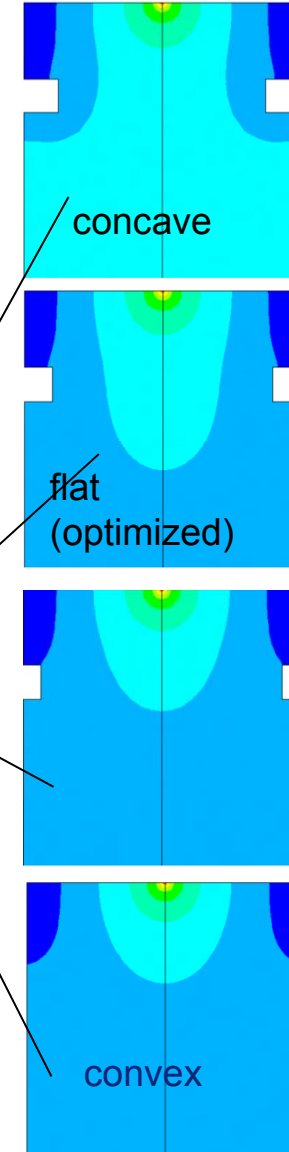
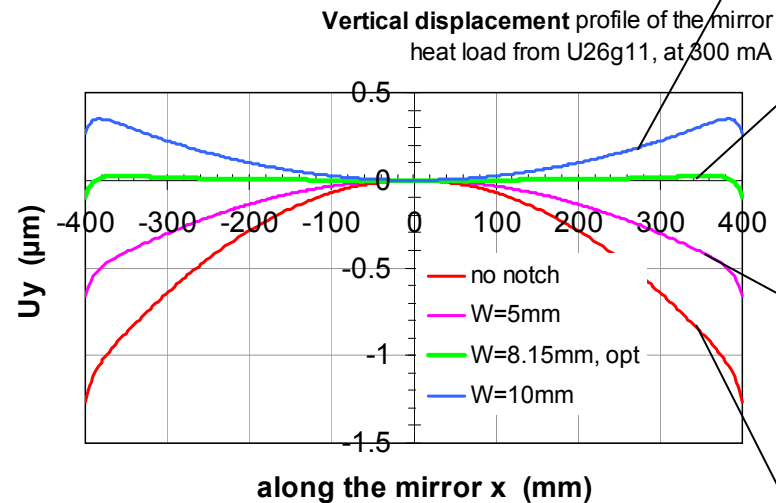
Cooling strategy: white beam mirror

Solution to minimize thermal deformation for white beam mirror
(smart shape + full illumination):



ESRF UPBL06 (ID16)

- Mirror size: 800x80x80
- Grazing angle 3.1 mrad
- 2~3 coatings
- Heat load: **834 W**
Gaussian distribution
 $\sigma = 3.86 \text{ mm}$



Zhang L. et al., *J. Phys.: Conf. Ser.* **425** (2013) 052029
doi:10.1088/1742-6596/425/5/052029

Cooling strategy: mirror and monochromator

Can monochromator crystal be cooled as mirror (full illumination) ?

White beam mirror

$$P_a = 1 \text{ W/mm}^2$$

$$W_{bm} = 2 \text{ mm}, H_{cool} = 10 \text{ mm}$$

$$h_{cv-eq} = 5000 \text{ W/m}^2/\text{°C}$$

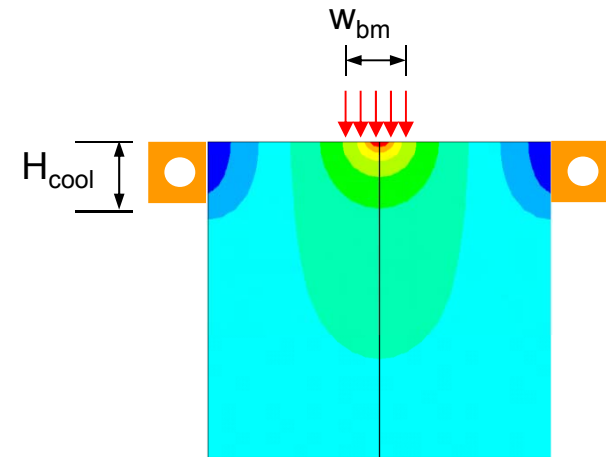
$$\overline{\Delta T}_{min} = \overline{T}_{min} - T_f = \frac{P_a}{h_{cv-eq}} \frac{W_{bm}}{2H_{cool}}$$

$$\overline{\Delta T}_{min} = 20\text{°C}$$

For Monochromator crystal

$$P_a \sim 50 \text{ W/mm}^2$$

$$\rightarrow \overline{\Delta T}_{min} = 1000\text{°C} \quad !!!$$



Impossible to cool the Monochromator as the mirror

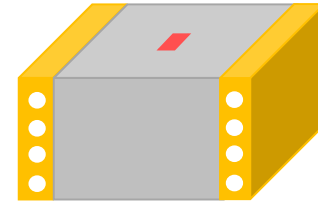
Cooling strategy for monochromator crystal

Full side cooling (to increase cooling surface area)

- $P_a \sim 50 \text{ W/mm}^2$
- $W_{bm} = 2 \text{ mm}$, $L_{bm} = 5 \text{ mm}$,
- $H_{cool} = t_{mono} = 50 \text{ mm}$
- $L_{cool} = L_{mono} = 100 \text{ mm} \gg L_{bm}$
- $h_{cv-eq} = 5000 \text{ W/m}^2/\text{°C}$

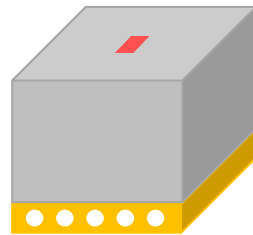
$$\overline{\Delta T}_{min} = \frac{P_a * W_{bm} * L_{bm}}{h_{cv-eq} * 2 * H_{cool} * L_{cool}}$$

$$\overline{\Delta T}_{min} = 10^\circ\text{C}$$



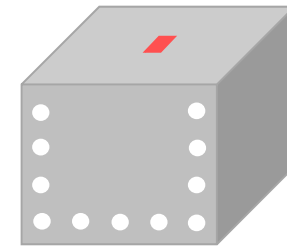
Cooling of monochromator needs crystal significantly longer than beam footprint

Bottom cooling



- Cooling surface area reduced

Direct cooling



- No thermal contact resistant
- Sealing difficulty
- Sealing induced stress and deformation

Crystal material, Properties of Si

Materials for Monochromator crystal

➤ Silicon:

- Perfect crystal
- Large size $\Phi 100 \times 500$
- Very reasonable price
(900€/kg, 9000€ for $\Phi 100 \times 500$)
- Interesting properties at low temperature

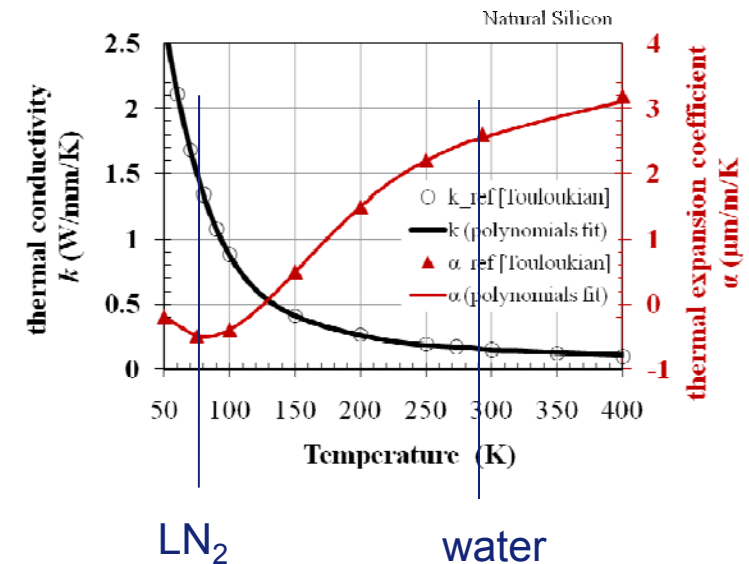
➤ Germanium

- Less perfect
- Medium size $\Phi 100 \times 75$
- 4 ~ 40 times more expensive than Si

➤ HPHT Synthetic Diamond

- Imperfect
- Small size $10 \times 10 \times 1$
- Expensive

$$\text{Thermal slope : } \Delta\theta \propto \frac{\alpha}{k}$$



$$\frac{\alpha}{k}(T = 295 K) \Big/ \frac{\alpha}{k}(T = 77 K) \approx 100$$

Anisotropic elasticity of Si

- Silicon: cubic diamond crystal structure
- Stiffness coefficient matrix
 - 3 three independent elastic coefficients for Si (100)
 - Can be calculated for any crystallographic orientation
 - Analytically
 - By codes (MatLab, Python)

$$C_{100} = \begin{bmatrix} c_{11} & c_{12} & c_{12} & & & \\ c_{12} & c_{11} & c_{12} & & & \\ c_{12} & c_{12} & c_{11} & & & \\ & & & c_{44} & & \\ & & & & c_{44} & \\ & & & & & c_{44} \end{bmatrix}$$

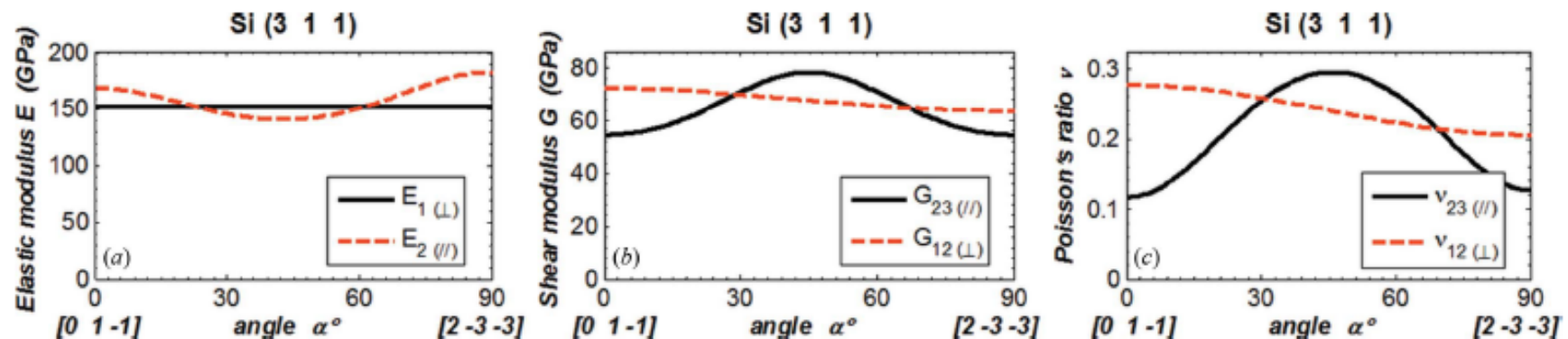


Figure 6
 (a) Elastic modulus in the directions \mathbf{e}'_1 and \mathbf{e}'_2 . (b) Shear modulus and (c) Poisson's ratio in the directions 12 and 23 for silicon (311). The vector \mathbf{e}'_1 is fixed in the normal direction [311], and the vectors \mathbf{e}'_2 and \mathbf{e}'_3 are in the crystal plane (311). The angle α is between the vectors \mathbf{e}'_2 and $[0\ 1\ -1]/2^{1/2}$ in the crystal plane: $\mathbf{e}'_2(\alpha=0^\circ) = [0\ 1\ -1]/2^{1/2}$, $\mathbf{e}'_2(\alpha=90^\circ) = [2\ -3\ -3]/(22)^{1/2}$.

- Important for bent silicon crystal
- For thermal deformation ?

L. Zhang et al., J. Synchrotron Rad. (2014). 21, 507–517

Anisotropic elasticity of Si

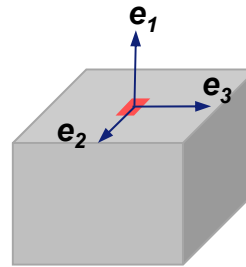
➤ Thermal deformation

- Depends on the Poisson's ratio:

$$\Delta \theta \propto (1 + \nu) \frac{\alpha}{k}$$

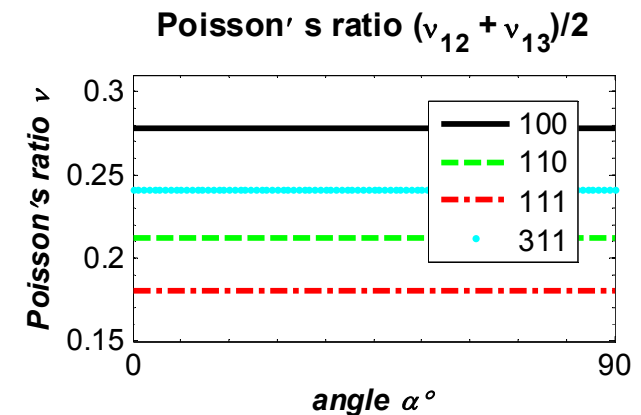
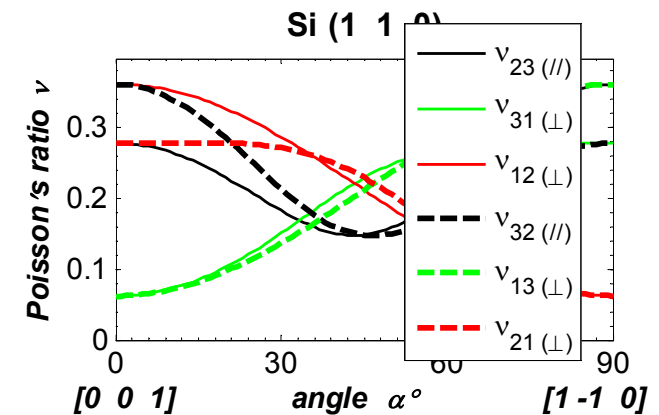
- Poisson's ratio depends on the crystal orientation
- Thermal slope error

$$\Delta \theta = \frac{\partial u_1}{\partial x_2} \propto (\nu_{12} + \nu_{13})/2$$



- But the average $\nu_{av} = (\nu_{12} + \nu_{13})/2$ is constant

➤ Thermal deformation with anisotropic elasticity of silicon → Simulation with isotropic and constant elasticity (ν_{av})



L. Zhang et al., *J. Synchrotron Rad.* (2014). **21**, 507–517

Si related Crystal material: Germanium doped silicon

➤ Germanium doped silicon $\text{Si}_{100-x}\text{-Ge}_x$ ($x \leq 2\%$)

- Ge doping decreases dislocation mobility, and modifies dislocation nodes in Si crystalline lattice

→ Increasing semi-conducting device efficiency: material strength, current carrier mobility

- Application to DCM: $\text{Si}_{100-x}\text{-Ge}_x$ for 1st crystal (LN_2), Si for 2nd crystal (water)

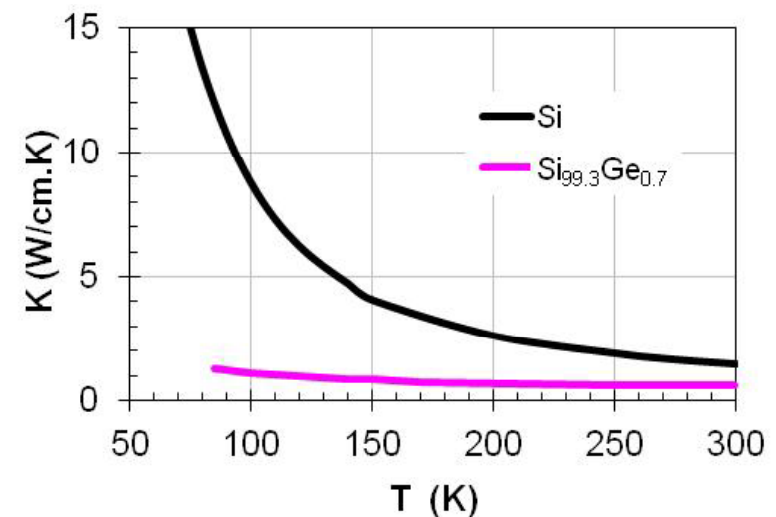
– Vegard's law: $\frac{\Delta d}{d_{\text{Si}}} = \mu x$
($\mu = 4.18 \times 10^{-4}$)

– Concentration $x \sim 0.7\%$

- Ge doping reduces dramatically the thermal conductivity of Si especially at LN2 temperature

→ Therefore the application of Si-Ge crystals to cryogenic cooling cannot be recommended

A. Souvorov and A. Snigirev, Rev. Sci. Instrum. 68, 1997



A. Freund, J.A. Gillet & L. Zhang, Proc. SPIE 3448, (1998); doi:10.1117/12.332526

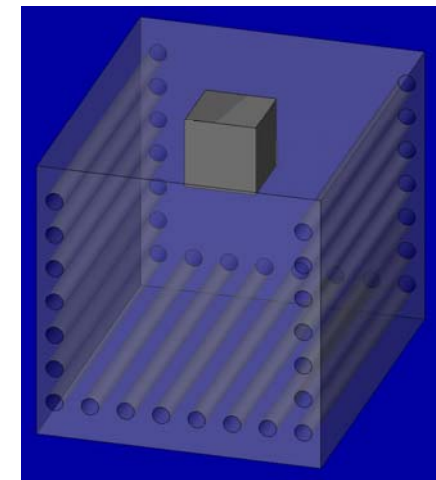
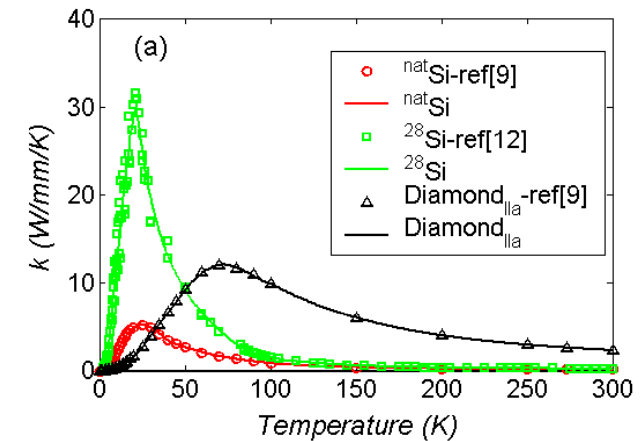
Si related Crystal material: pure isotope silicon

➤ Three stable isotopes in natural silicon:

- Silicon-28 : 92%
- Silicon-29 : 4.7%
- Silicon-30 : 3.3%

Single-isotope silicon-28 crystal (99.9%)

- Very high thermal conductivity ($k = 30\,000\text{ W m}^{-1}\text{ K}^{-1}$ at 20 K, 6 times higher than natural Si)
- Available, used in semiconductor industry
- Small size, very expensive
- Technology challenge for effective cooling
 - Huge size and high cost of cooling system for 500 W cooling power

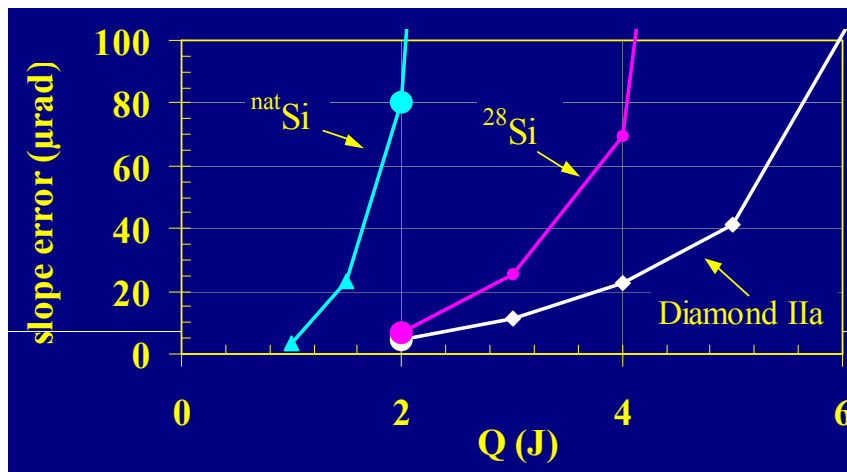
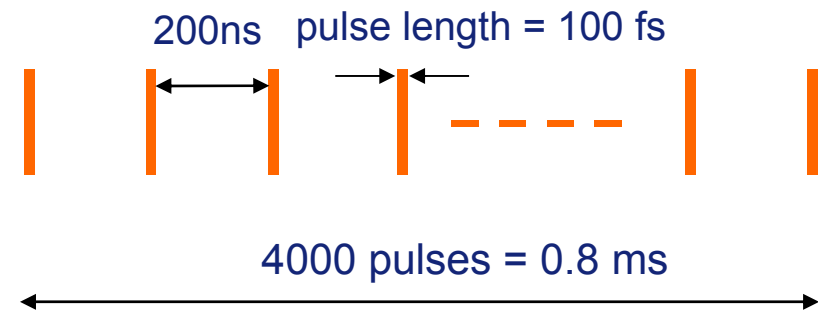
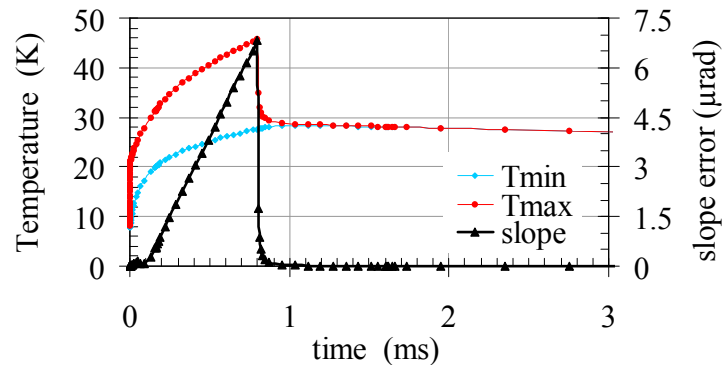


L. Zhang et al., AIP Conference Proceedings, 705, pp.639-642 (2003)

natSi, ²⁸Si and Diamond for very high heat-load monochromator

Macro-pulse train effects (f=10Hz)

- LN2 cooled diamond crystal (**20mm x 20mm x 20mm**)
- LHe cooled single-isotope silicon-28 crystal (**20mm x 20mm x 20mm**)
- LHe cooled natural silicon crystal (**120mm x 60mm x 60mm**)



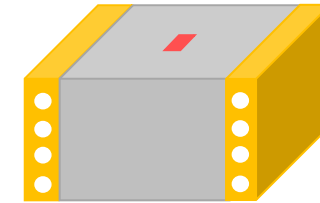
**Time-structure proposal
of TESLA X-FEL
(repetition rate 10 Hz)**

L. Zhang et al., AIP Conference Proceedings, **705**, pp.639-642 (2003)

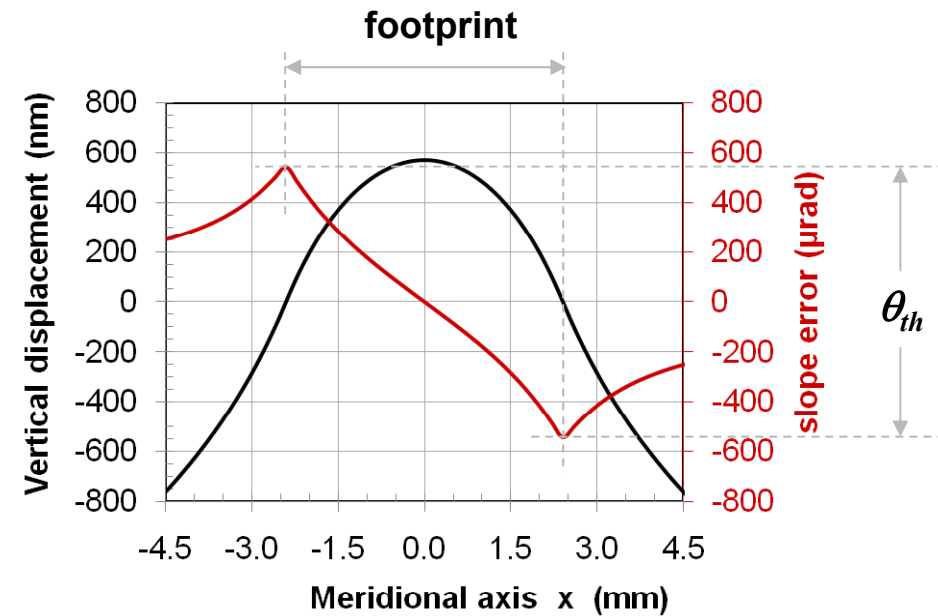
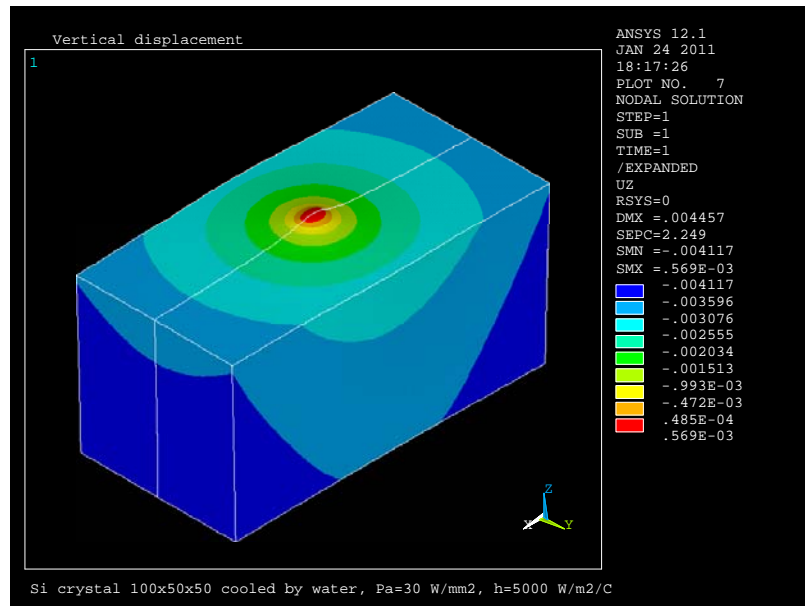
Thermal deformation of the monochromator crystal

For monochromator crystal

- 3D temperature and deformation
- Non-linear material properties (k , α)
- Finite Element Analysis (FEA) for the modeling



Example of water cooling

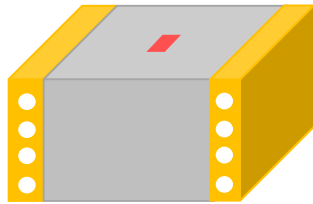


Thermal deformation : side cooling versus bottom cooling

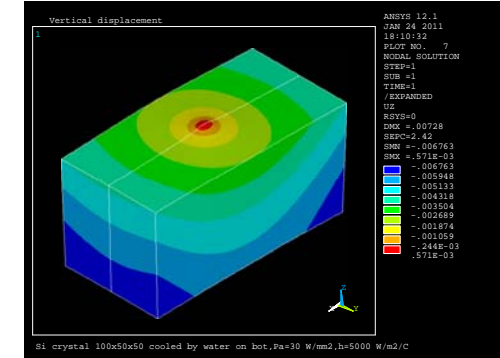
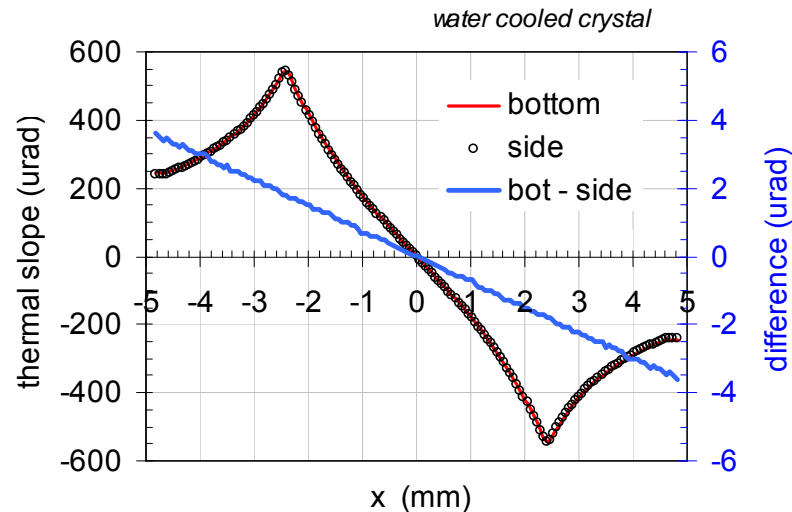
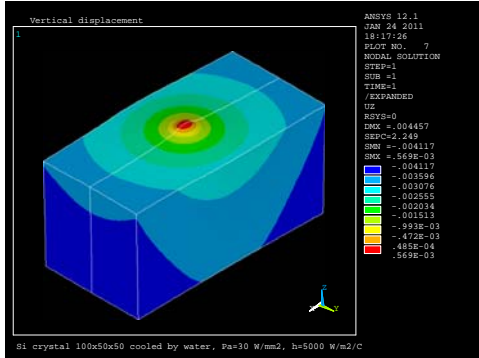
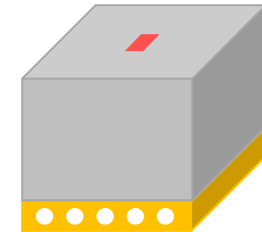
Side cooling

(by water)

bottom cooling



- Similar temperature distribution but low temperature with side cooling
- Very comparable thermal deformation: 0.7% lower thermal deformation with side cooling
→ Thermal bump deformation predominant !



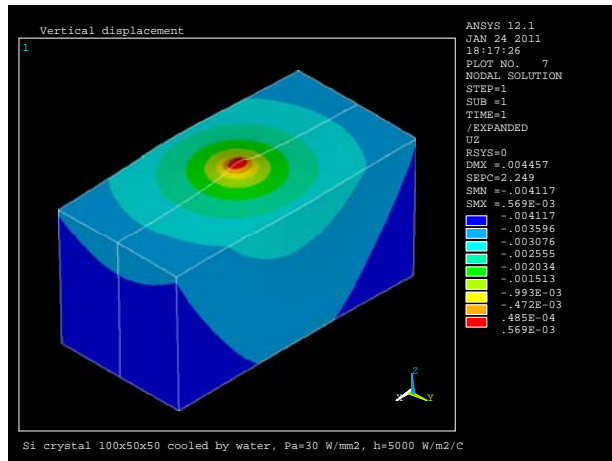
How to reduce this huge thermal slope error $\theta_{th} = 1085 \mu\text{rad}$?

Thermal deformation : water cooling versus LN2 cooling

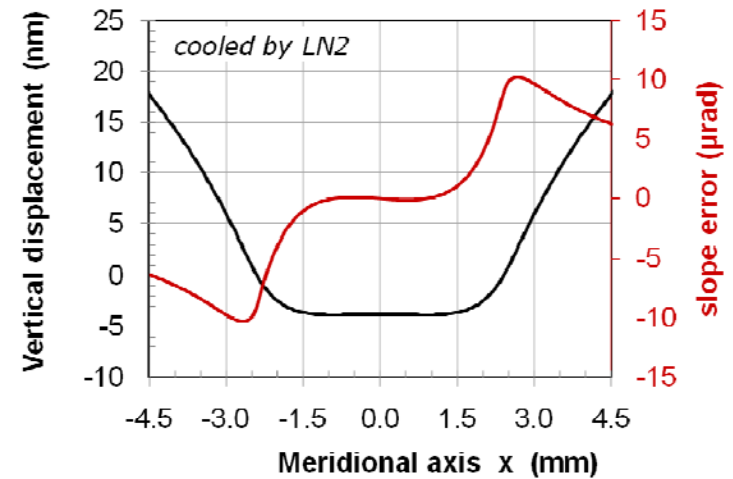
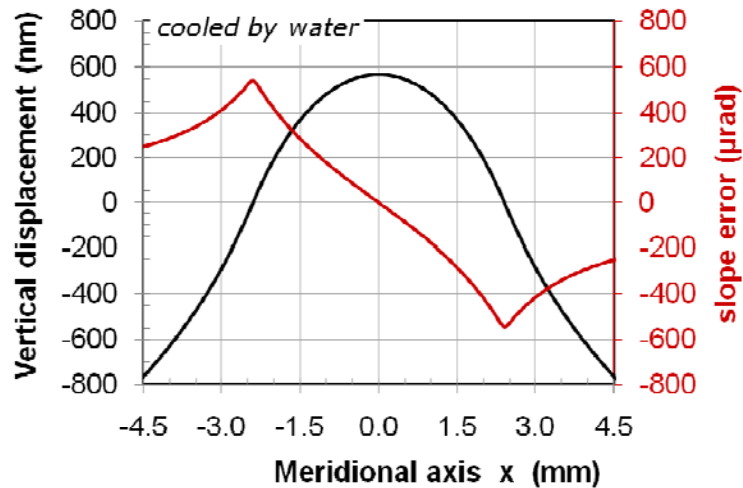
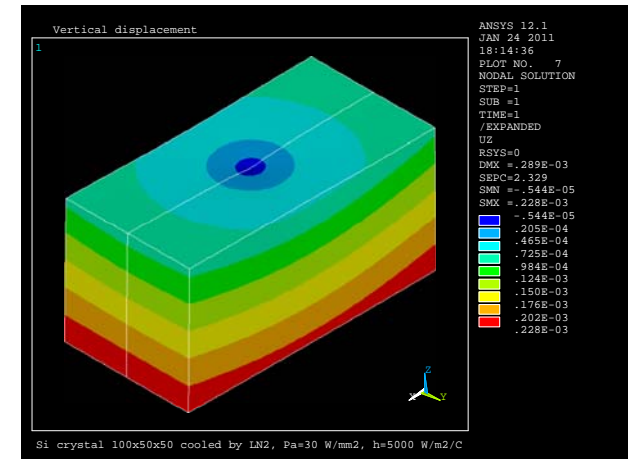
Water cooling

vs

LN2 (Liquid Nitrogen) cooling



For LN2 cooling
 $\theta_{th} = 18 \mu\text{rad}$
 $\theta_{RMS} = 3 \mu\text{rad}$
 Reduced by a
 factor of 61 for θ_{th}
 (96 for θ_{RMS})

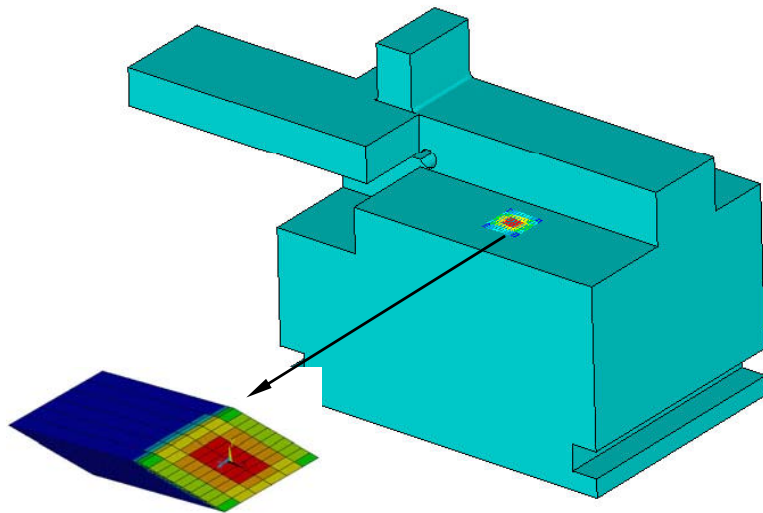
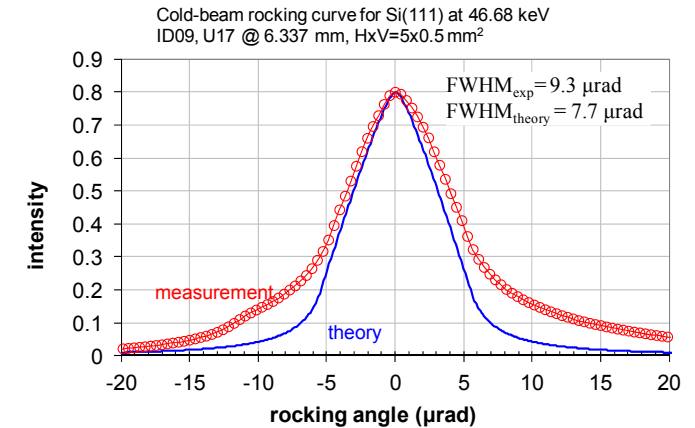


Thermal deformation: indirect measurement technique

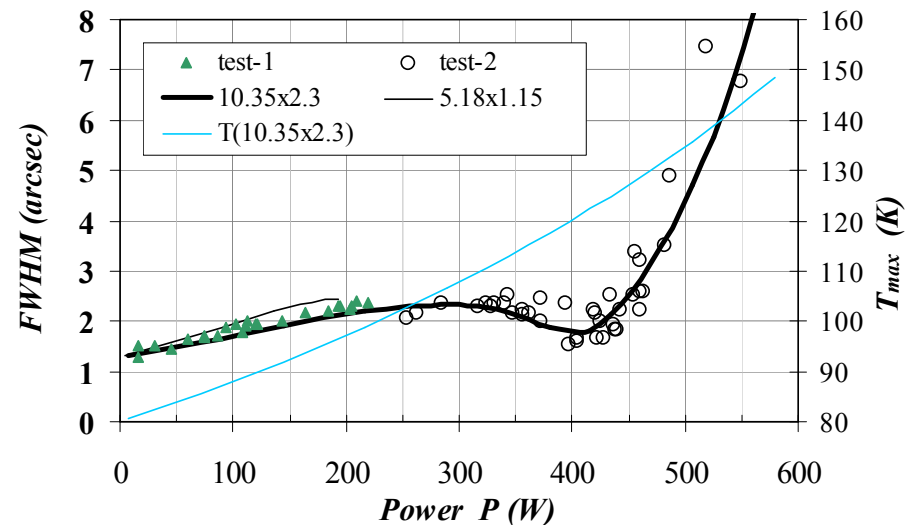
- Thermal deformation → Rocking-curve broadening
- Rocking-curve width:

$$FWHM_c = \sqrt{(\theta_{th} + \theta_0)^2 + FWHM_{intr}^2}$$

- Comparison of **test and FEA results** for ID09 LN2 cooled Si crystal (Channel-Cut Monochromator)



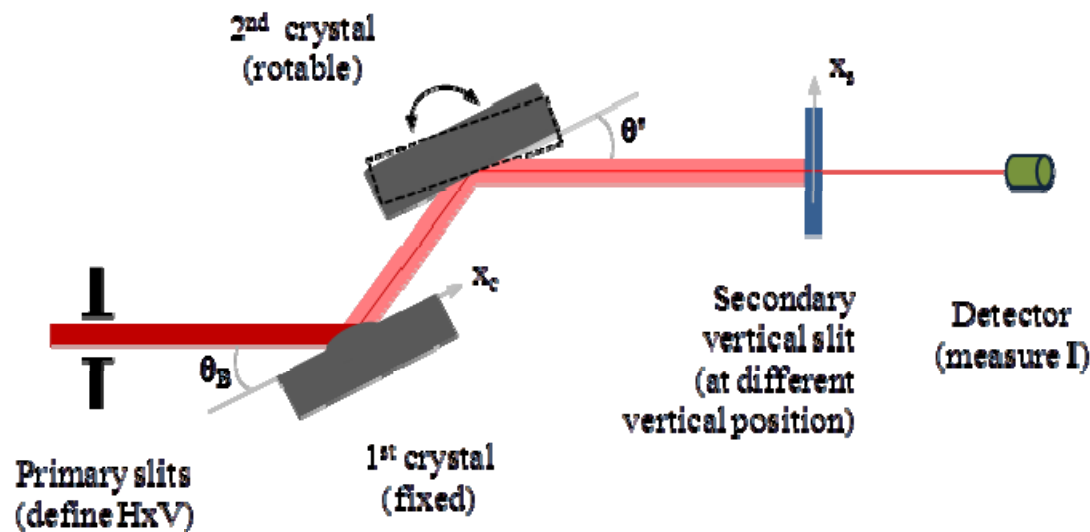
Zhang L. et al., JSR (2003). 10, 313-319



Thermal deformation: direct measurement technique

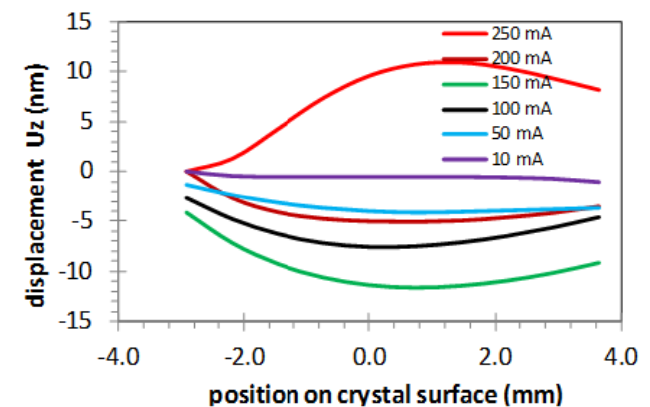
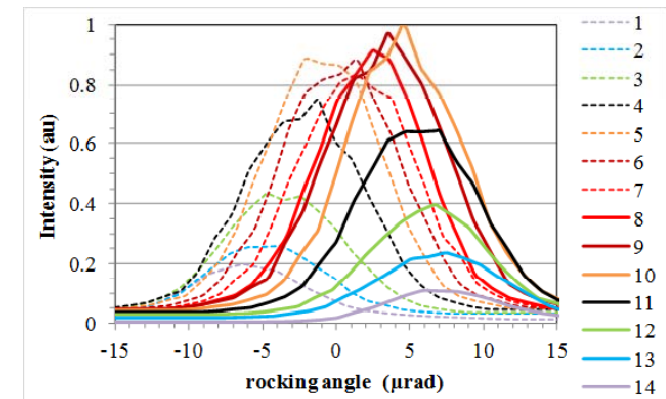
Applied to ID06, ID18 and ID26 LN2 cooled Si crystal

- Multiple angular scans across the Bragg peak (rocking curve) at various vertical positions of a narrow-gap slit downstream from the monochromator



- Thermal slope: $\Delta\theta_{th} = \theta'_{peak} - \theta_B$

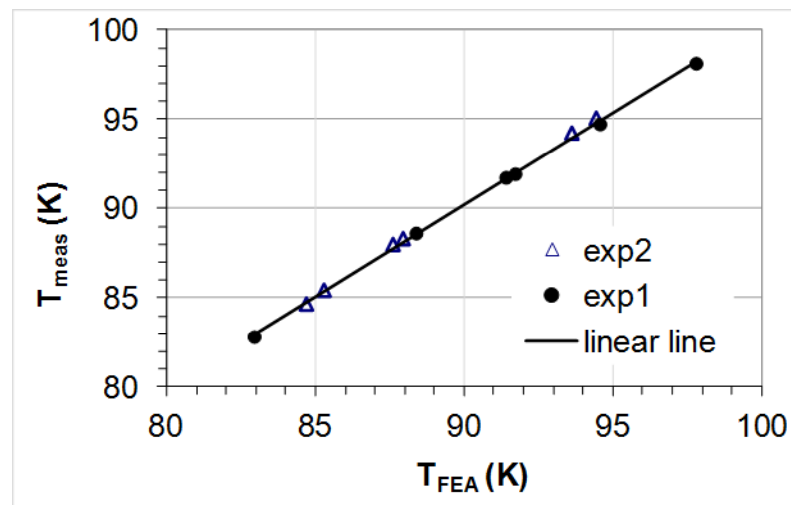
Zhang L. et al., *J. Synchrotron Rad.* (2013). **20**, 567–580



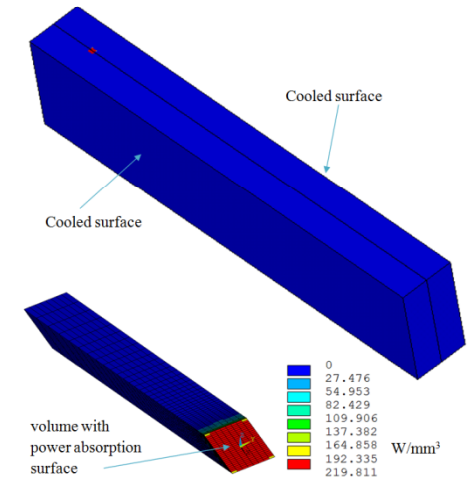
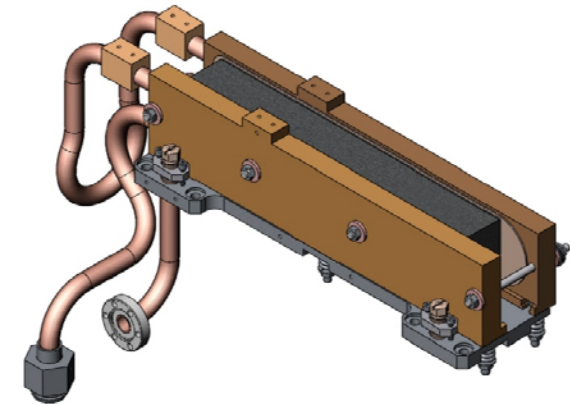
Thermal deformation: direct measurement technique

ID06 LN2 cooled Si crystal (DCM)

- **FEA** (Gaussian distribution and volume power absorption, h_{cv} determined by fitting temperature in only one case)
- **For various other cases (I, HxV)**



- **Excellent agreement in Temperature**



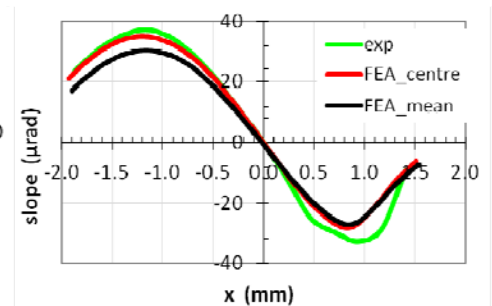
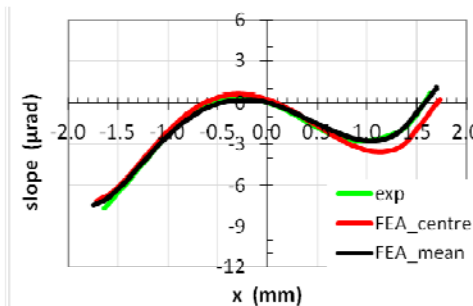
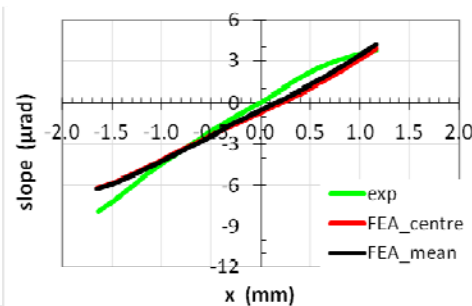
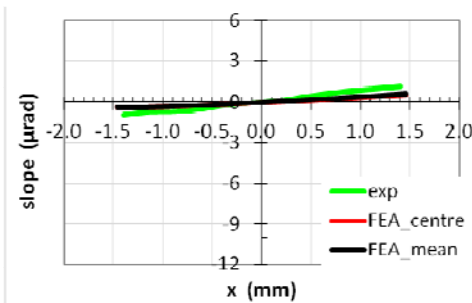
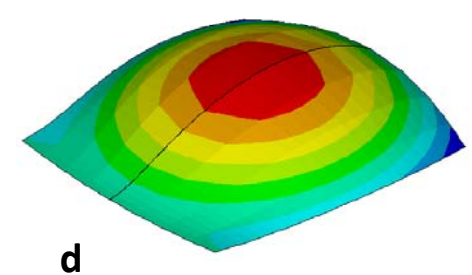
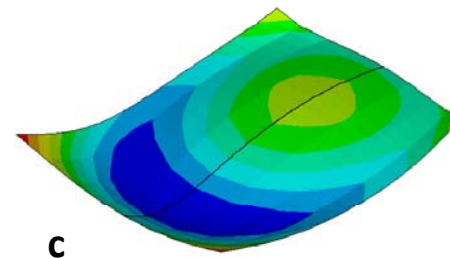
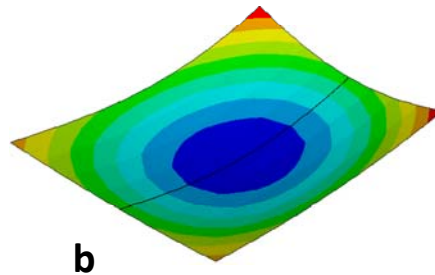
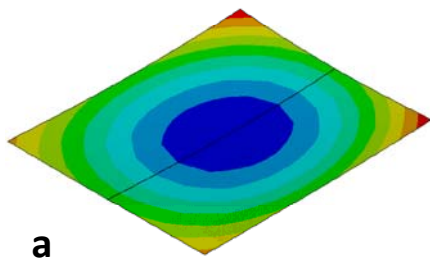
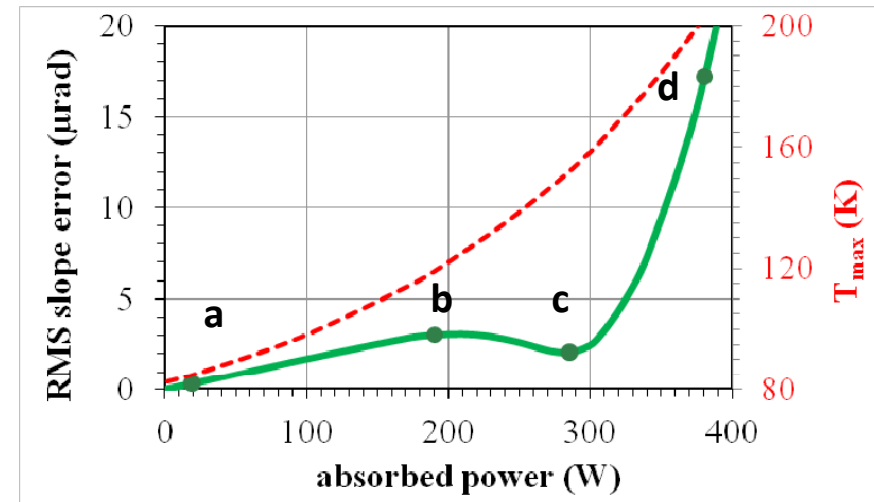
Zhang L. et al., *J. Synchrotron Rad.* (2013). **20**, 567–580

Thermal deformation: direct measurement technique

ID06 LN2 cooled Si crystal (DCM)

- (1st) Direct comparison of test results and FEA results

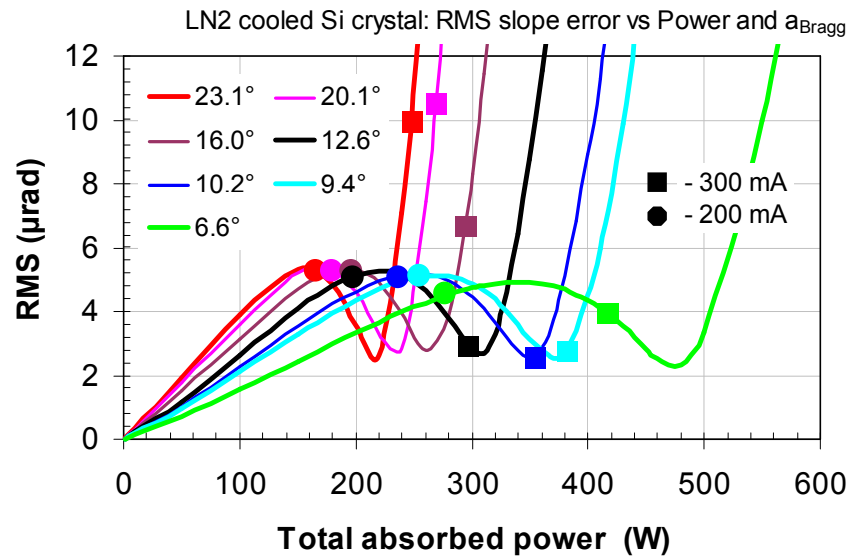
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Thermals slope versus Power and Bragg angle

For UPBL06 LN2 cooled monochromator crystal

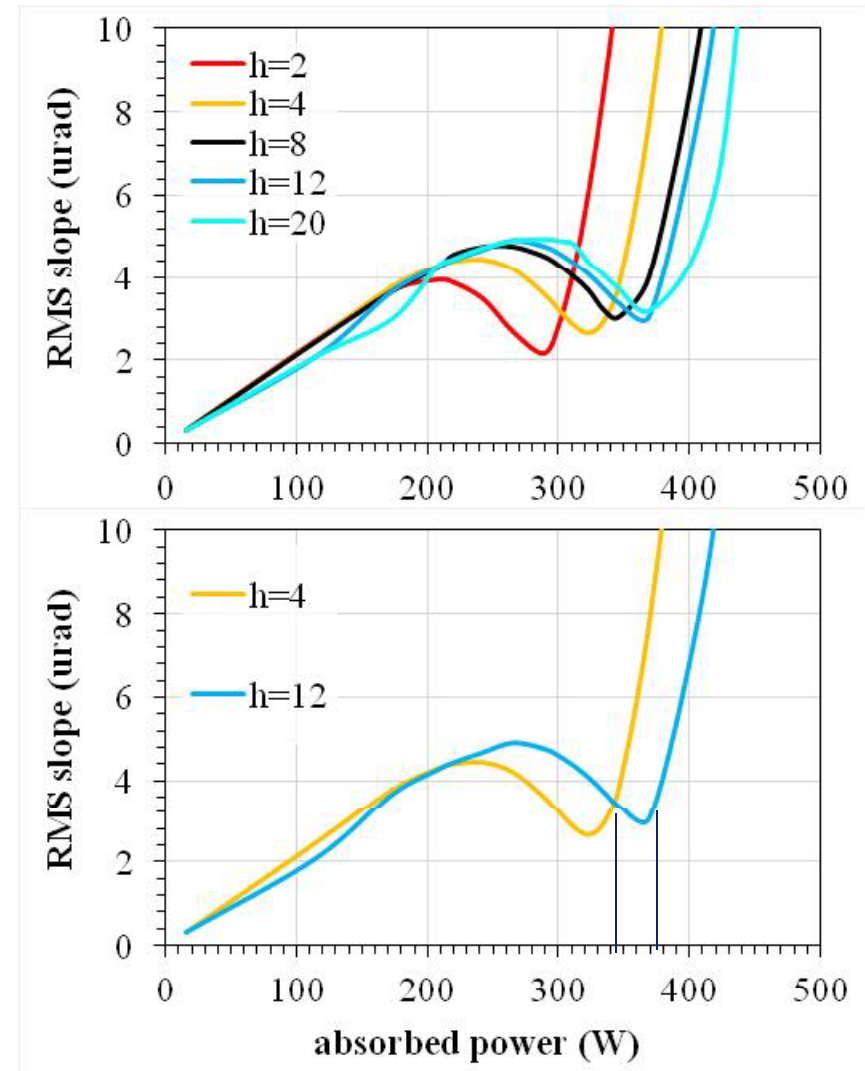
- Si 111, 5~20 keV
 - $L \times W \times T = 100 \times 60 \times 80 \text{ mm}^3$
 - White beam mirror used to reduce the heat load
 - Beam size $H \times V = 2 \times 1 \text{ mm}^2$
 - Indirect cooling $h_{cv} = 4000 \text{ W/m}^2/\text{K}$
- **Bragg angle: 5.6 ~ 23.1°**



Thermals slope versus Power and Cooling coefficient

For UPBL06 LN2 cooled monochromator crystal

- Bragg angle: 10.4,
- **Effective cooling coefficients:**
 - h_{cv} (W/m²/K)
 - 2000 poor contact
 - 4000 correct contact
 - 8000 excellent contact
 - 12000 direct cooling
 - 20000 enhanced direct cooling
- **Indirect cooling vs direct cooling**
 - P_{limit} (Indirect cooling) = 345 W
 - P_{limit} (direct cooling) = 375 W
 - Direct cooling is interesting for the heat load in a small range (345, 375) W
- **Good contact between cooling block and silicon crystal is needed**



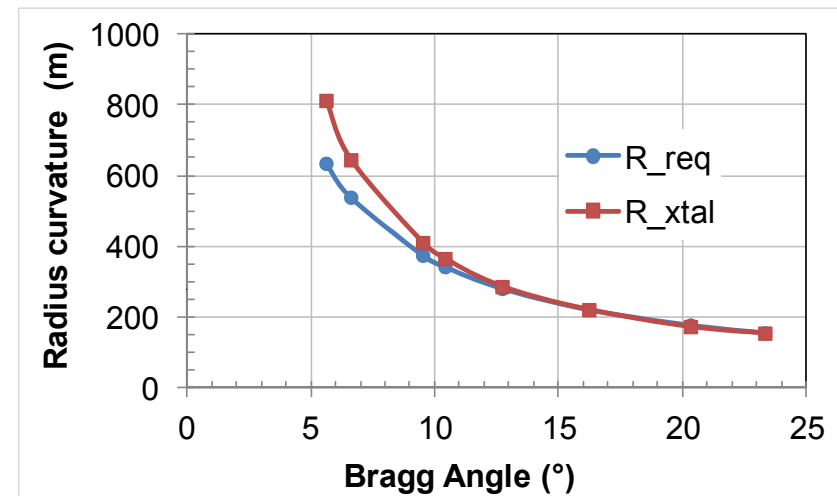
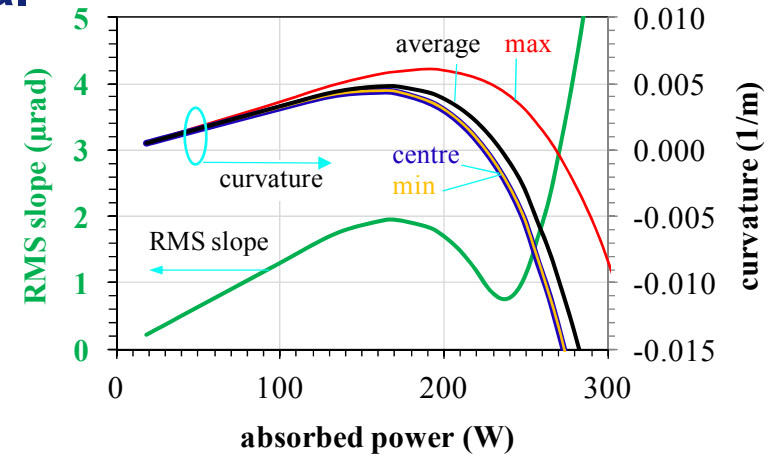
Focusing effects of the monochromator crystal

For UPBL06 (ID20) LN2 cooled Si crystal

- Silicon crystal at $p=31$ m
- Beam size: $H \times V = (1.8 \sim 2.8) \times 0.8$ mm² at 27m
- Bragg angle: $5.6 \sim 23.1^\circ$
- Variable absorbed power
- Gaussian power distribution
- Thermal deformed crystal shape calculated by FEA: radius R_{xtal}
- Required radius R_{req} for beam collimation ($q \rightarrow \infty$):

$$R_{req} = \frac{2p}{\sin(\theta_{Bragg})}$$

- Beam collimation is achievable by using only monochromator and by monitoring primary slits opening



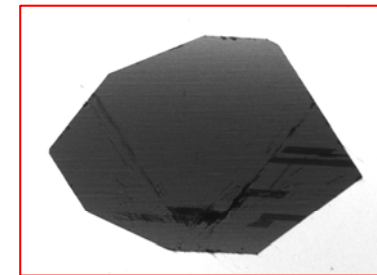
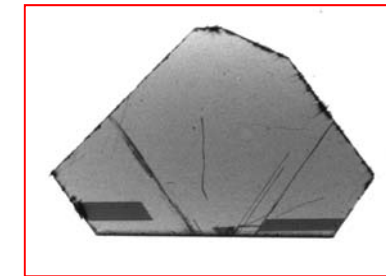
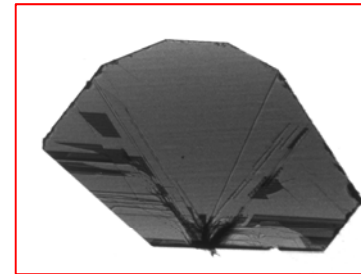
Zhang L. et al., *J. Phys.: Conf. Ser.* **425** (2013) 052008
 doi:10.1088/1742-6596/425/5/052008

Diamond crystal monochromator

ID28 SS Diamond monochromator, U32g15

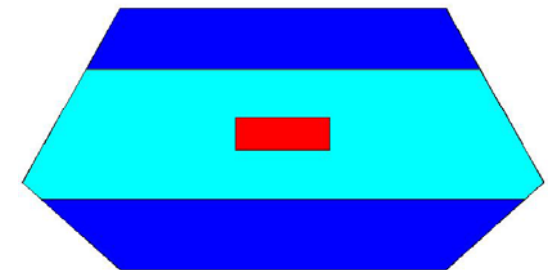
➤ Parameters

- $e_{ph} > 12$ keV
- At 28 m from the sources
- Incident angle: 26 degrees
- Beam size: $H \times V = 1.3 \times 0.5$ mm²
- Water cooling (indirect)
- Diamond crystal size: $4 \times 8 \times 0.3$ mm³
- Darwin width at 311: **2 μ rad**



➤ Recommendations for $\Delta\theta < 0.4$ μ rad, $T_{max} < T_{melt}(In)$

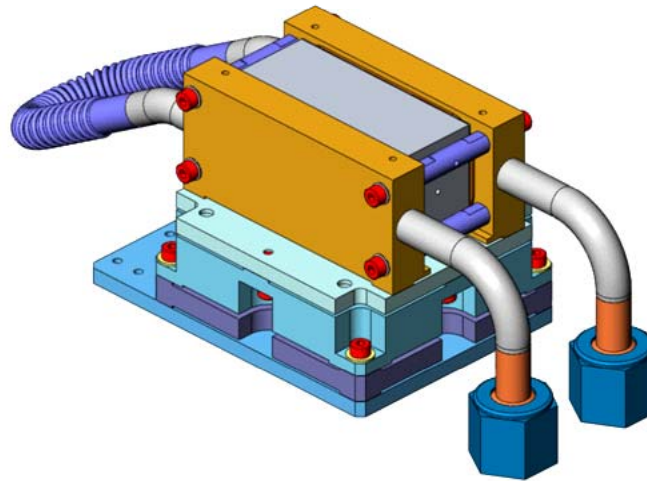
- Beam size reduced to just cope with centre cone $H \times V = 1.3 \times 0.5$ mm²
- 0.8-mm (0.3+0.5) thick diamond attenuator in front
- Maximize contact surface area
- Thermal Contact Resistance (TCR) > 7000 W/m²/°C (Indium foil to be used)



Initial deformation of the crystal

Heat load tests of the LN2 cooled monochromator → initial deformation of the crystal due to

- Monochromator components **manufacturing**, crystal **cutting**, **mounting** and **assembling**, cooling down from T_{room} to T_{LN2}



* Chumakov A.I. *et al.*, J. Synchrotron Rad. (2014). **21**, 315–324



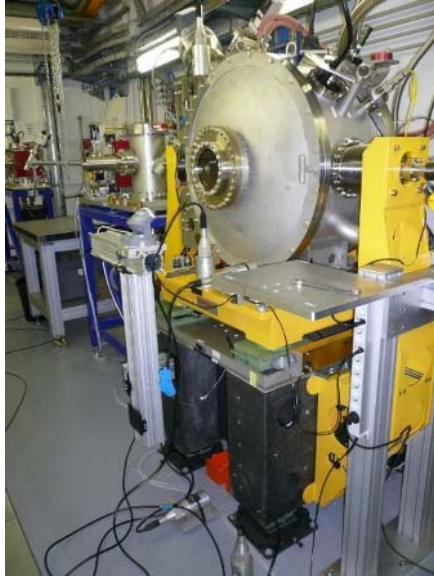
ID06 DCM
 $\theta_0 =$ **0.45**
 $h_{\text{eff}} =$ 2900

ID18 DCM
 $\theta_0 =$ **1.0***
 $h_{\text{eff}} =$ 3500

ID09 CCM
 $\theta_0 =$ **5.5** μrad
 $h_{\text{eff}} =$ 1400 $\text{W/m}^2/\text{K}$

Stability and vibration of the monochromator

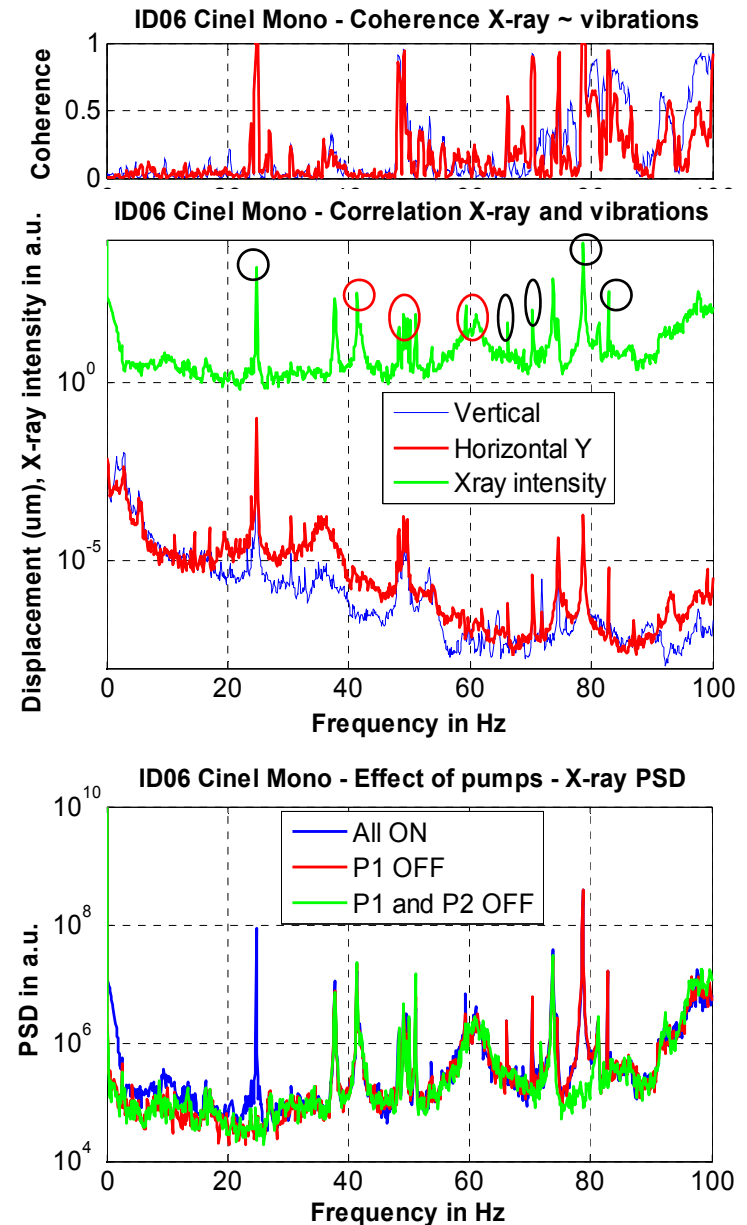
Example of ID06 Cinel mono



Correlation between X-ray intensity fluctuation and mechanical vibration

- $F=24.8, 66.2, 70.3, 78.7, 82.8$ Hz
- 1st peak due to vacuum pump 1, other 4 peaks due to pump 2

Remaining peaks **0** probably due to mechanics → room for improvement



DCM vibration tests in ID06 (2008)

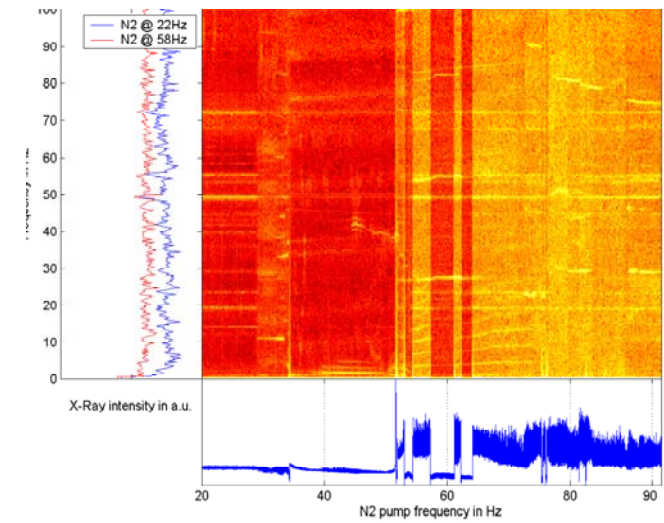
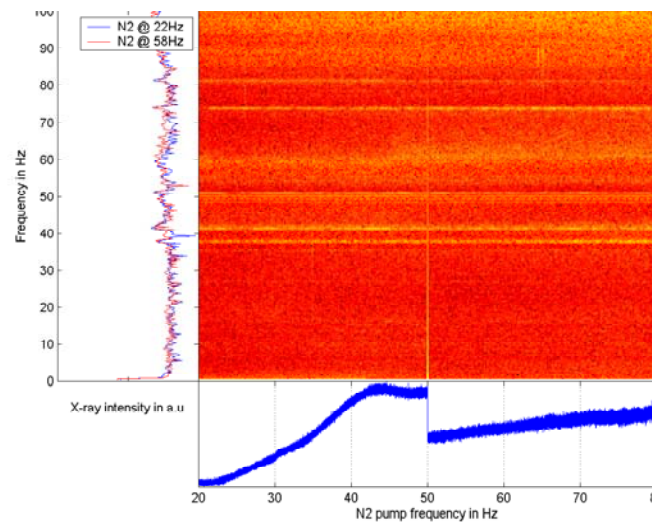
Cinel



Oxford



Beam intensity fluctuation ΔI versus the cryo-cooler pump frequency

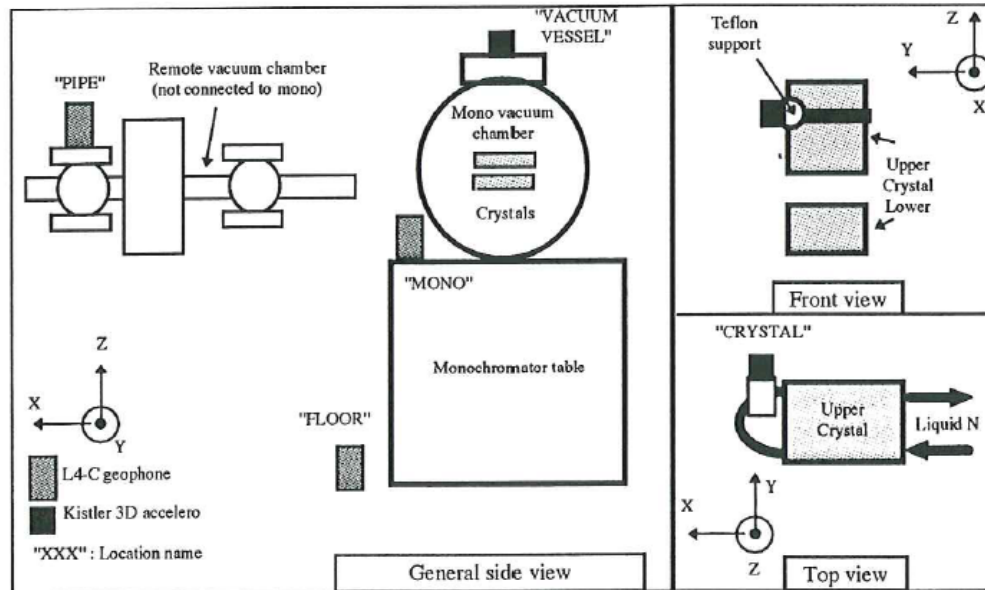


- For Oxford mono, high ΔI for $f_{\text{pump}} > 45$ Hz is due to the cooling scheme and mechanical structure of the mono

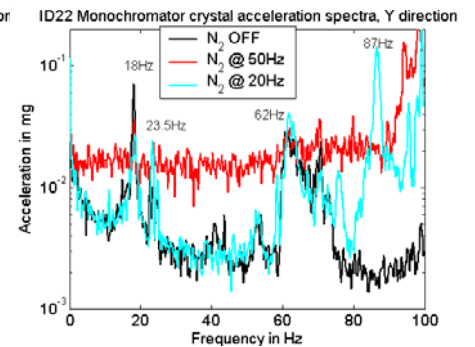
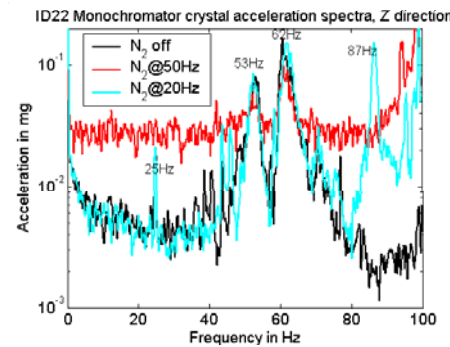
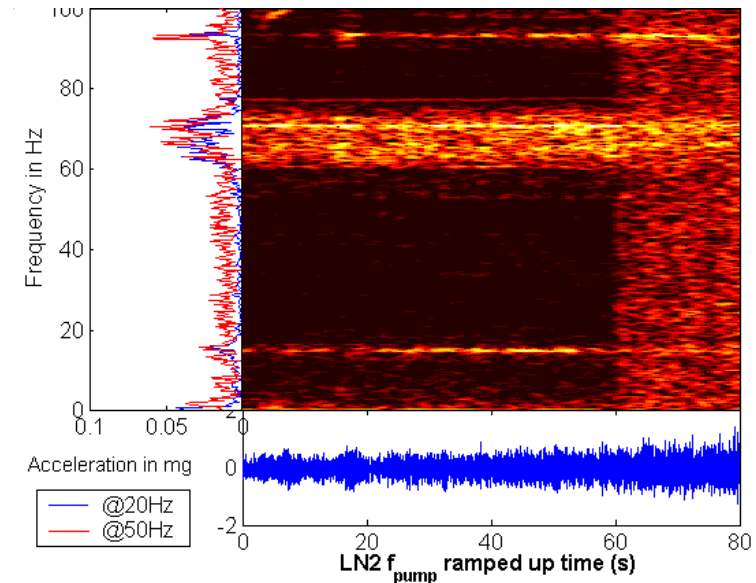
DCM vibration tests in ID22 (1997)

1997, ID22, 3D accelerometer
1st direct in-situ measurement
on the LN2 cooled crystal

SET-UP

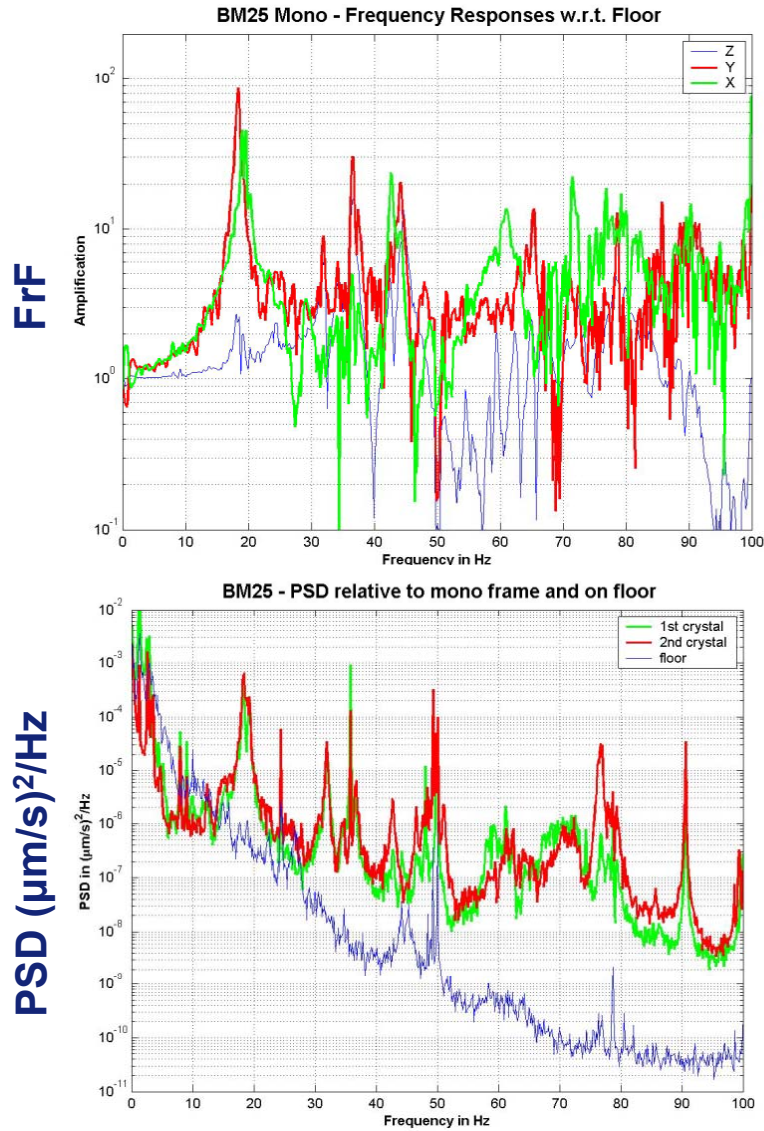


HP: 100Hz, 800 lines, teap: 80sec.
Matlab: high pass 0.5Hz, twin/ovlp: 8/0sec.
Spectrogram: twin/ovlp: 2/1sec.

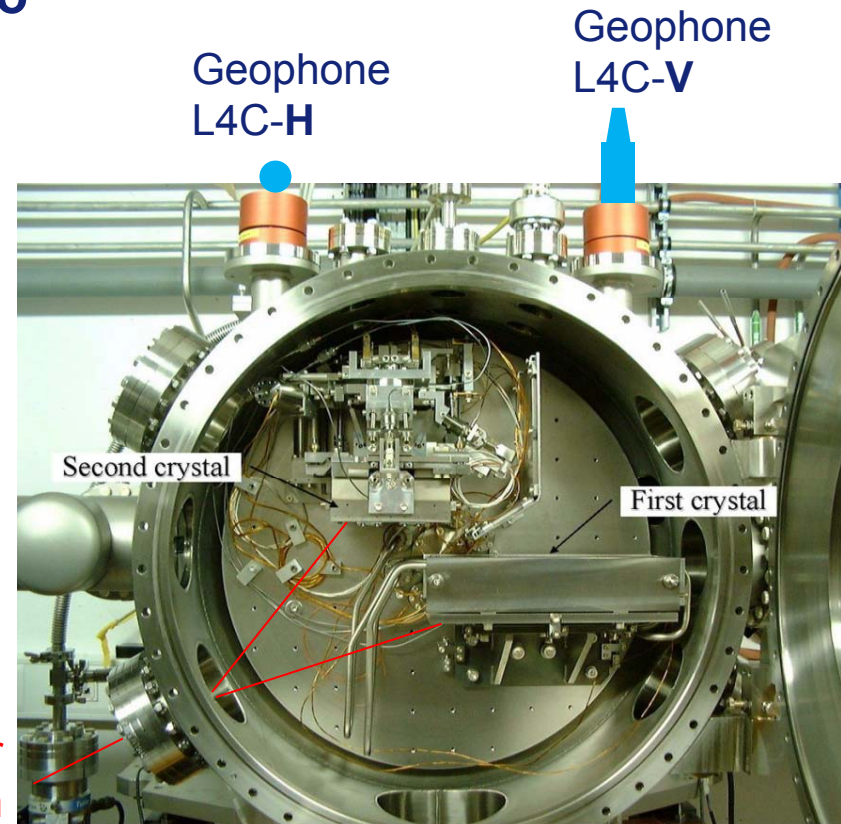


DCM vibration tests in BM25 (2004)

BM25 mono



Laser beam



Duo-beam Laser Vibrometer

Summary

- Thermal deformation can be accurately modeled
- Crystal monochromator has focusing effects ($R \sim 200$ m)
- Thermal deformation depends on Poisson's ratio ν :

$$\Delta\theta \sim (1 + \nu)$$

but Anisotropic elasticity of the silicon can be taken into account by use of an average Poisson's ratio in a simulation with isotropic and constant elasticity

- There are rooms for the improvement in terms of stability, and initial deformation of the crystal monochromator

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(* *Left ESRF*)

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