

Injection Efficiency – Impact of IDs on the Horizontal Beam Dynamics

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Introduction – Top Up, static and dynamic field components

Planar Undulator U125

- before re-shimming
- afterwards
- remaining problems

APPLE II-type Undulator UE112

compensation of dynamic field components:

- passive – with L-shims in the elliptical mode
- active – with current carrying wires in the inclined mode
- non-linear lens

Summary

Top Up operation - radiation safety requirement:

Injection efficiency > 90 %, assured by interlock

currently impossible with the IDs installed at BESSY – especially if located in high β_x straight sections (like the U125 and the UE112)

Mechanism of the beam interaction with IDs

problems can arise from poor field quality of ID – *static field components*:

prop. $1/E$ - example U125, before re-shimming

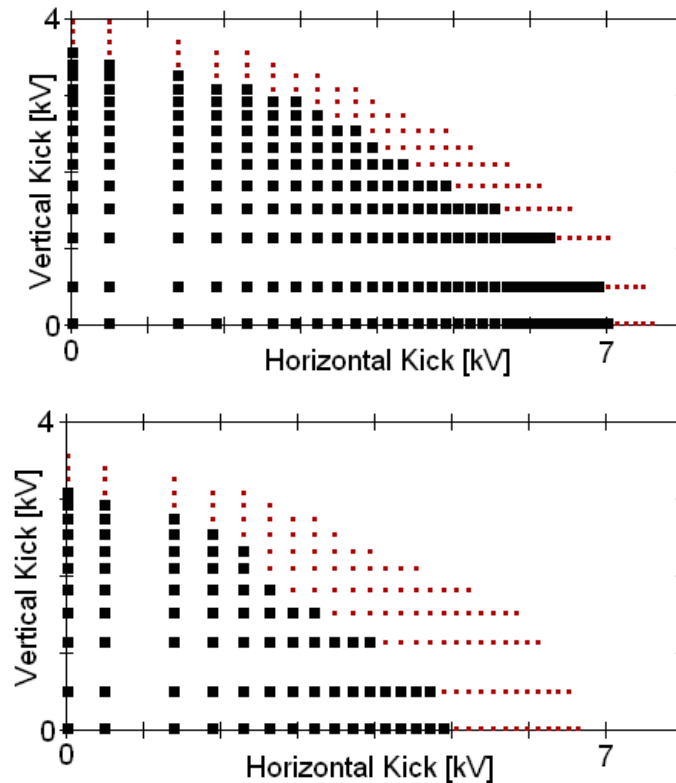
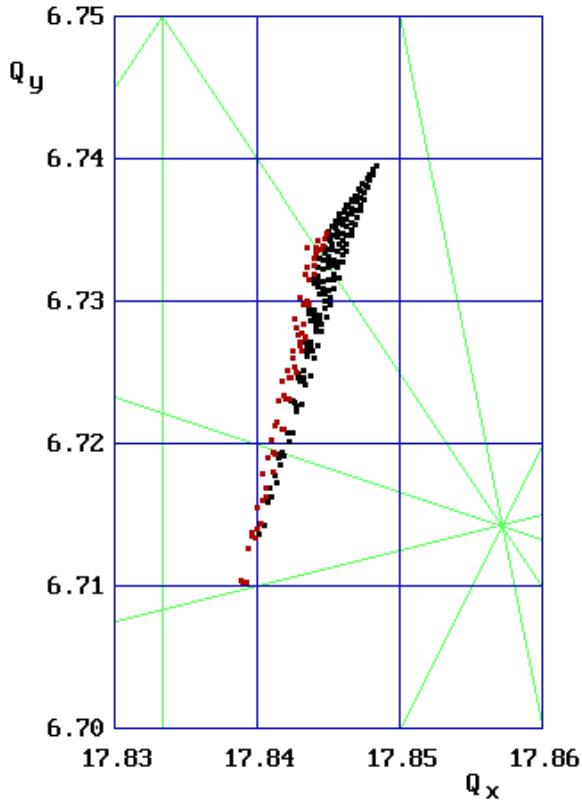
oscillatory beam motion - even in the ideal 3D-undulator fields - leads to noticeable modifications of the dynamics – *dynamic field components, prop. $1/E^2$* :

- horizontal plane – field roll-off due to finite width of poles, non-linearity important for large beam excursions
- vertical focusing – like in ordinary dipoles, non-linearity usually not important

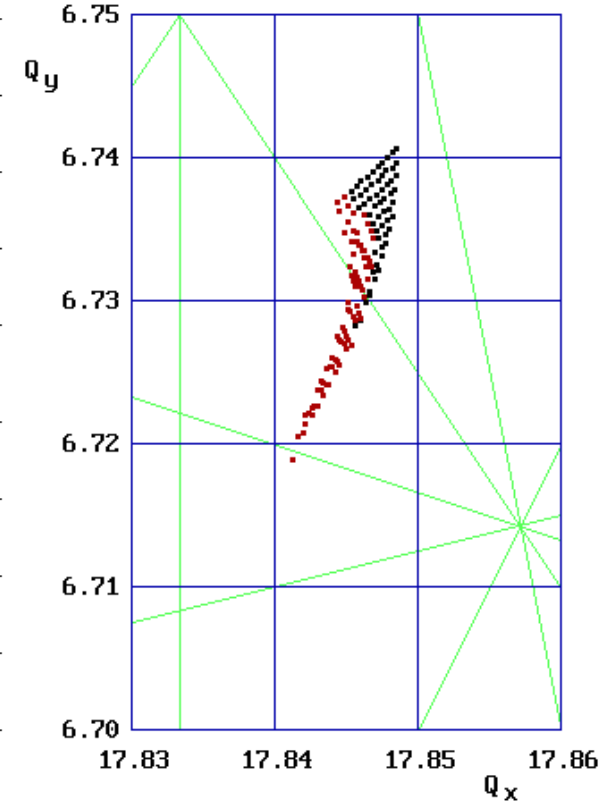
APPLE-type undulators show a mixture of both effects

general observation: injection efficiency scales with the available dynamic aperture

ID-gap open



U125ID2R = 15.7 mm



U125ID2R planar undulator with 1 T peak field:

- Expected modification of vertical beam dynamics – aperture reduction linear effect
- Unexpected horizontal dynamics – 30% reduction of dynamic aperture

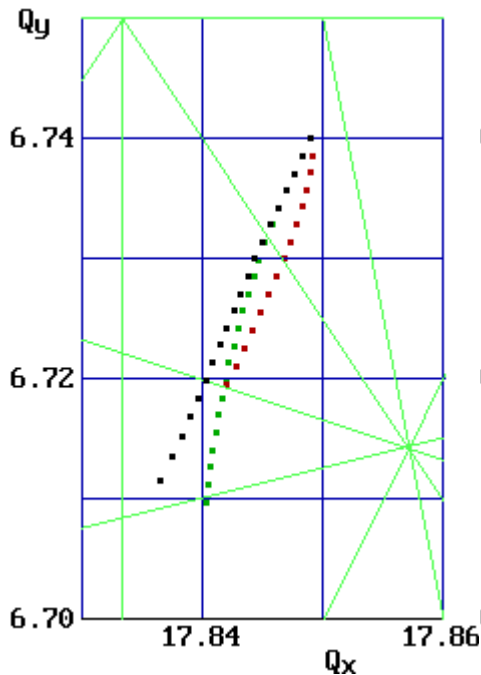
horizontal beam dynamics:

- dynamic field integrals due to field roll off (estimated by J. Bahrtdt)

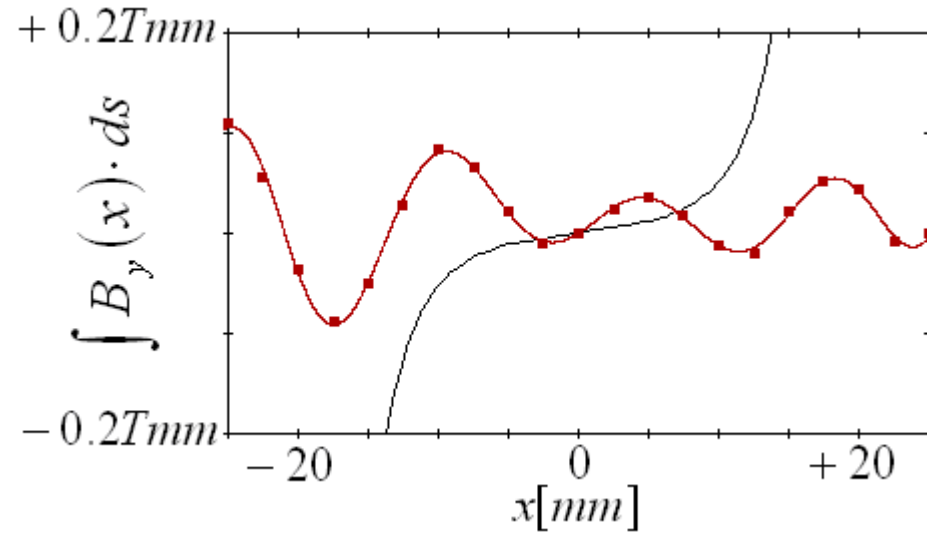
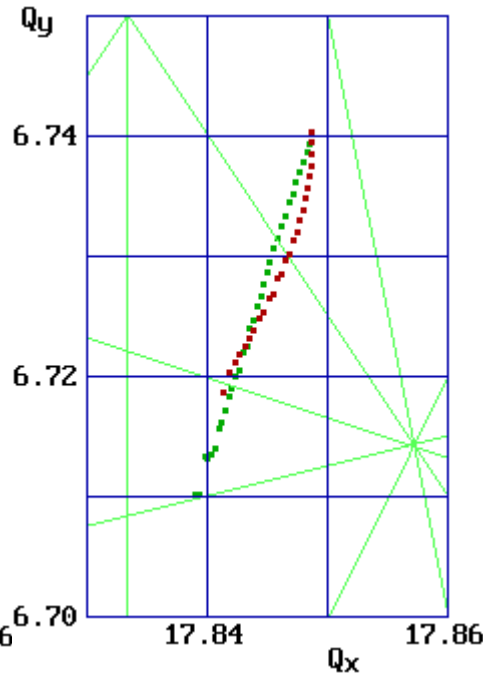
- static field integrals

stretched wire measurement (BESSY ID-group)

theory



measurement

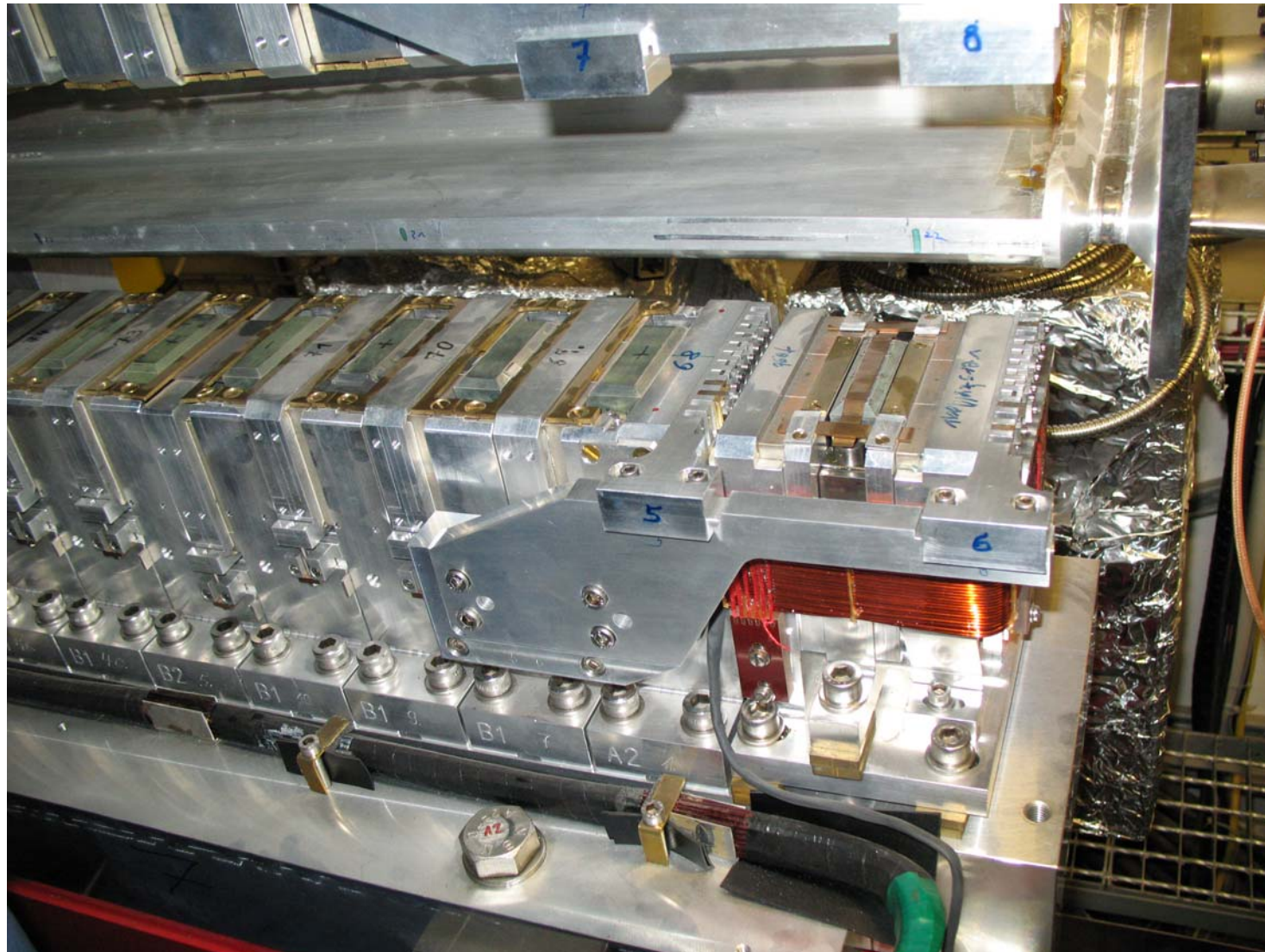


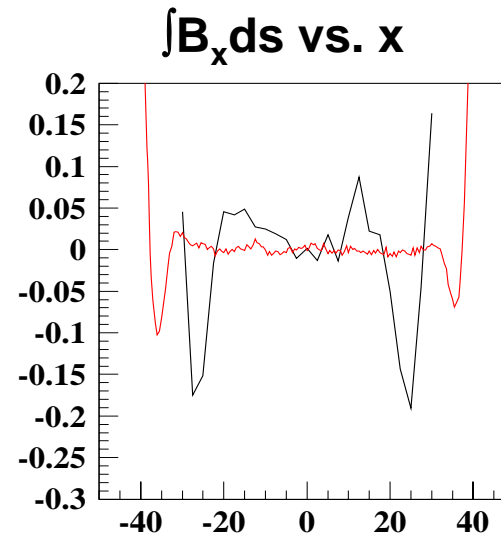
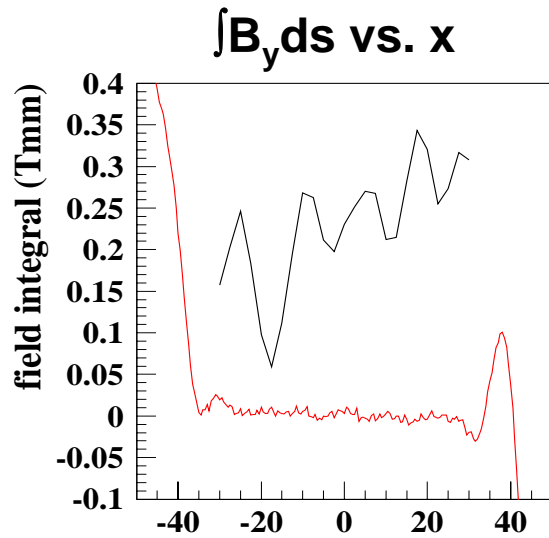
- gap open

- gap closed - dynamic effects only

- gap closed - dynamic and static effects

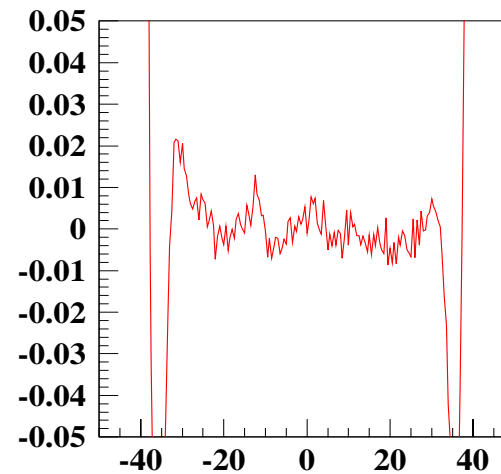
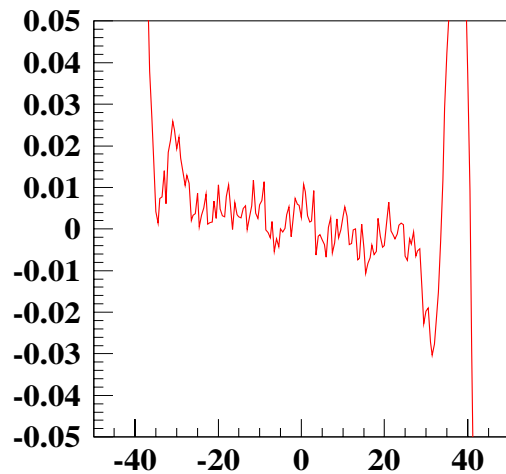
ID re-shimming required



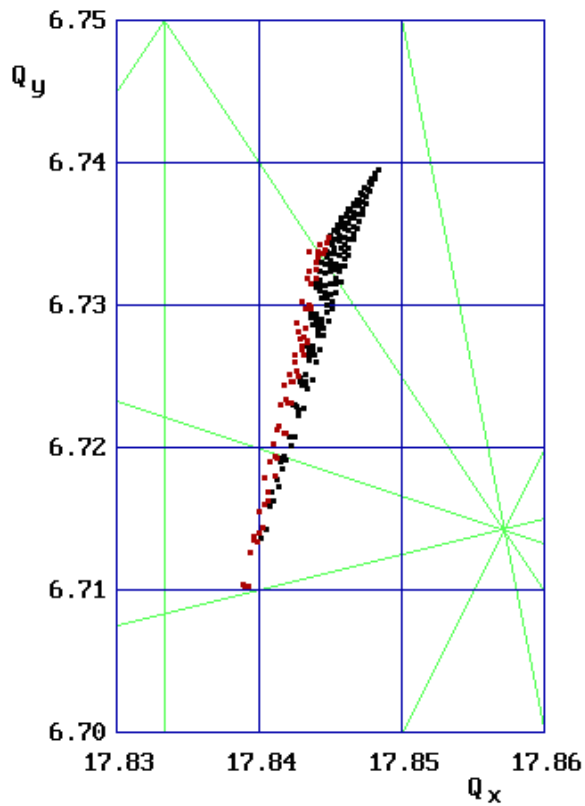


**before installation
of magic fingers**

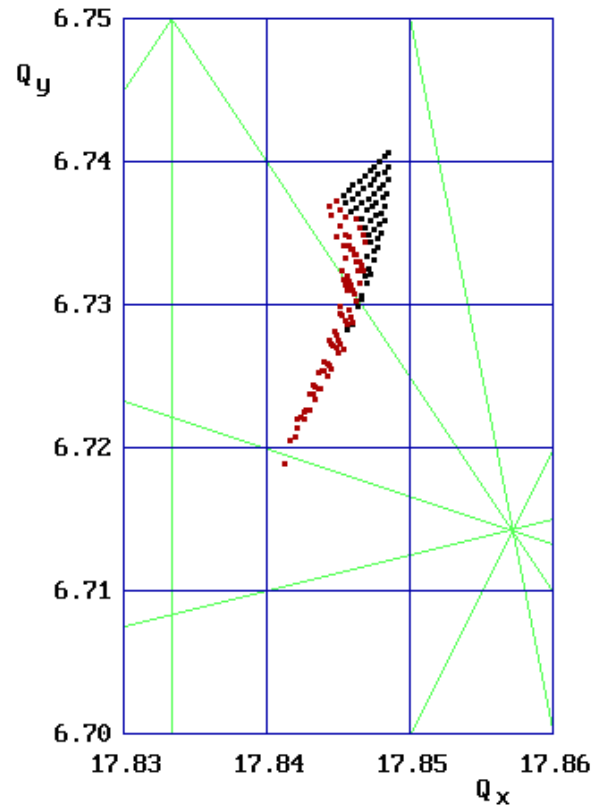
after installation



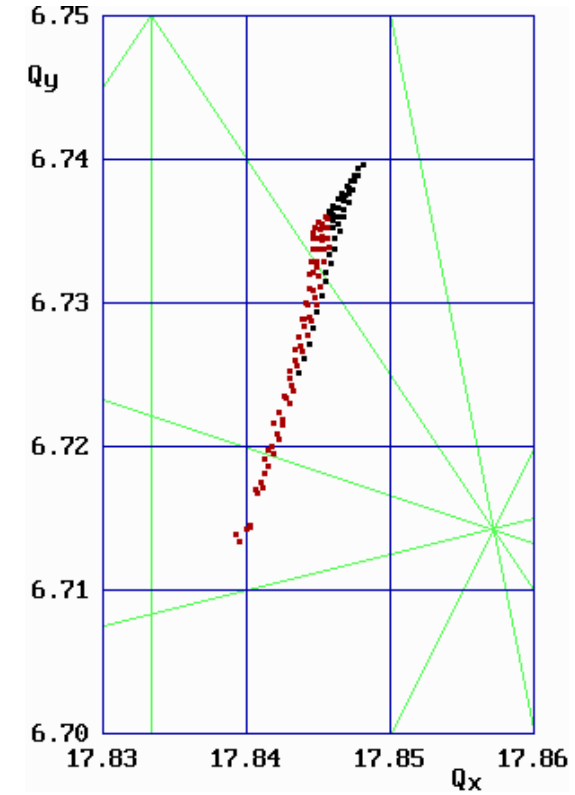
z (mm)



ID-gap open

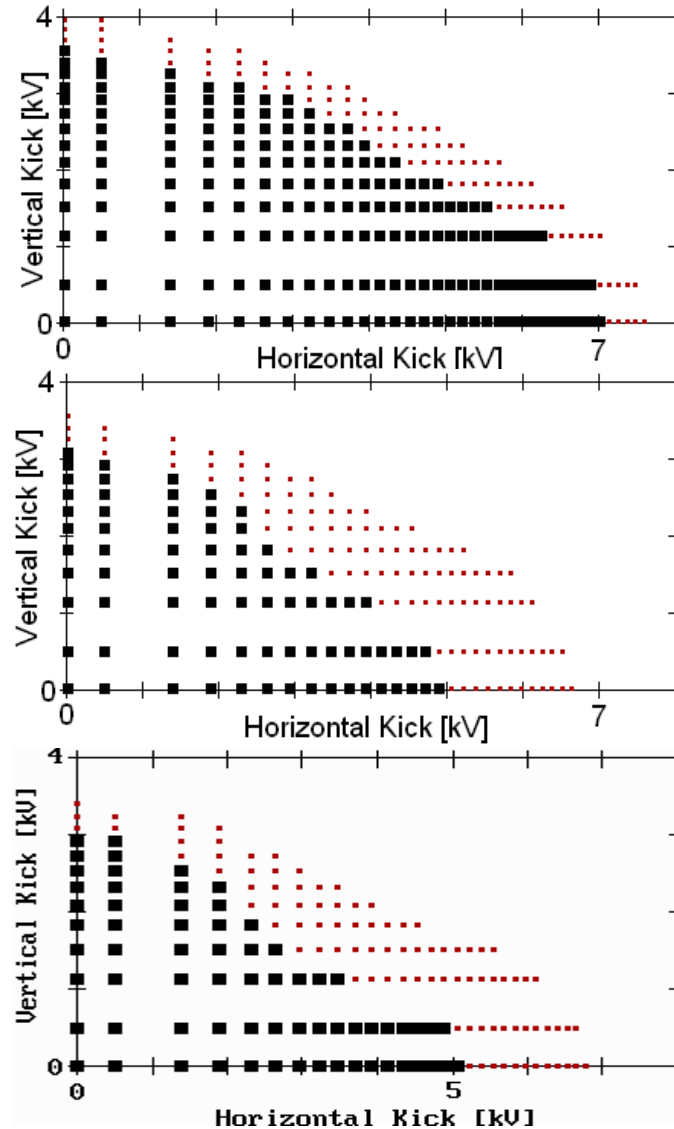


before



ID-gap = 15.7 mm

after re-shimming



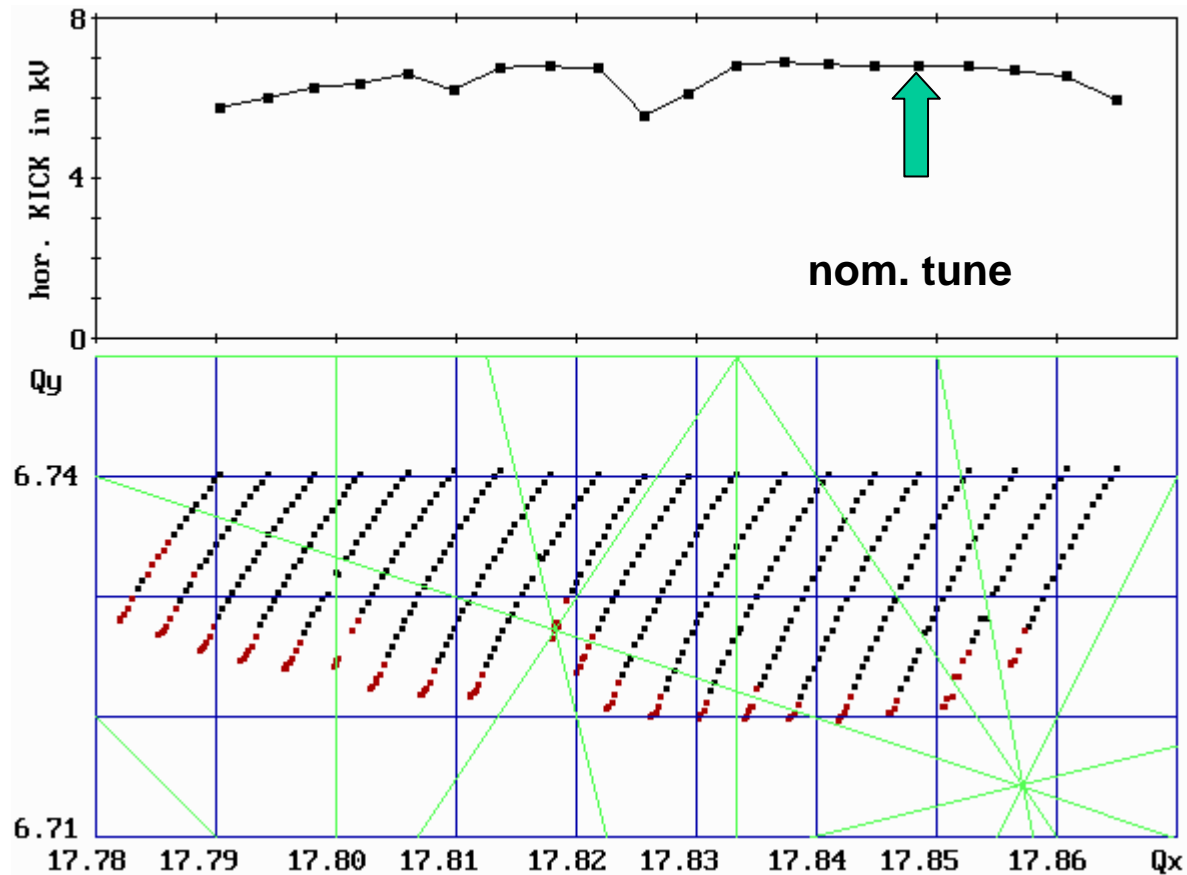
ID-gap open

**U125ID2R = 15.7 mm
before**

after re-shimming

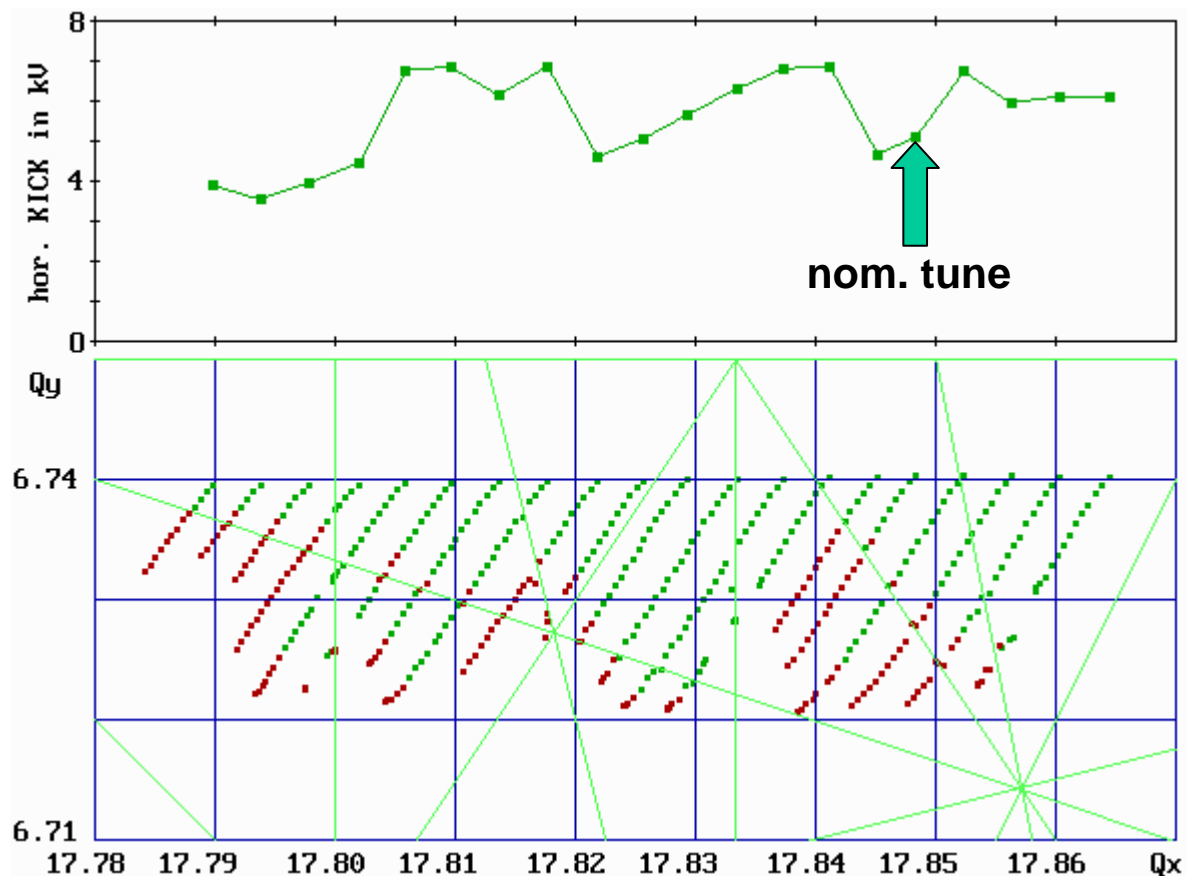
**next step – compensation of
dynamic field components**

ESLS @ DIAMOND



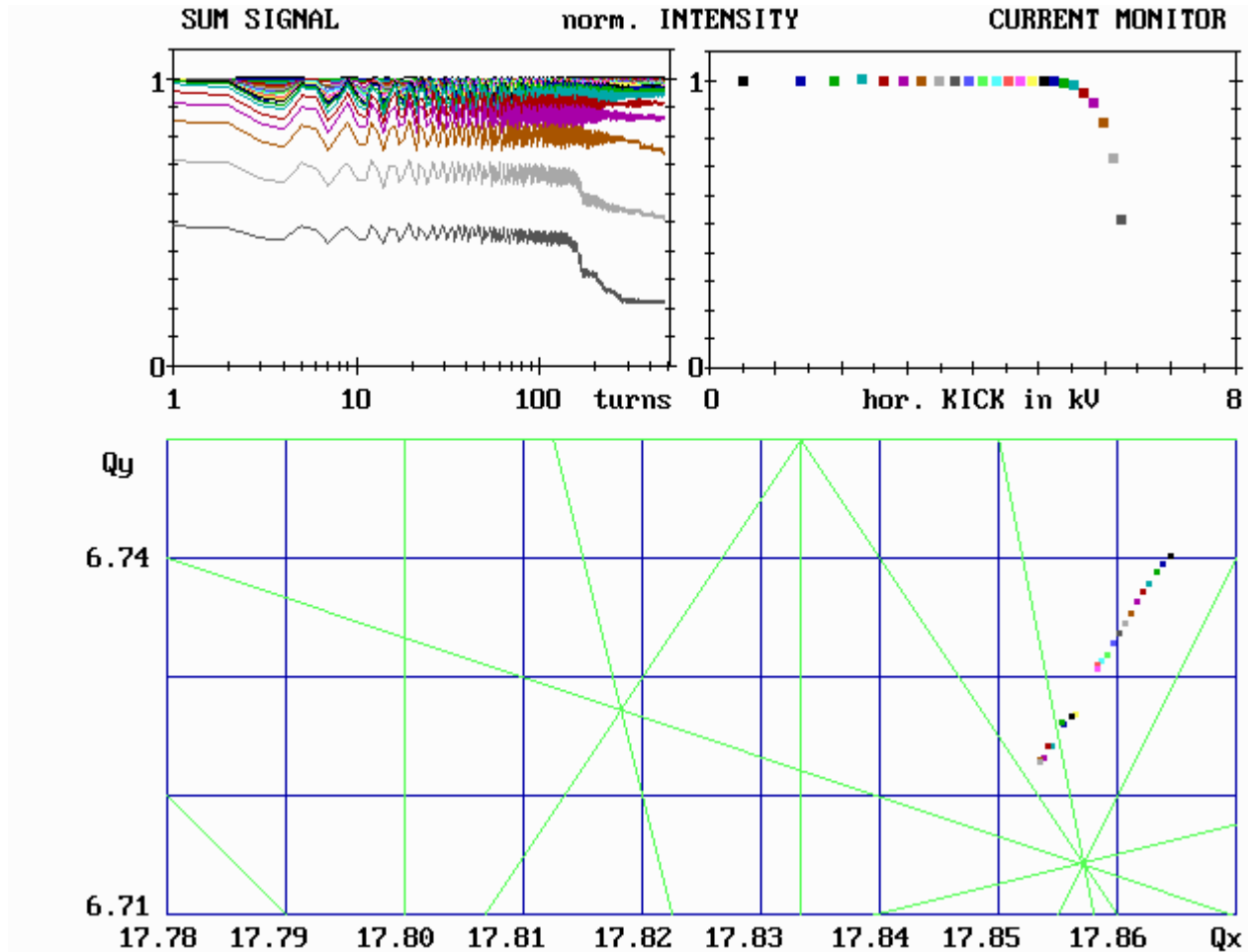
red dots –
beam loss >2%

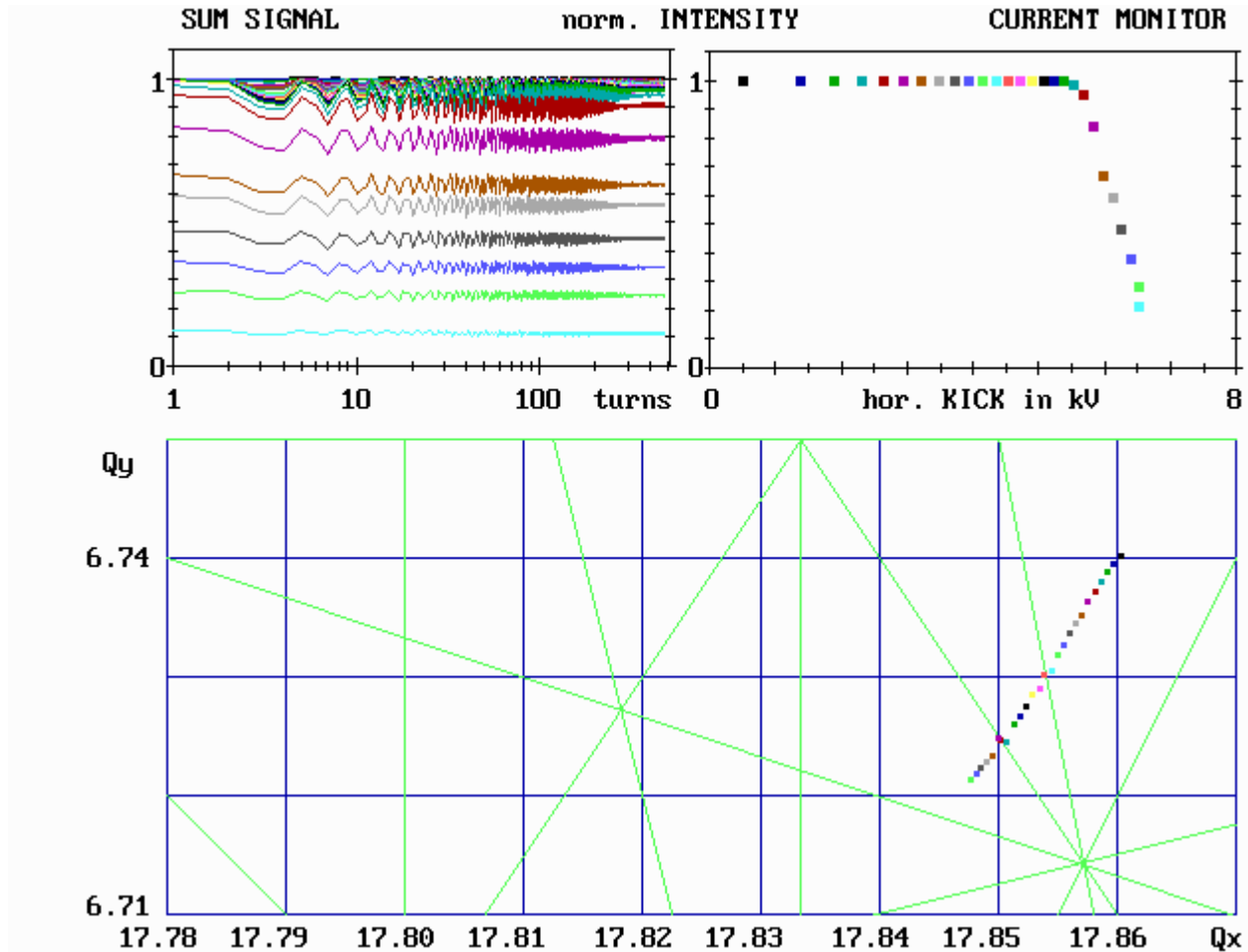
U125ID2R – gap=15.7 mm

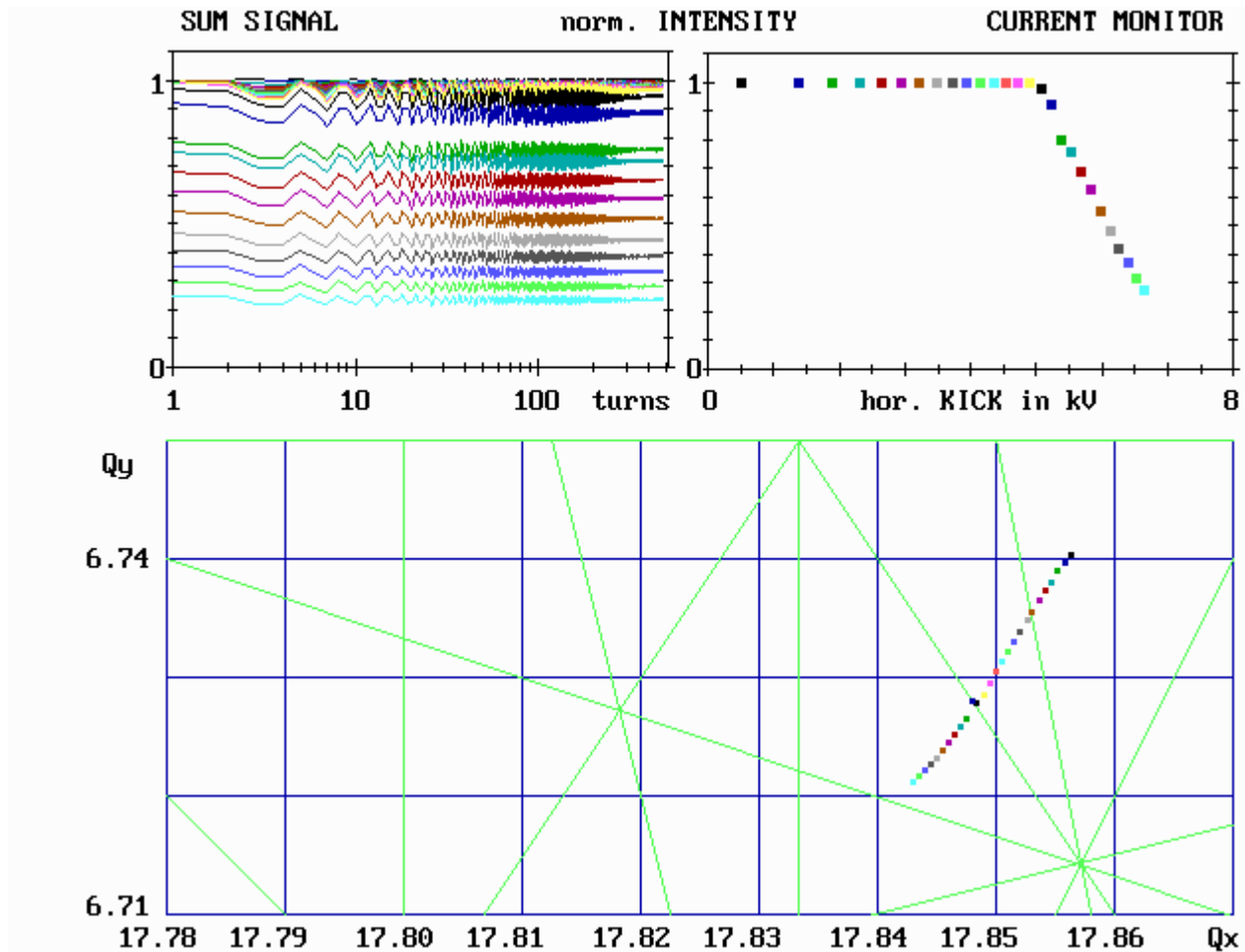


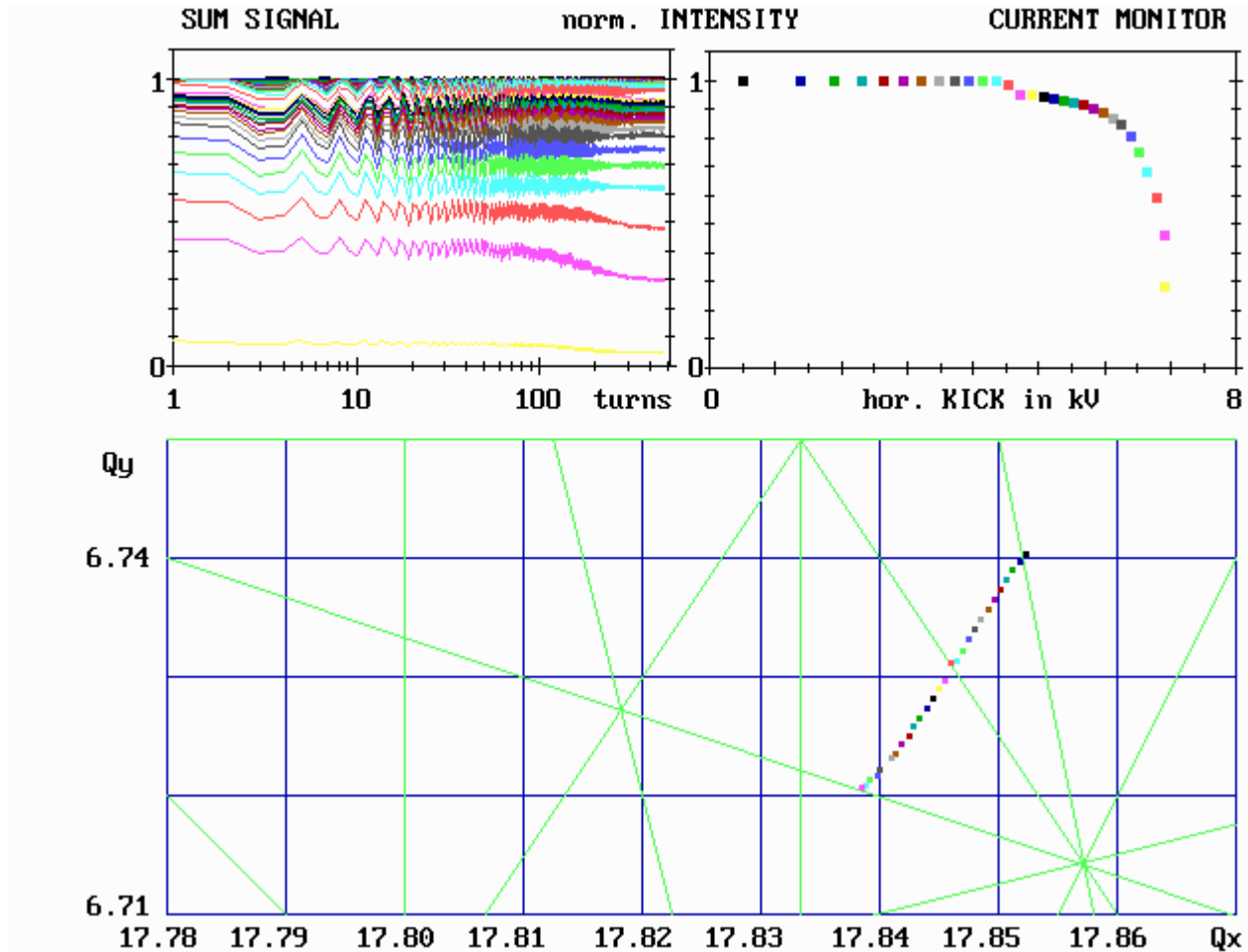
red dots –
beam loss >2%

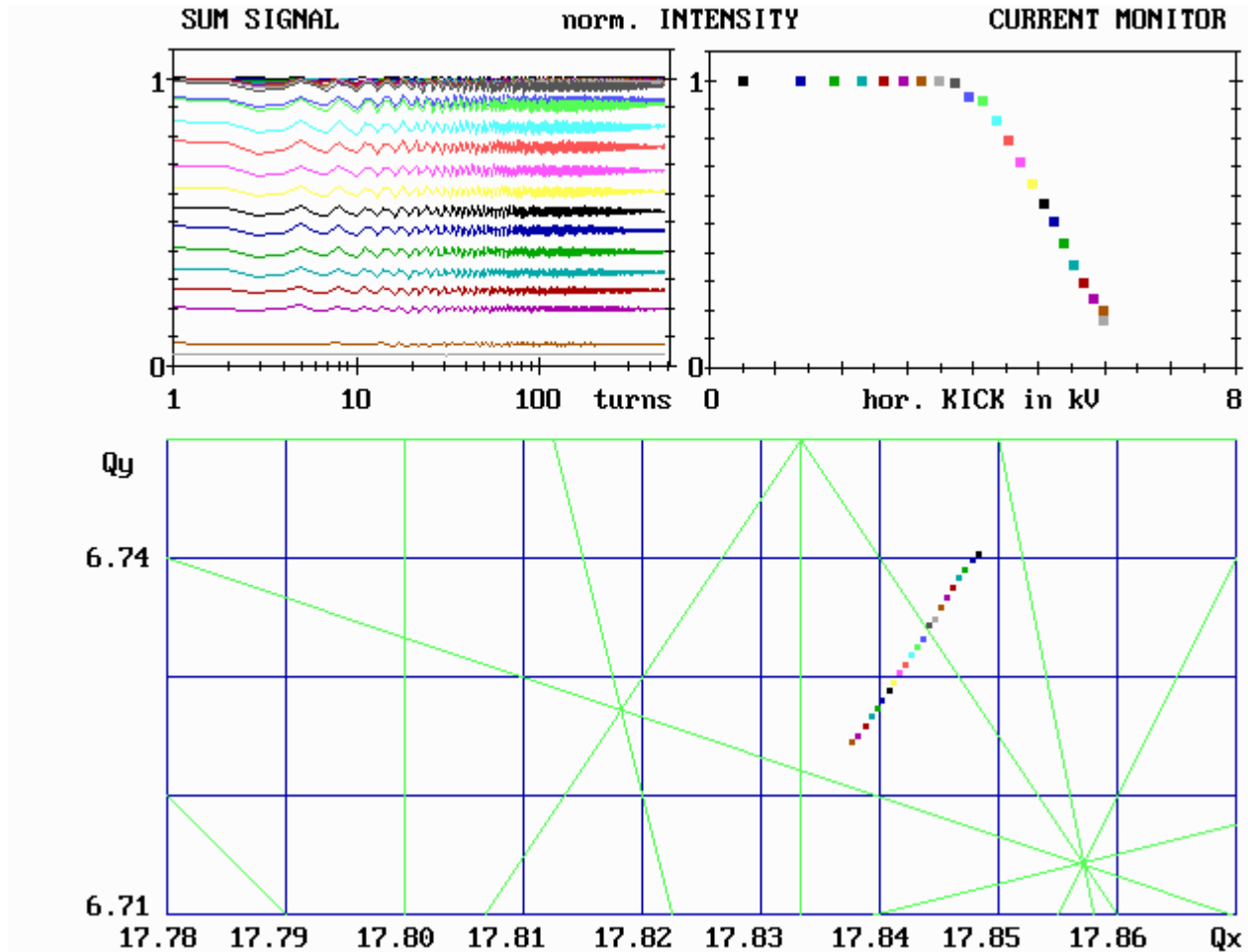
$3Q_x + 2Q_y$ – resonance critical at the nom. working point

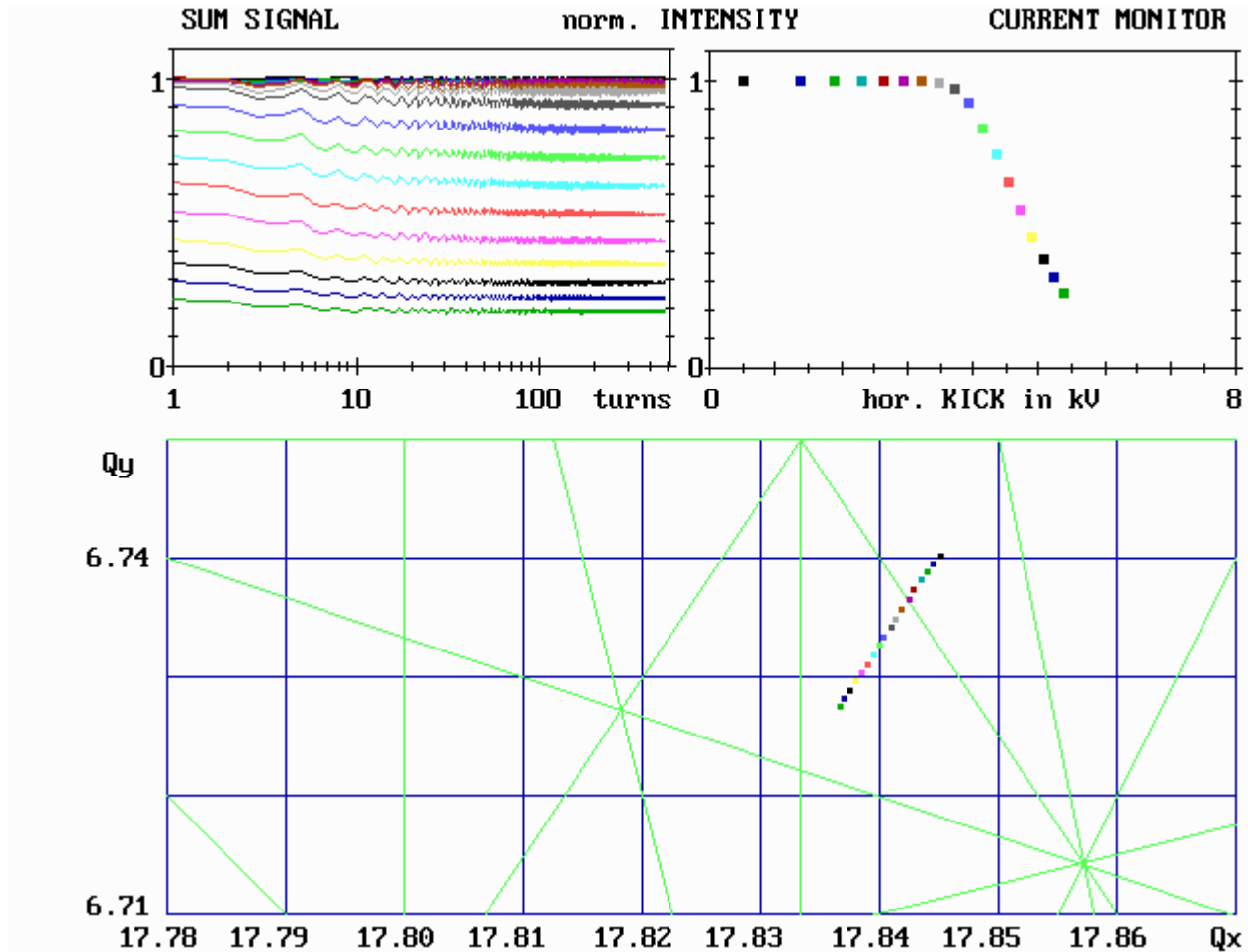


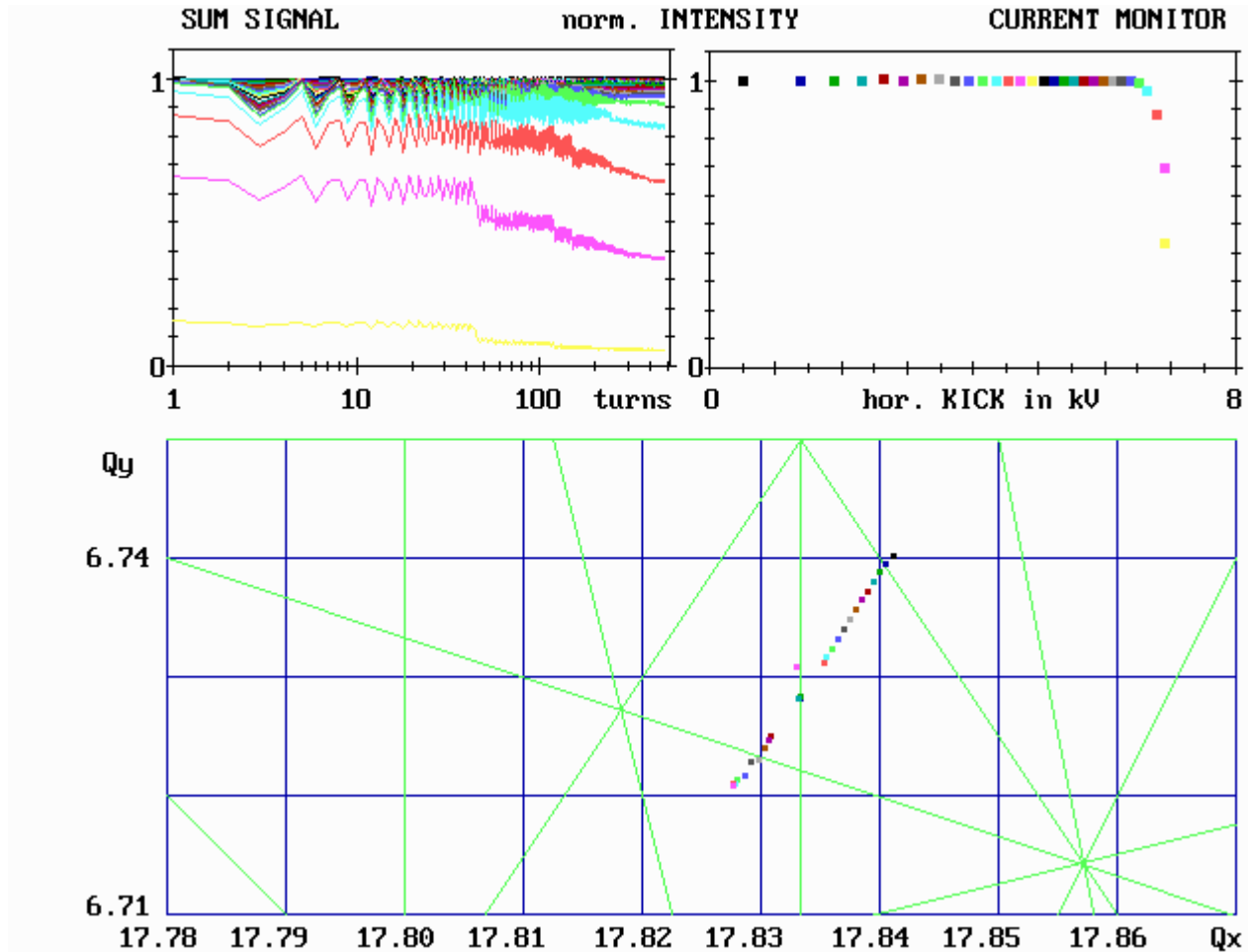


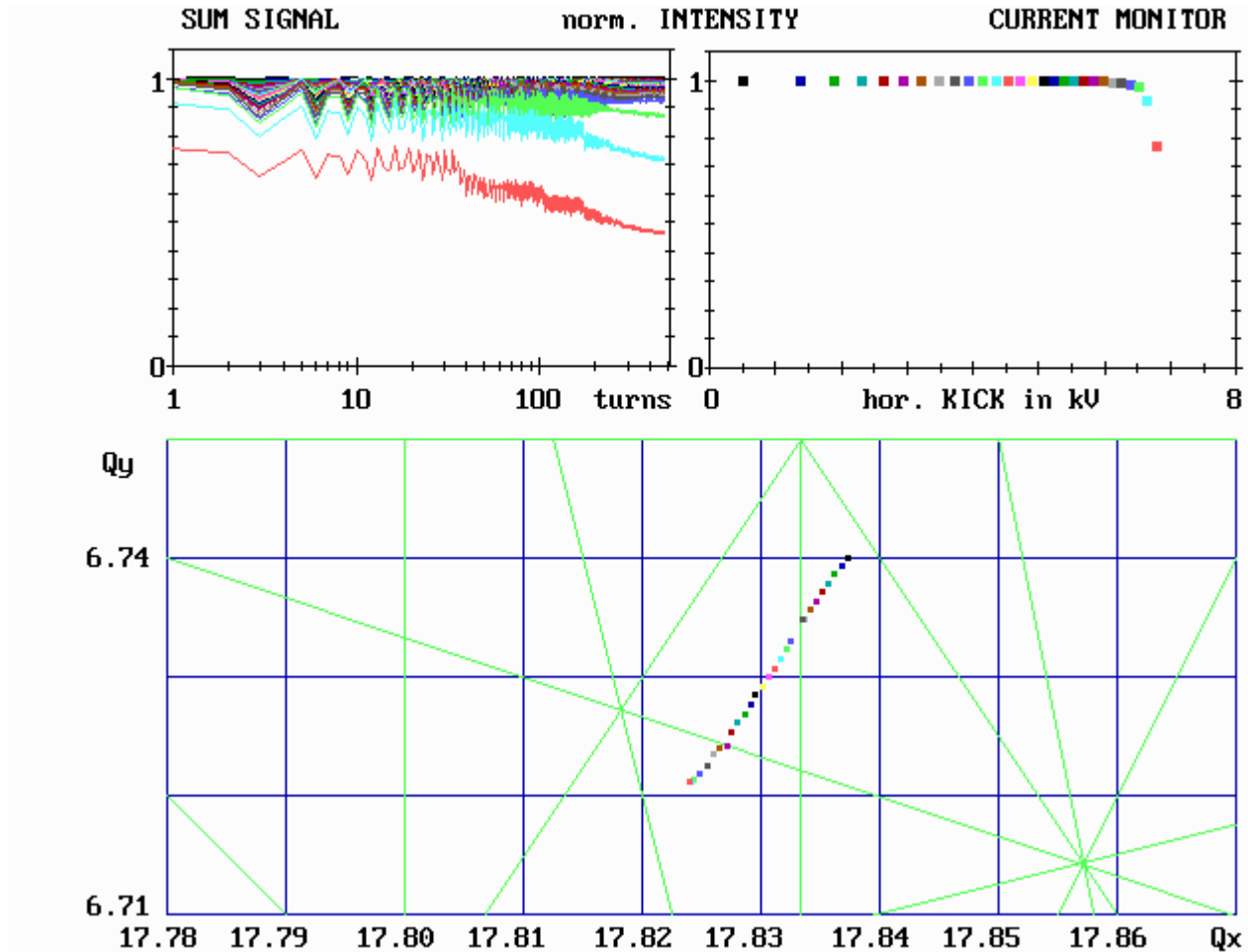


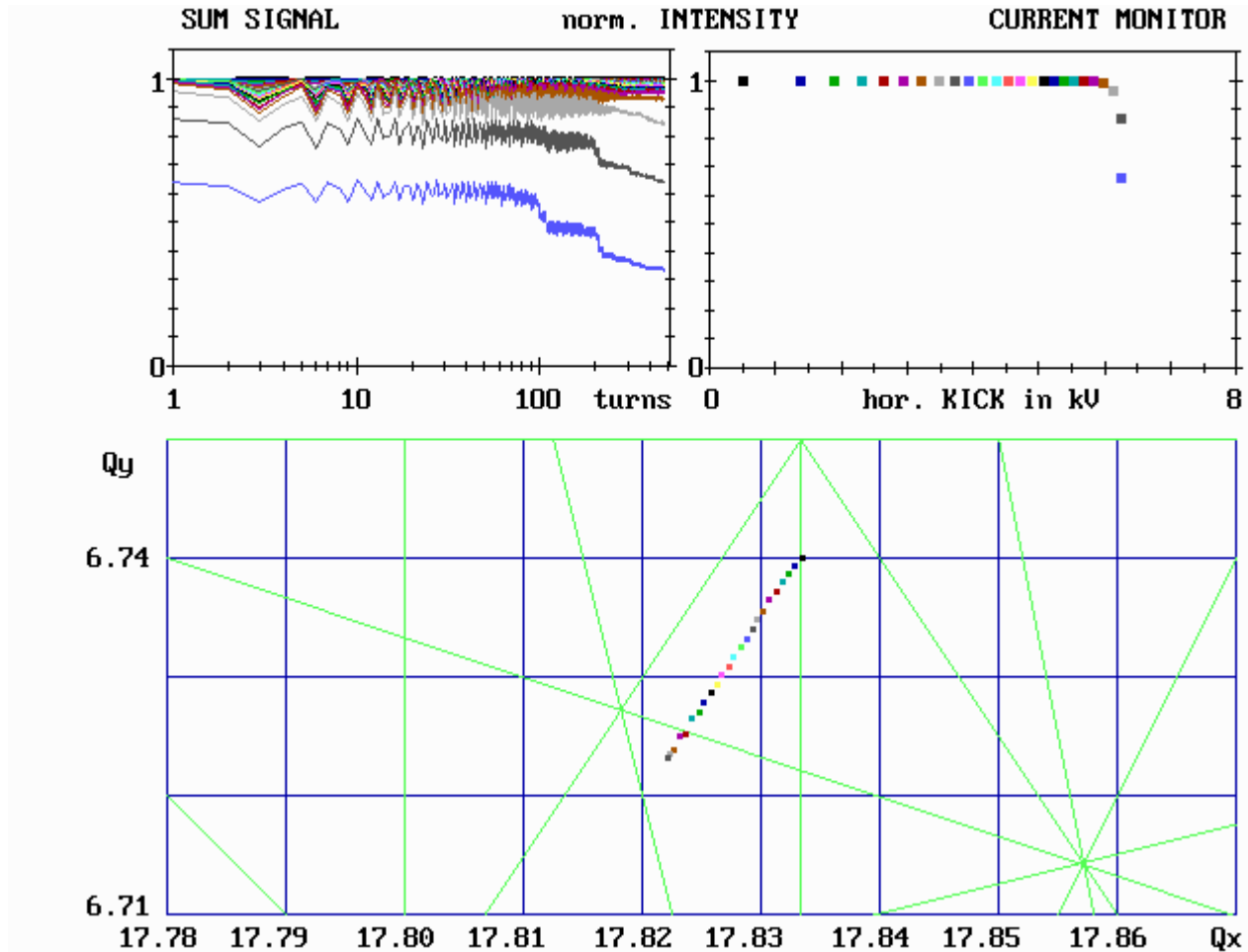


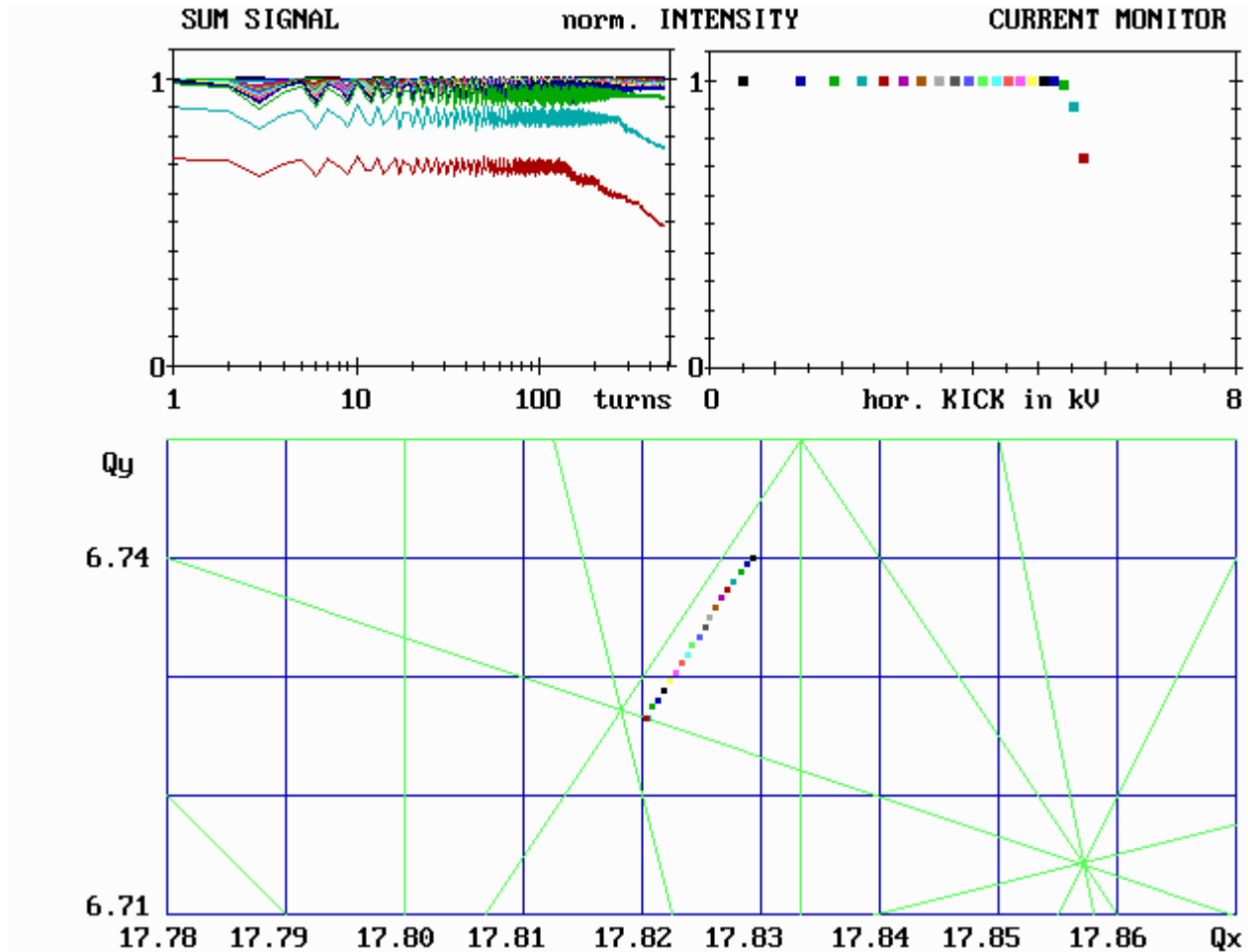


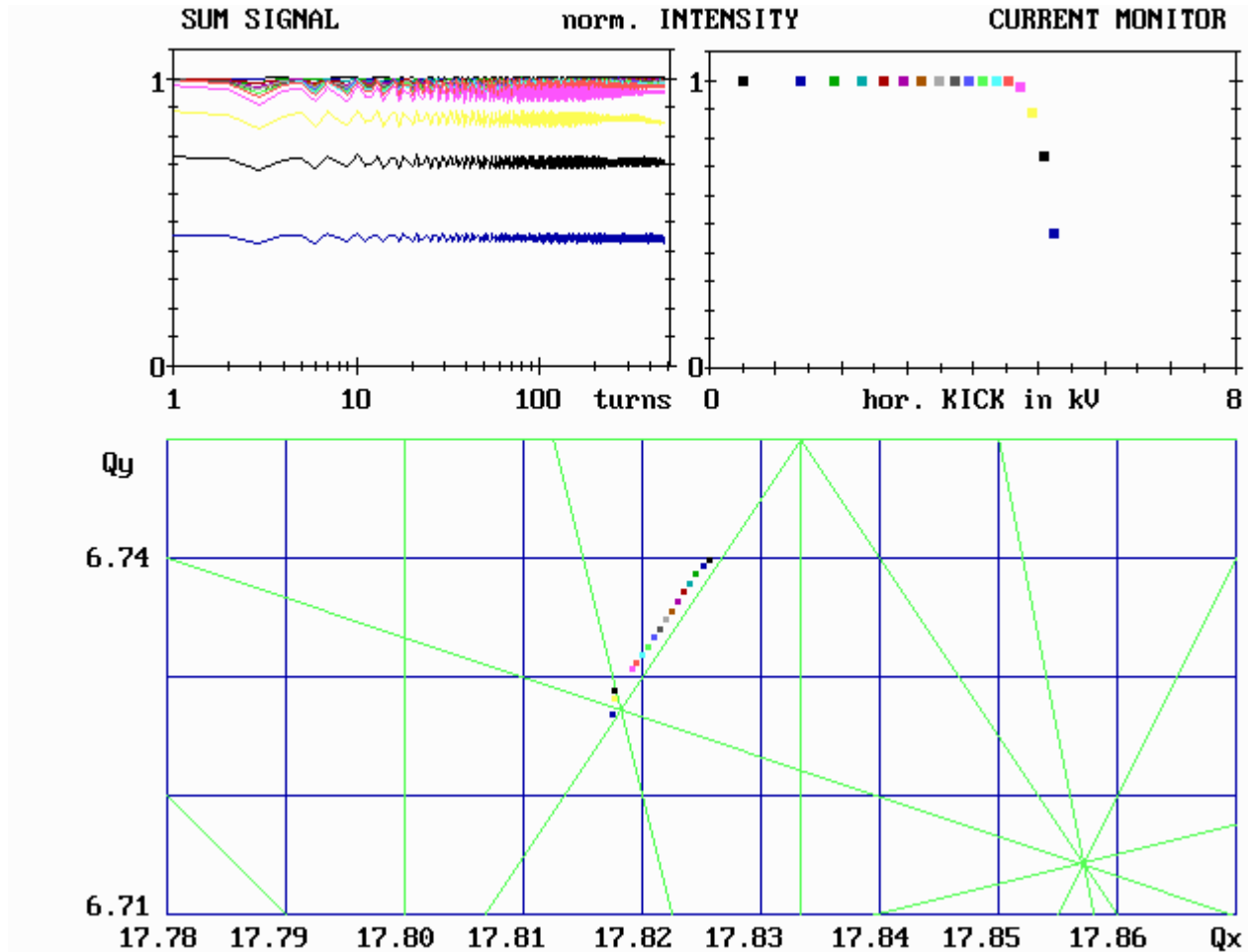


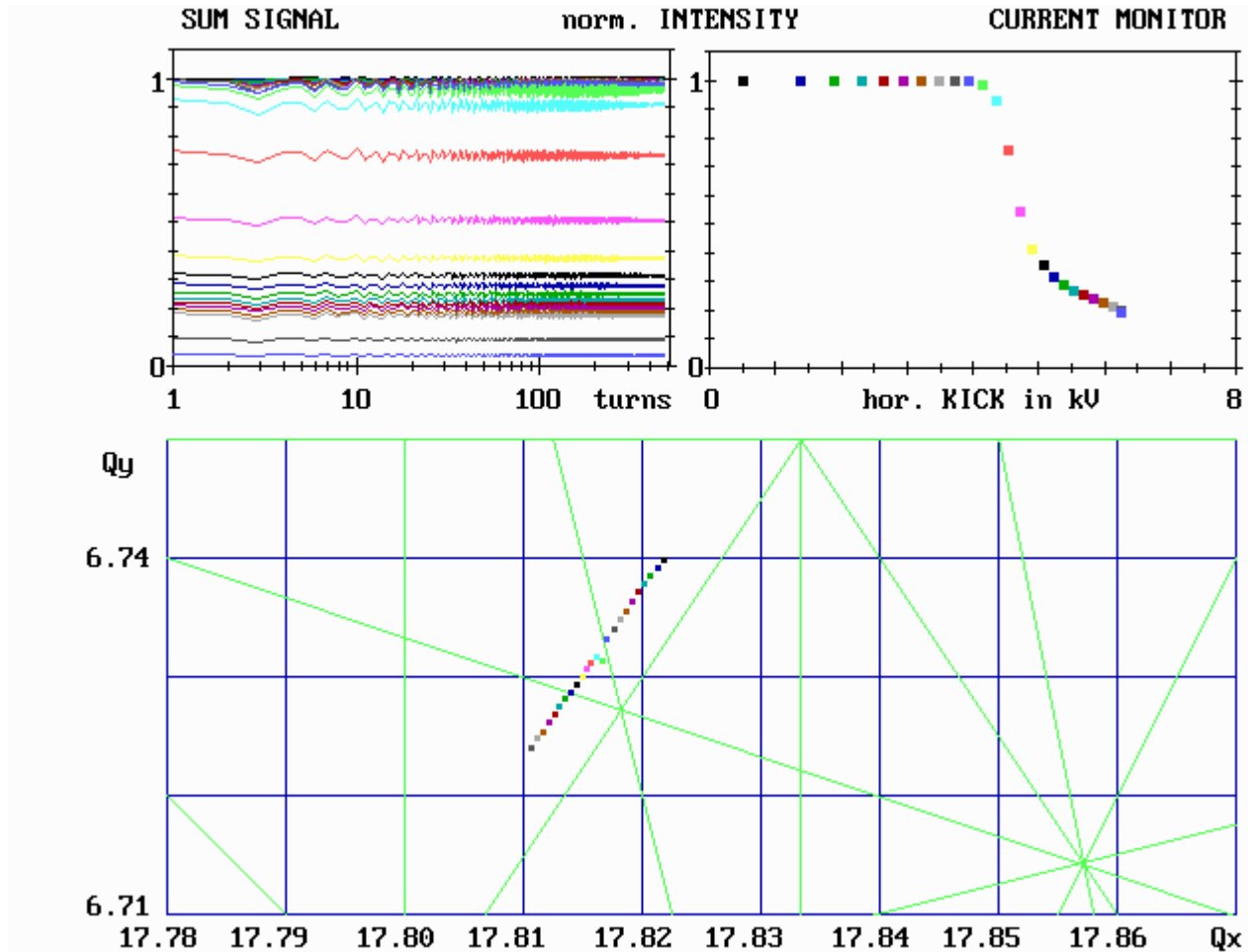


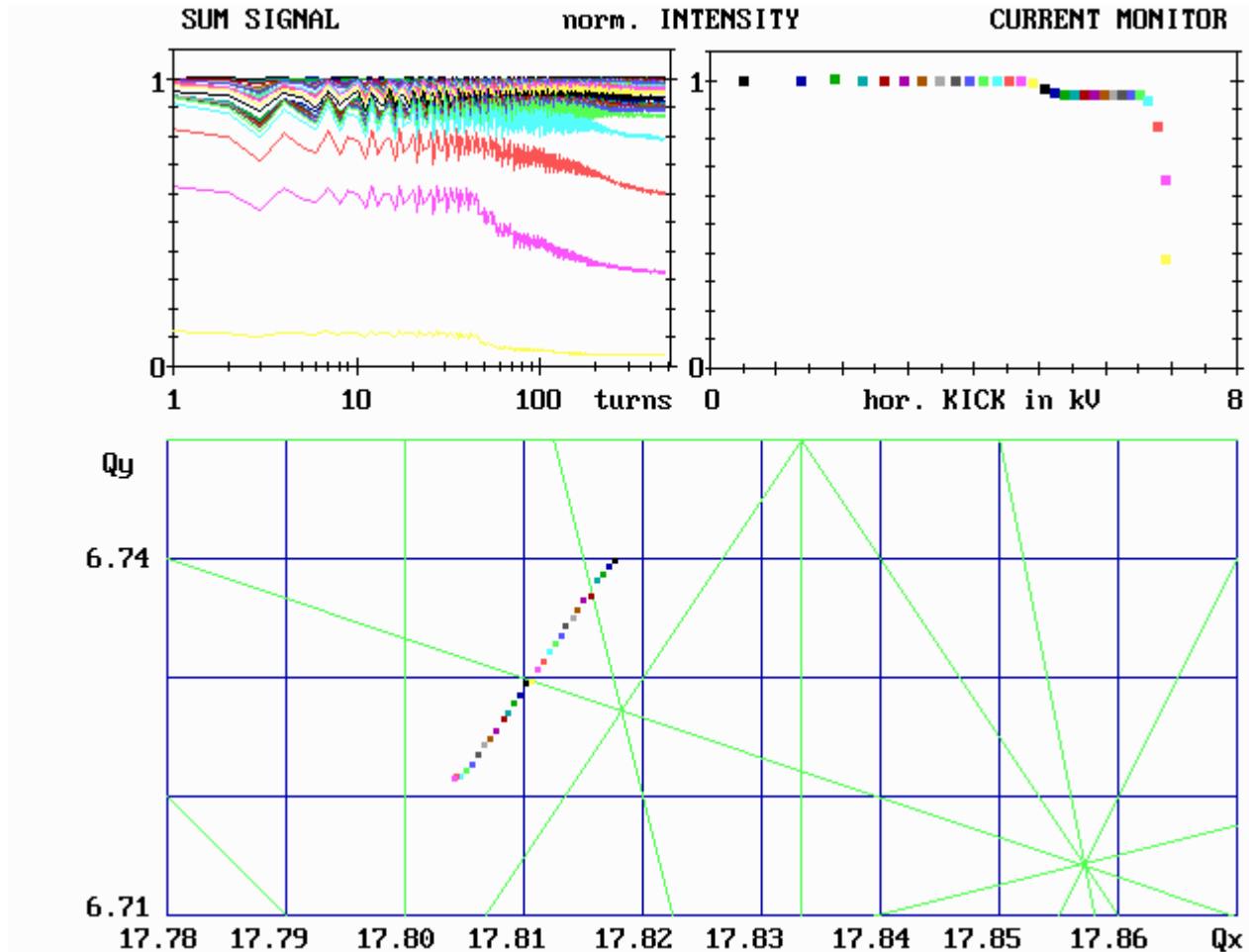


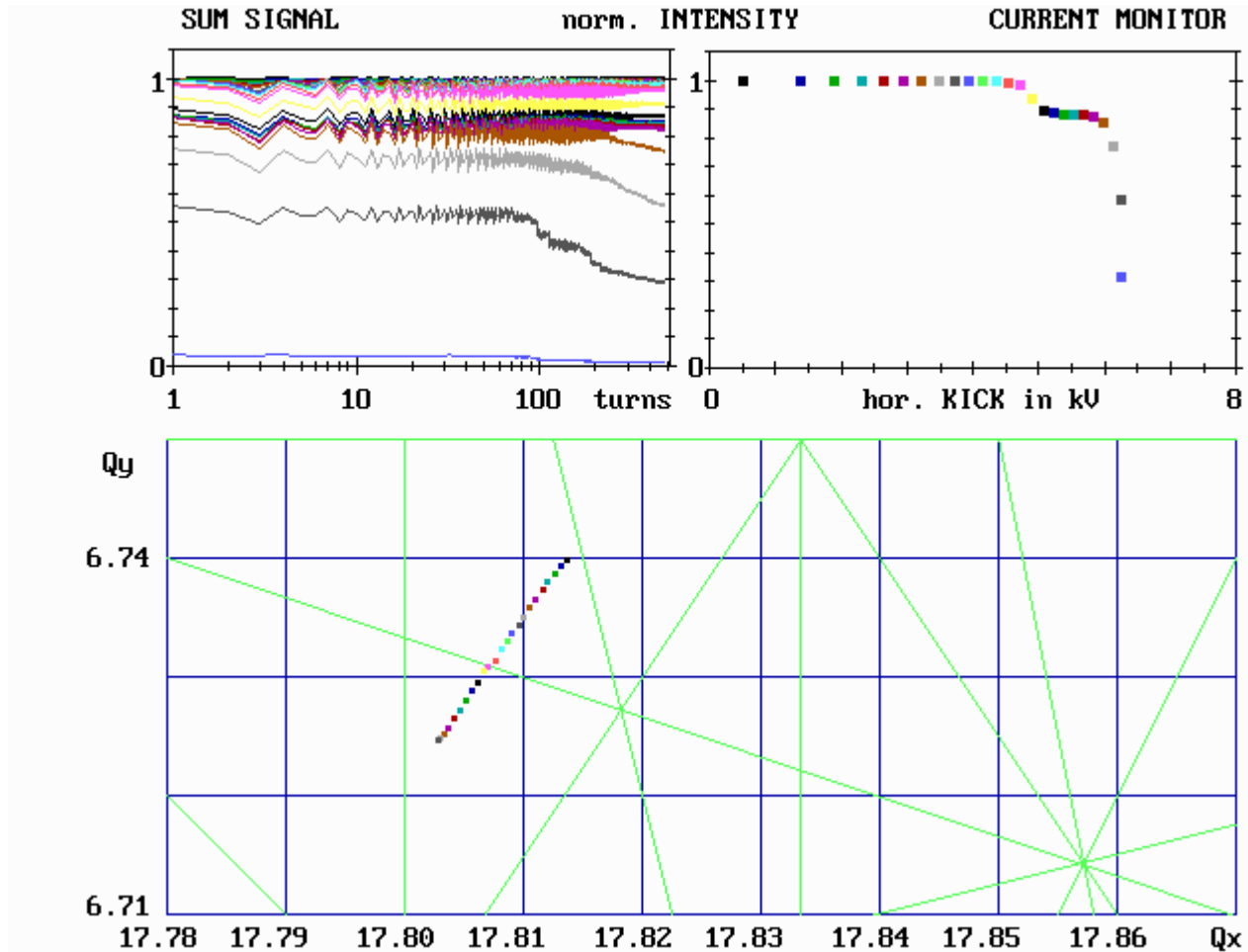


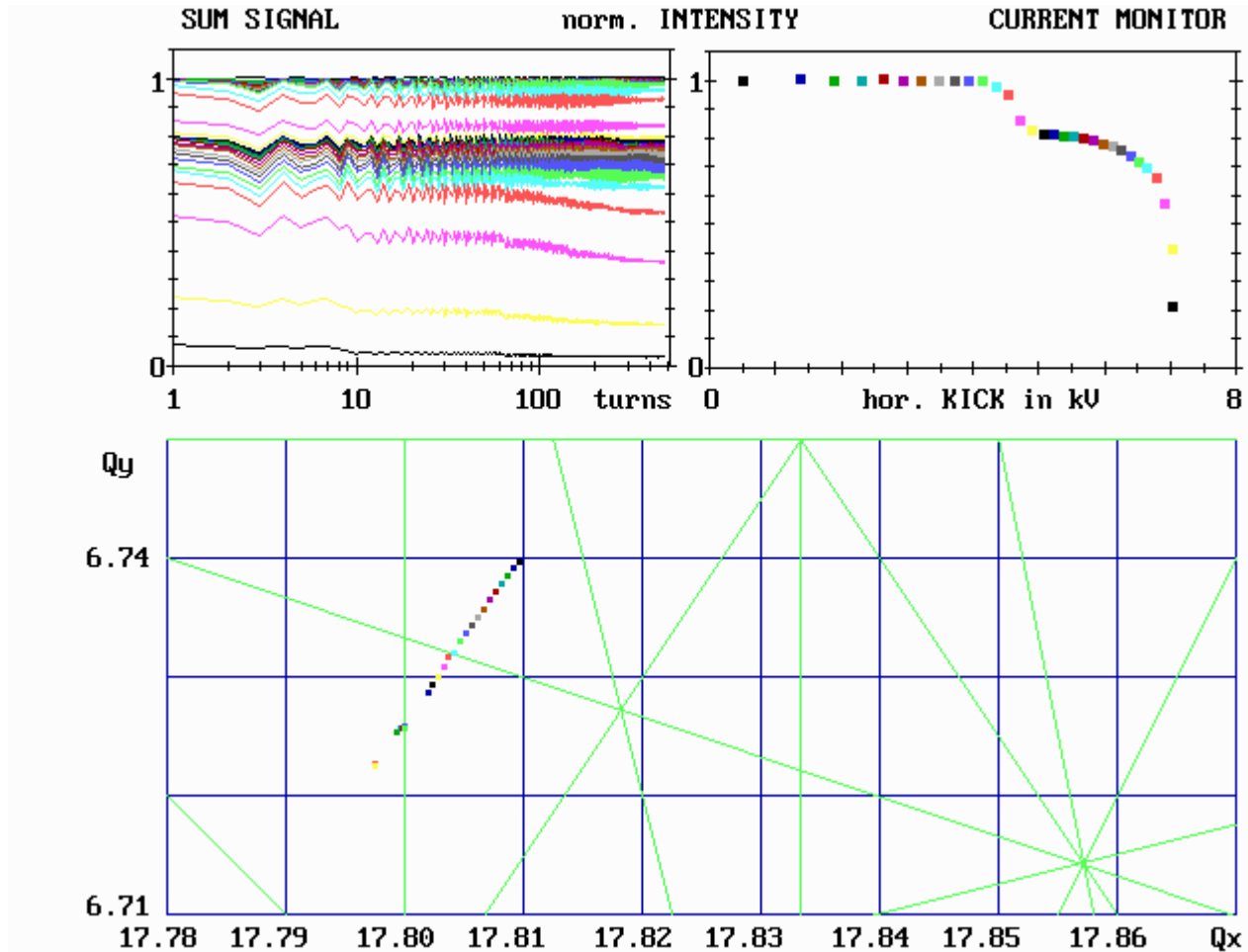


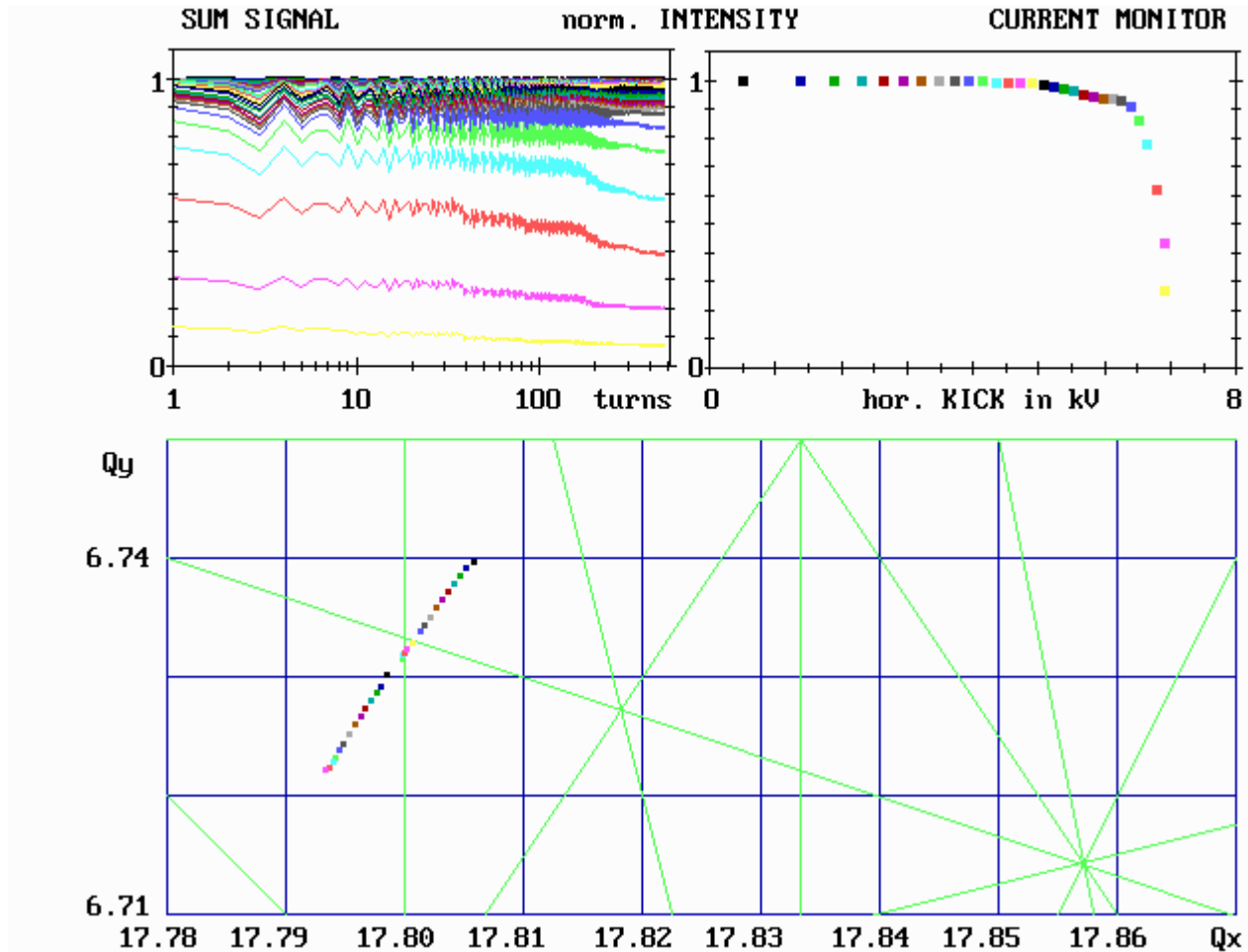


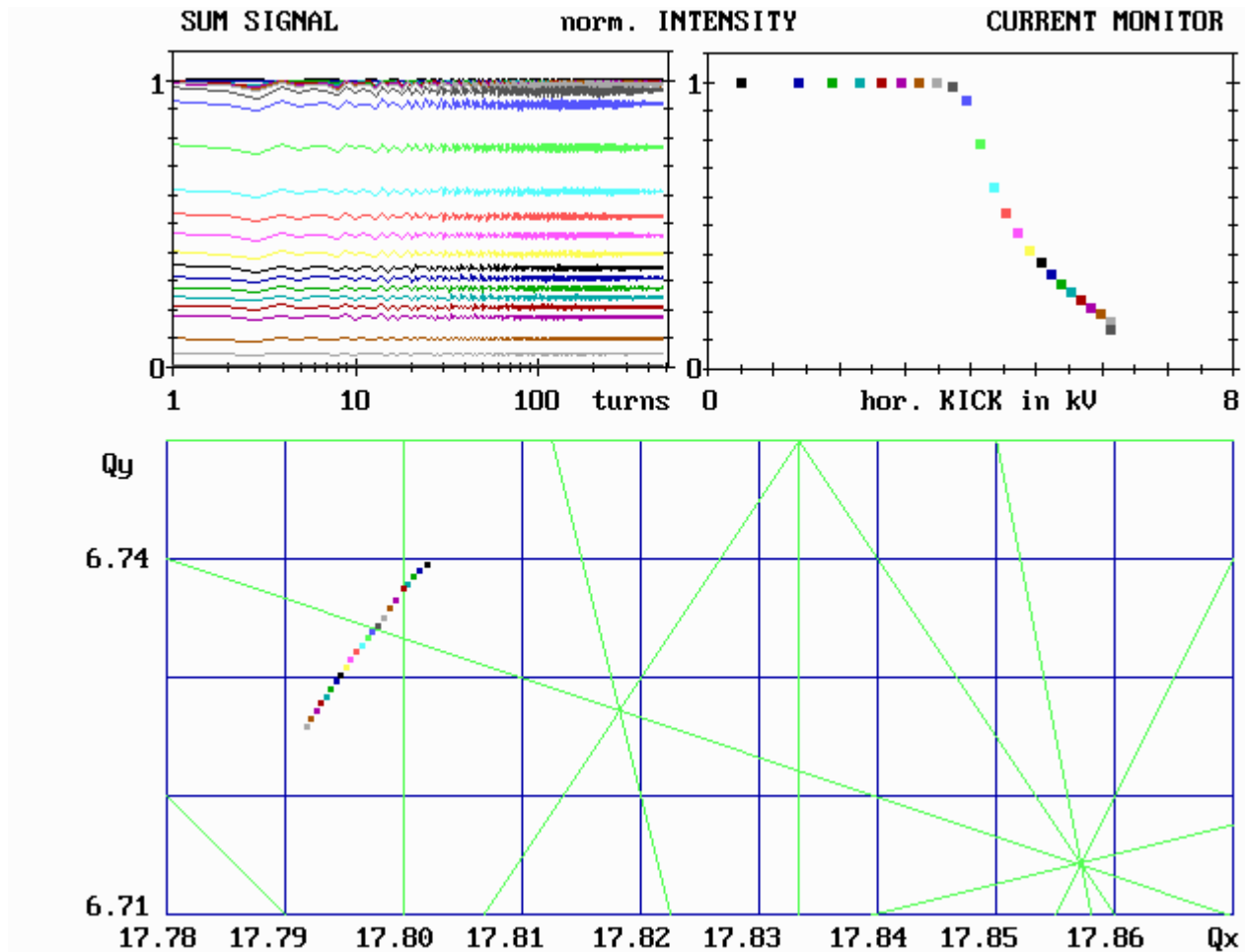


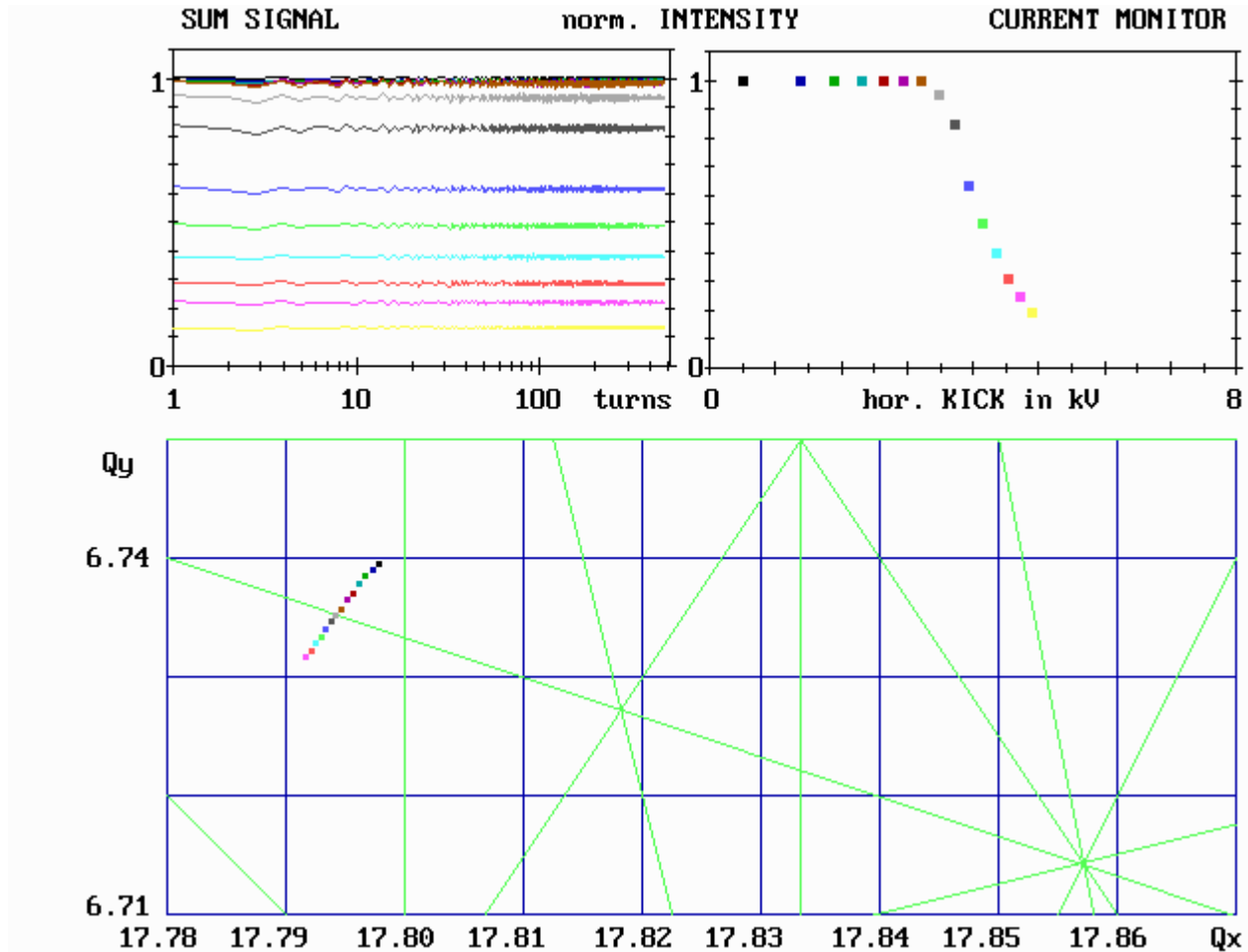


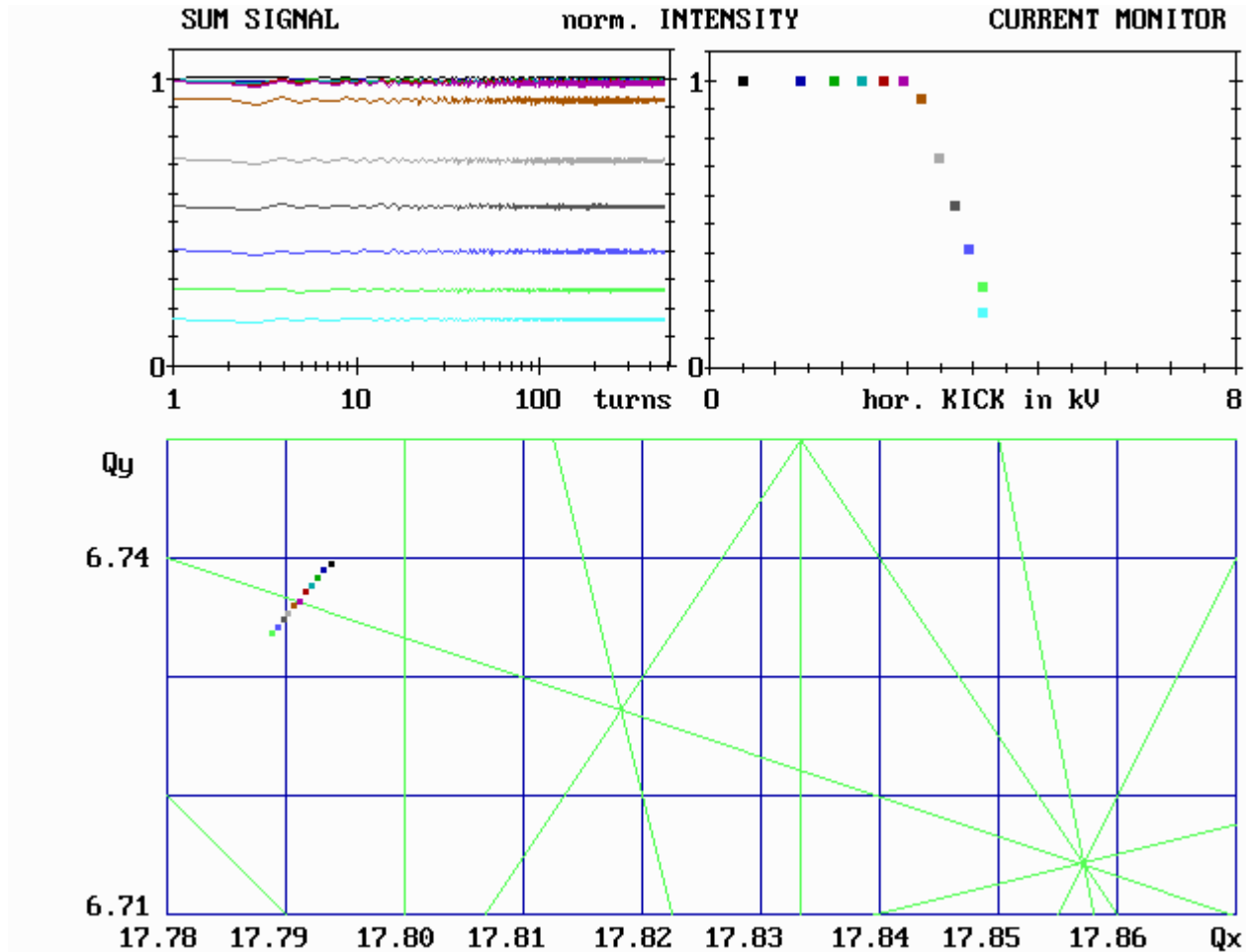


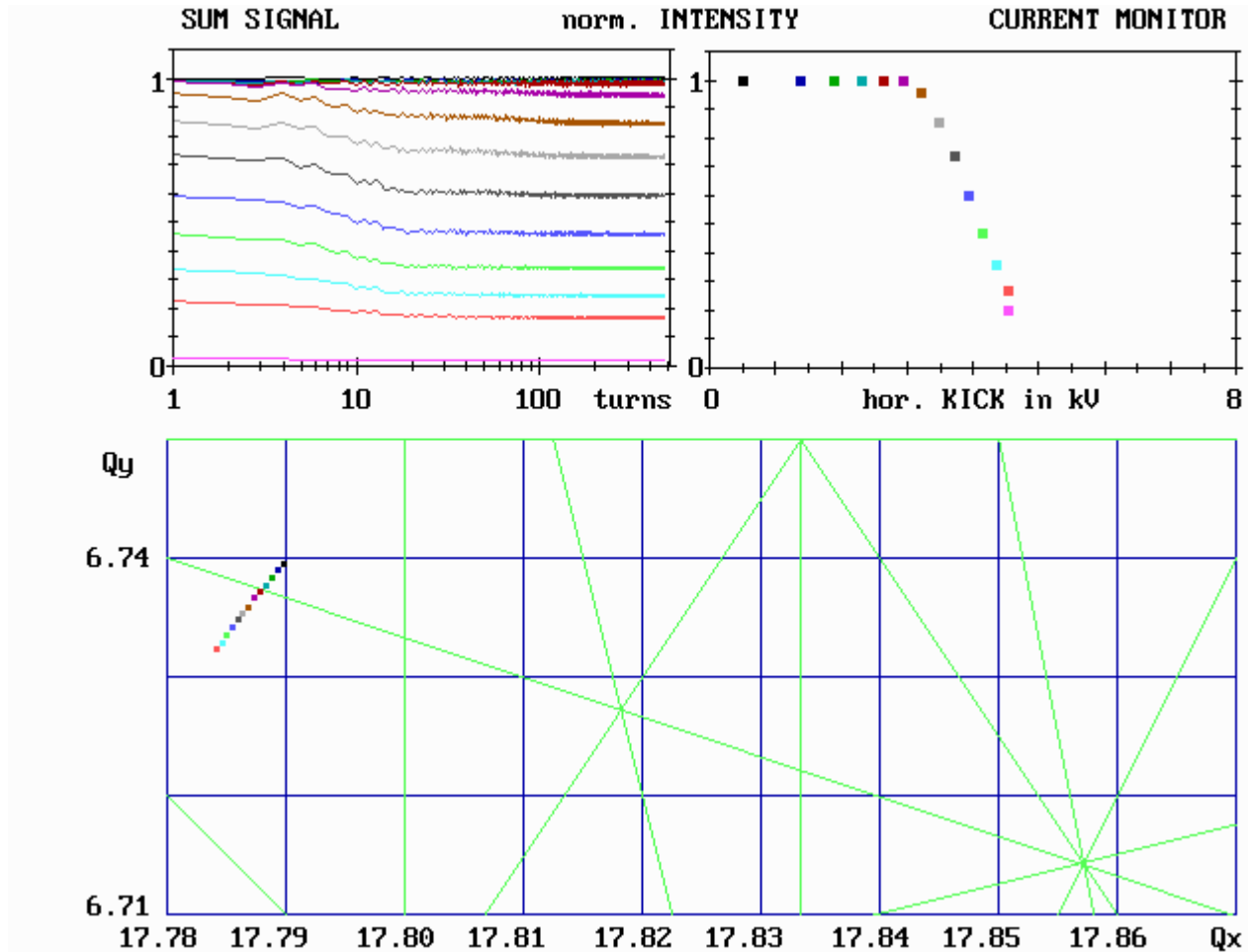




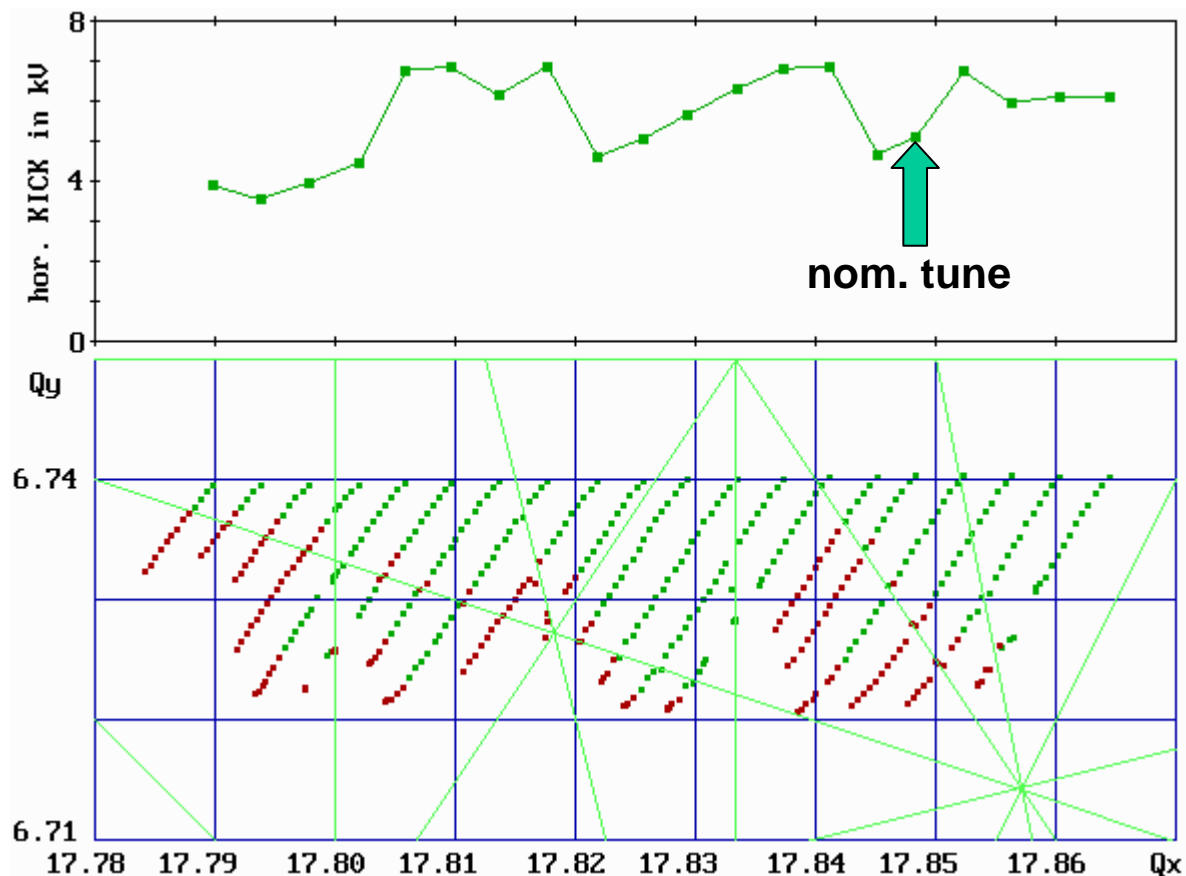






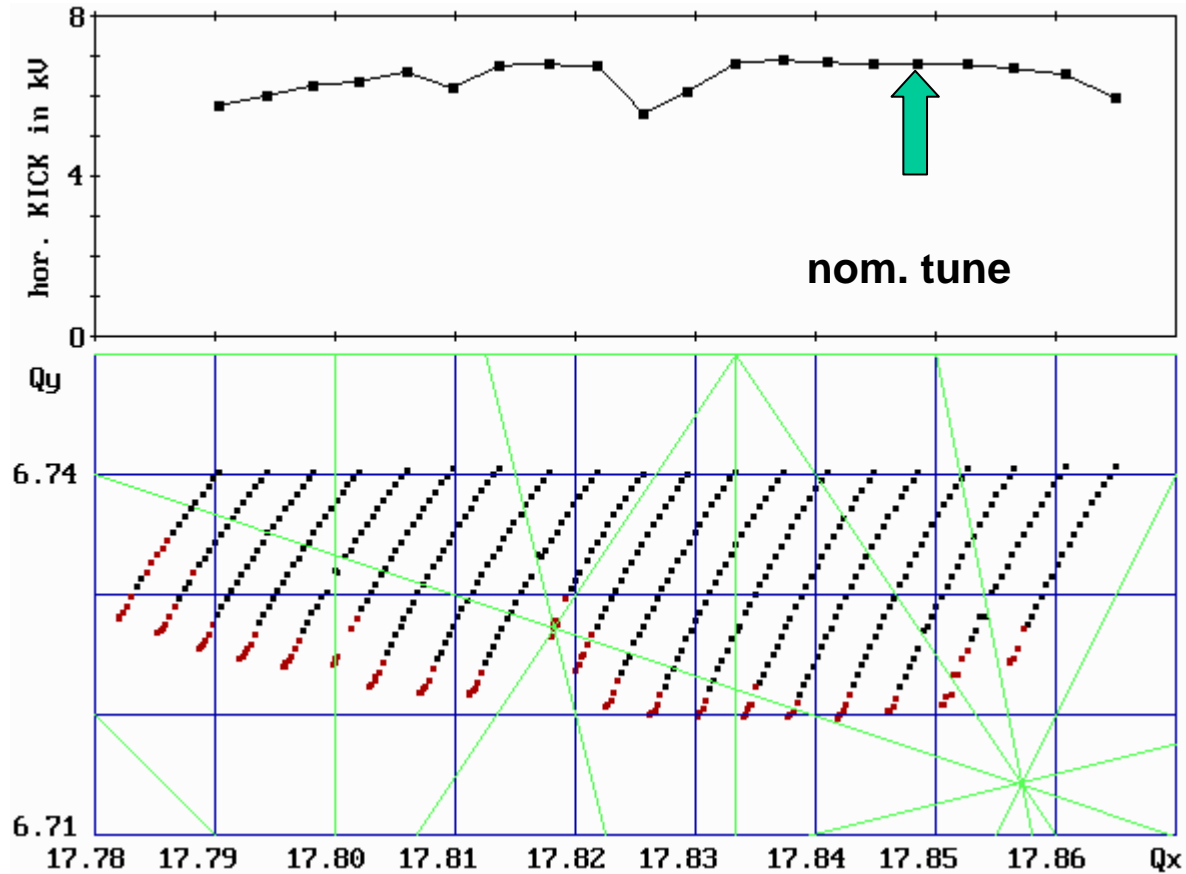


U125ID2R – gap=15.7 mm

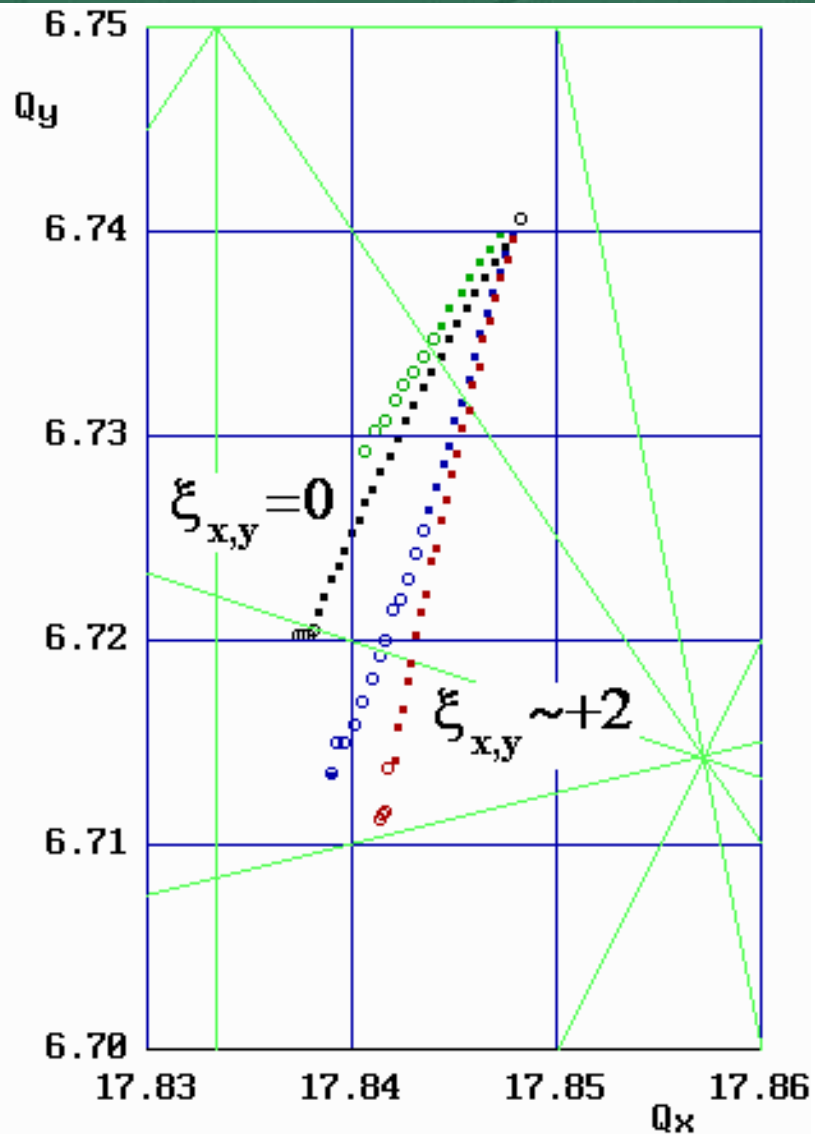
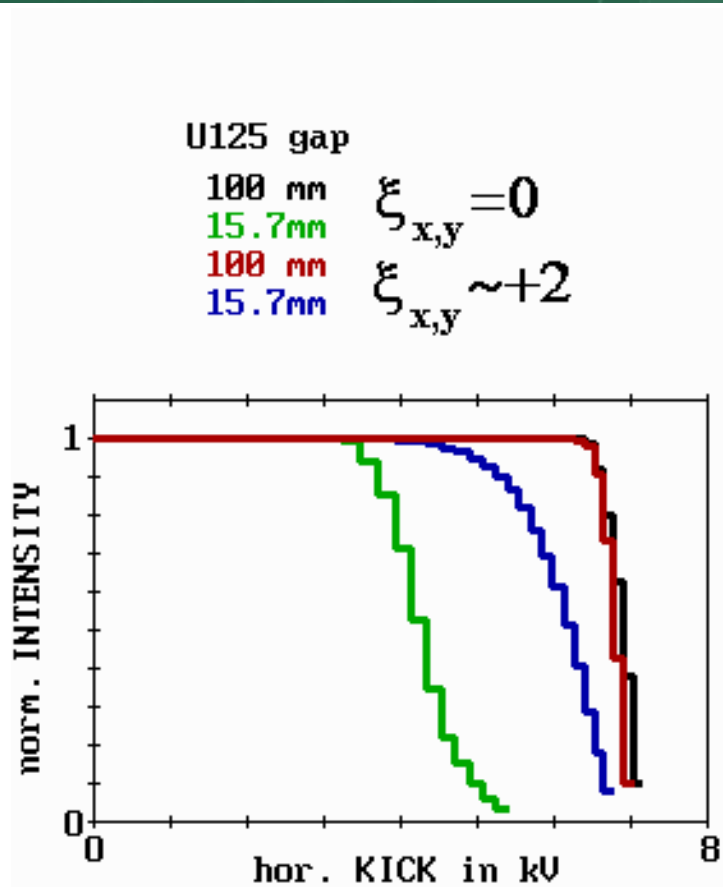


red dots –
beam loss >2%

$3Q_x + 2Q_y$ – resonance critical at the nom. working point



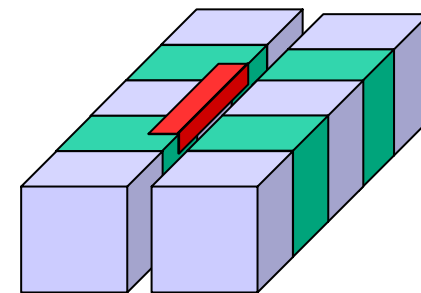
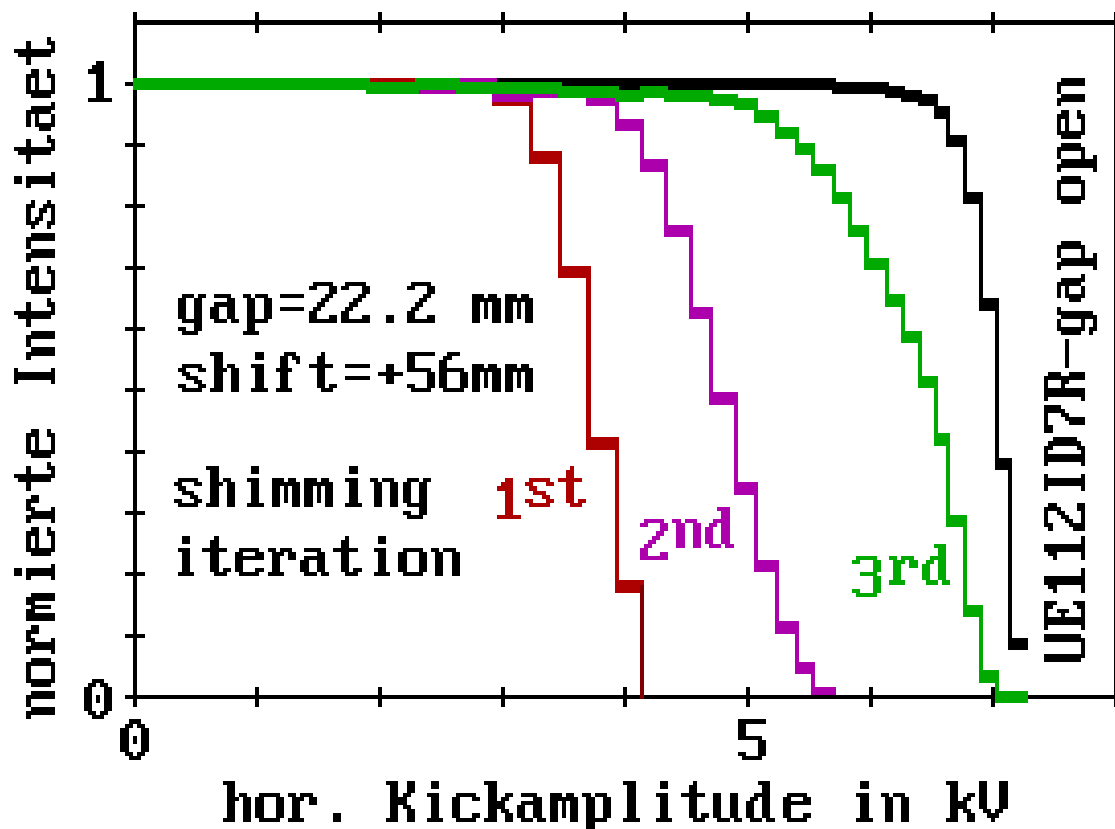
red dots –
beam loss >2%



APPLE II-type undulator: $\lambda=11.2$ cm, $B_{\max}>1$ T
 $E=1.72$ GeV, $\beta_x=14$ m

strong non-linear impact of ID
 high sensitivity of beam

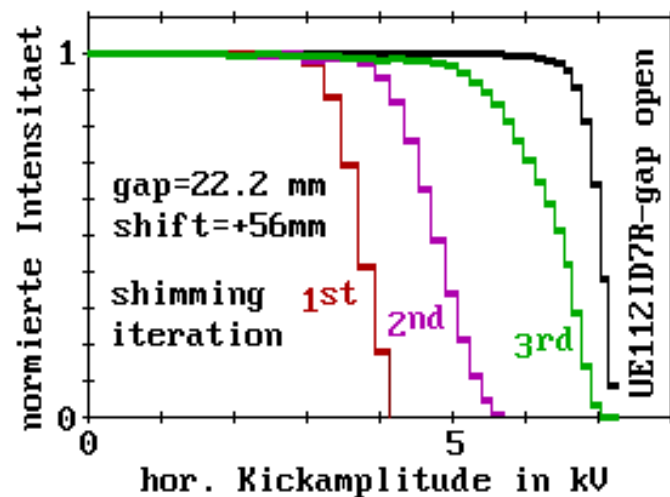
partly compensated for by L-shims – iterations required – found good shimming strategy



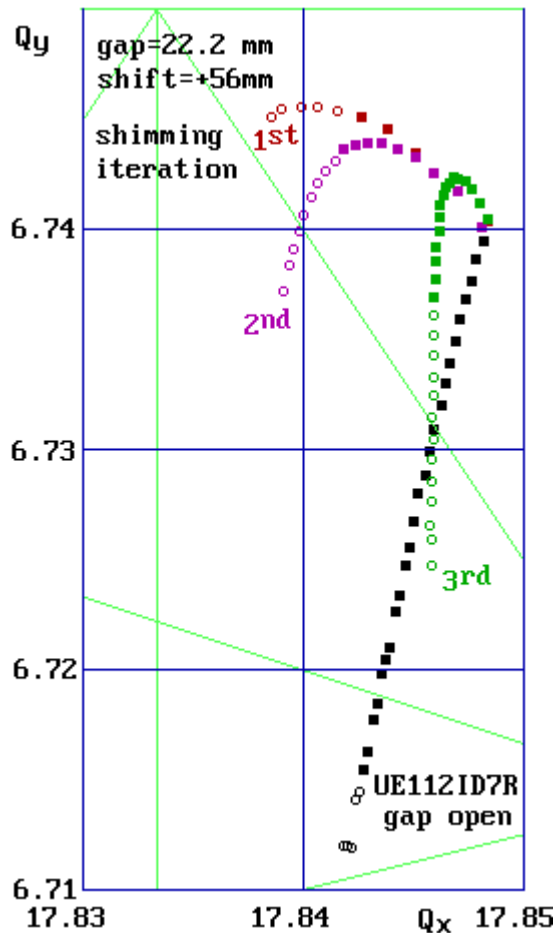
increase of horizontal aperture
 with L-shims as proposed by
 J. Chavanne, et al., EPAC 2000

passive shimming for elliptical mode

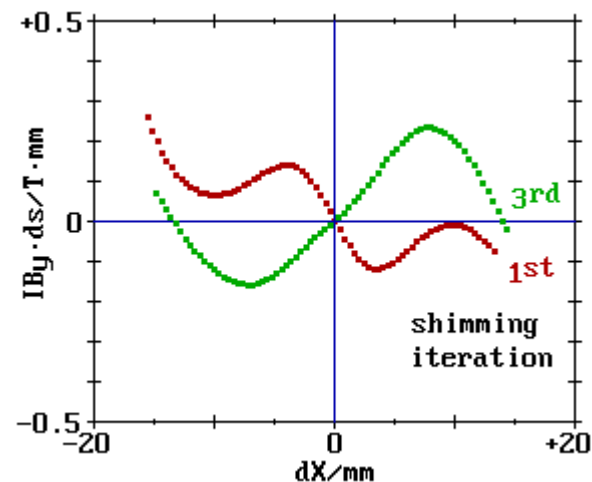
increase of the horizontal aperture by improved shimming of ID



amplitude dependent detuning for different shimming iterations – open symbols indicate beam loss of more than 2%



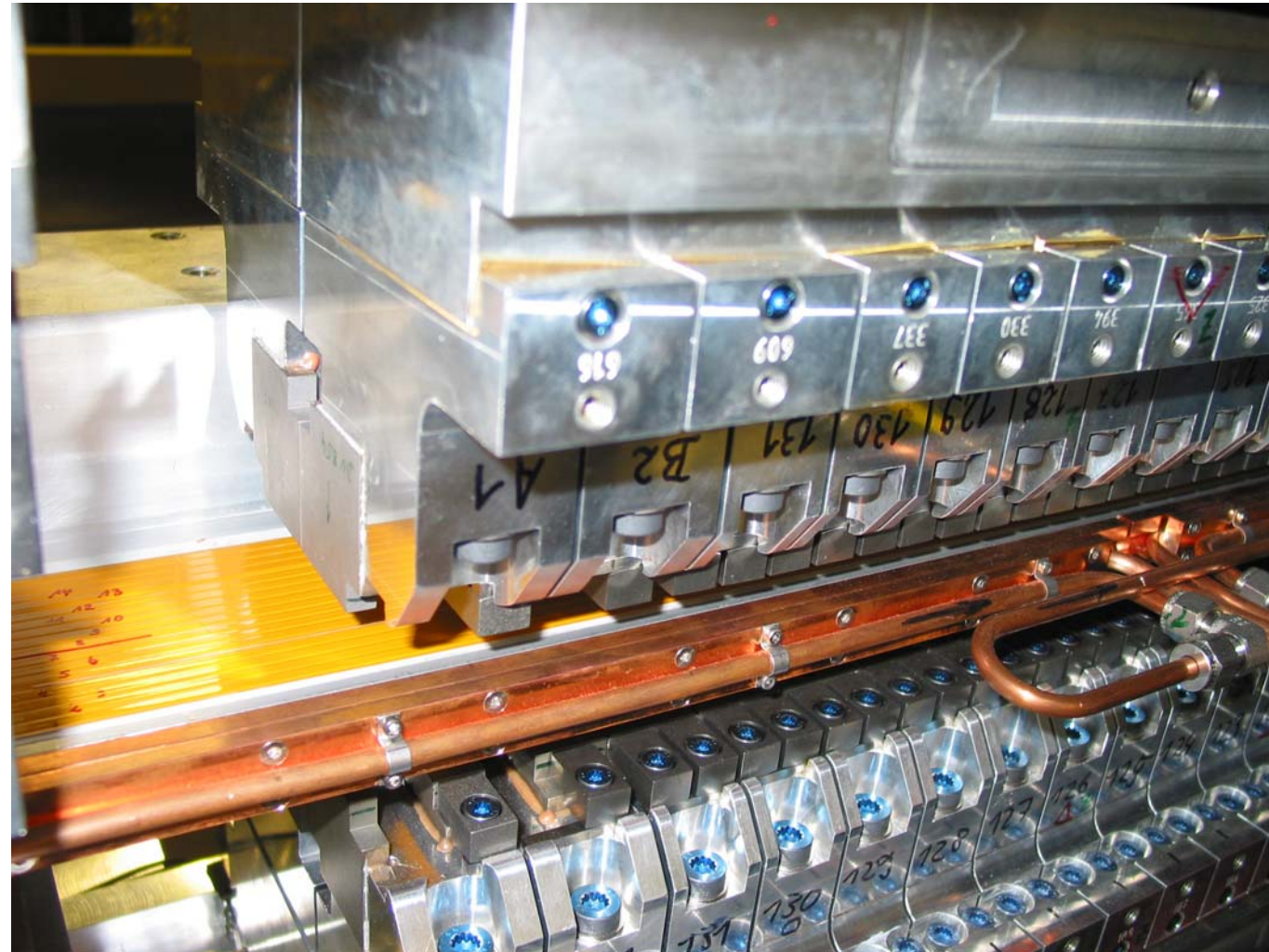
measured effective field integral



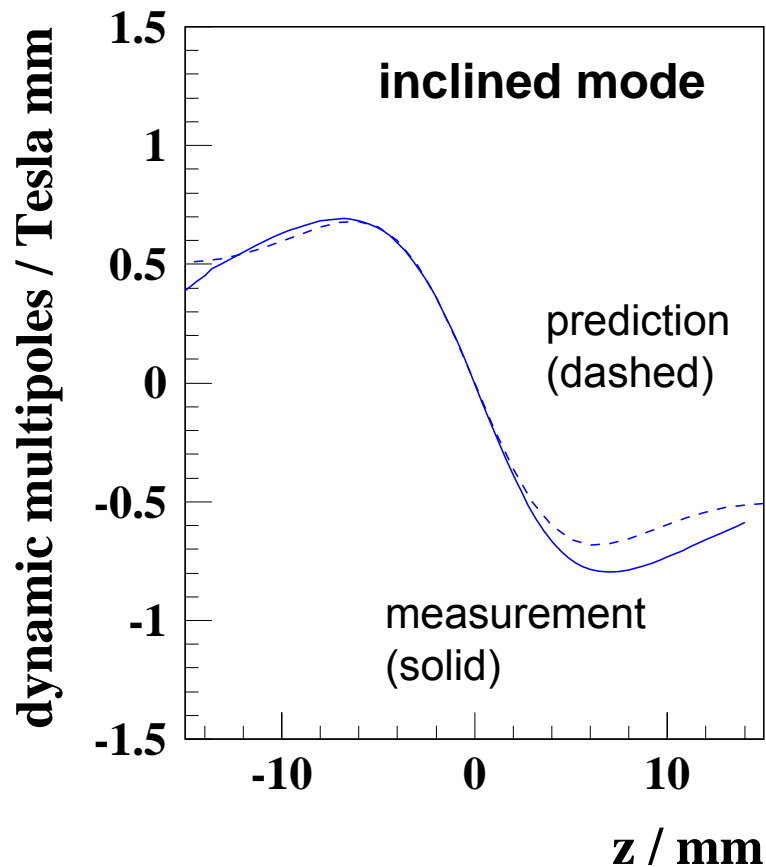
$$I_y^{eff}(x) \approx L \cdot B_0 \cdot \sin\left(\frac{x}{\lambda}\right) \approx \frac{L \cdot B_0}{\lambda} x - \frac{L \cdot B_0}{\lambda^3} \frac{x^3}{3!} + \frac{L \cdot B_0}{\lambda^5} \frac{x^5}{5!} - \dots$$

increasing λ is better than reducing B_0

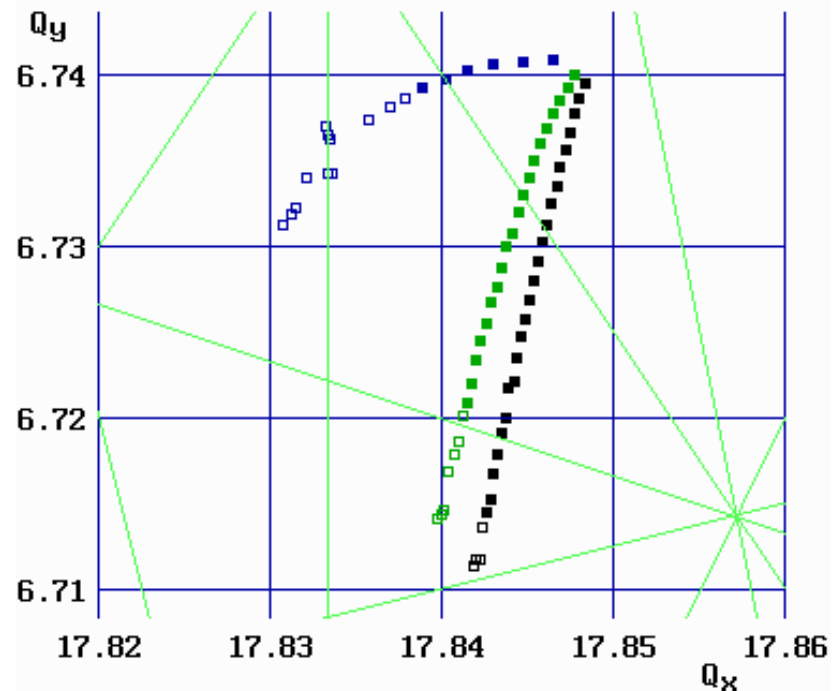
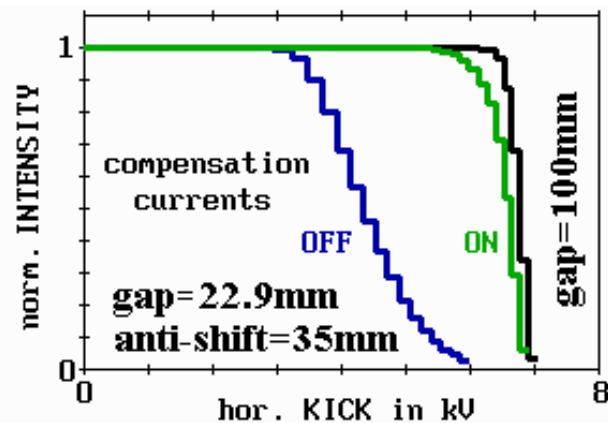
active compensation of dynamic field components in the linear/inclined mode

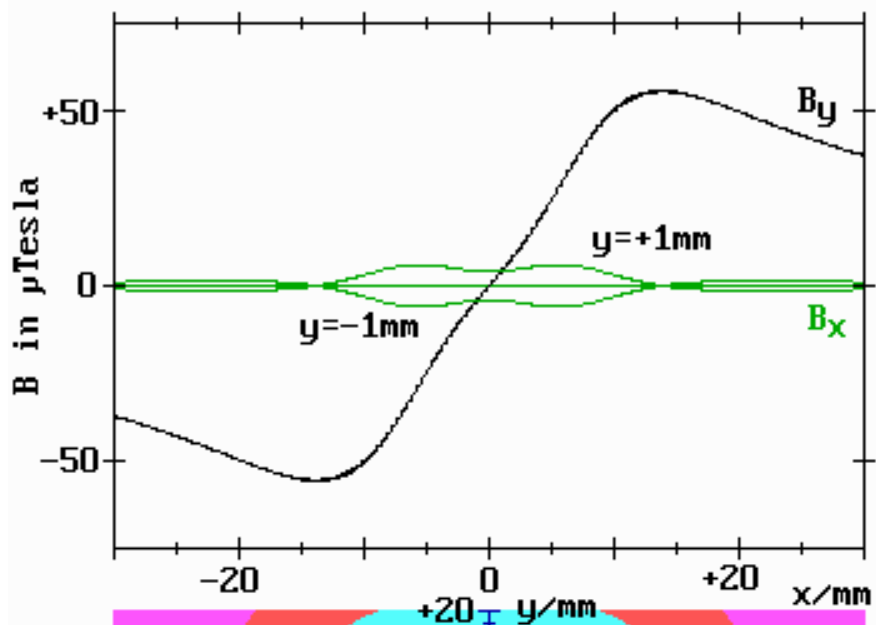


**32 flat wires along
the ID-chamber with
16 individual PS**

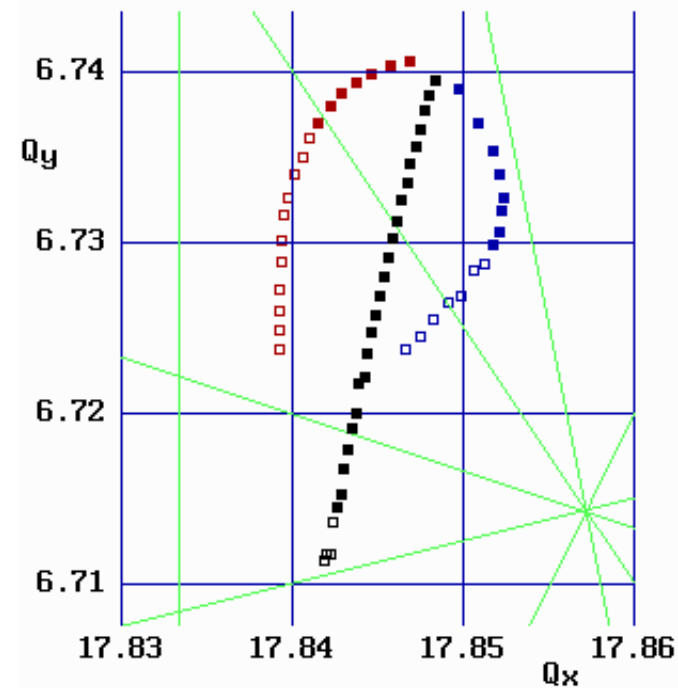
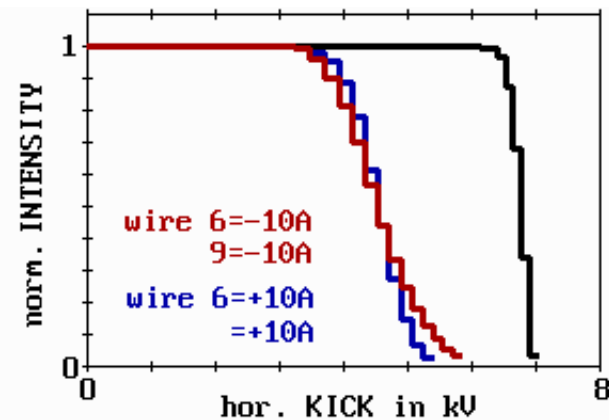
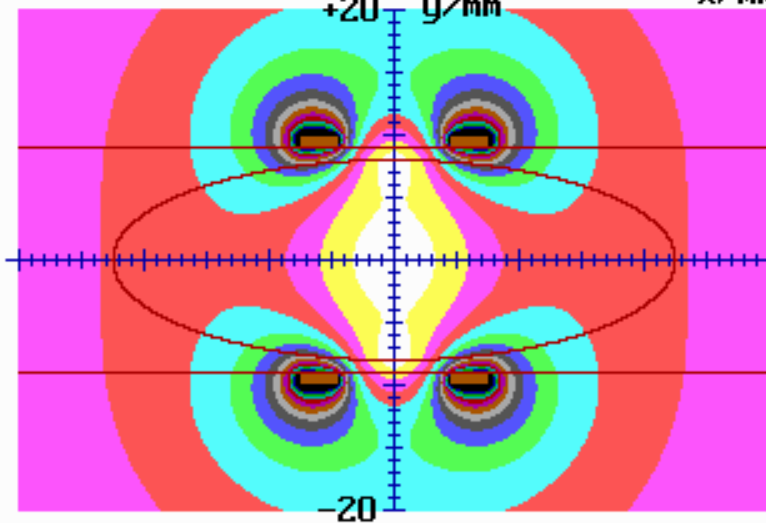


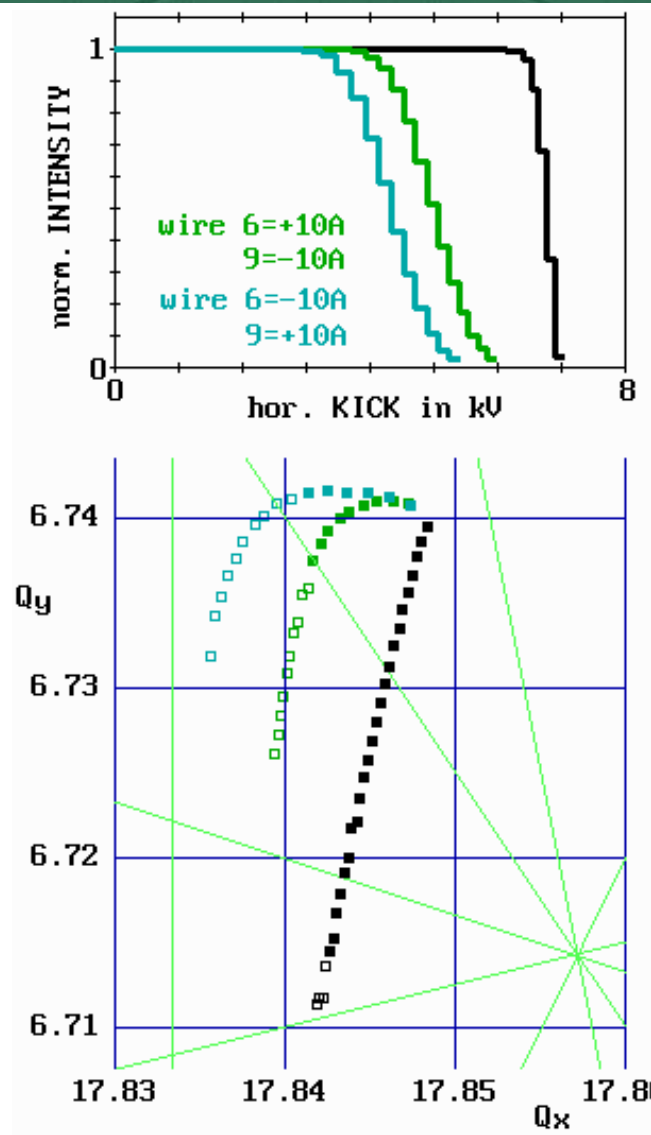
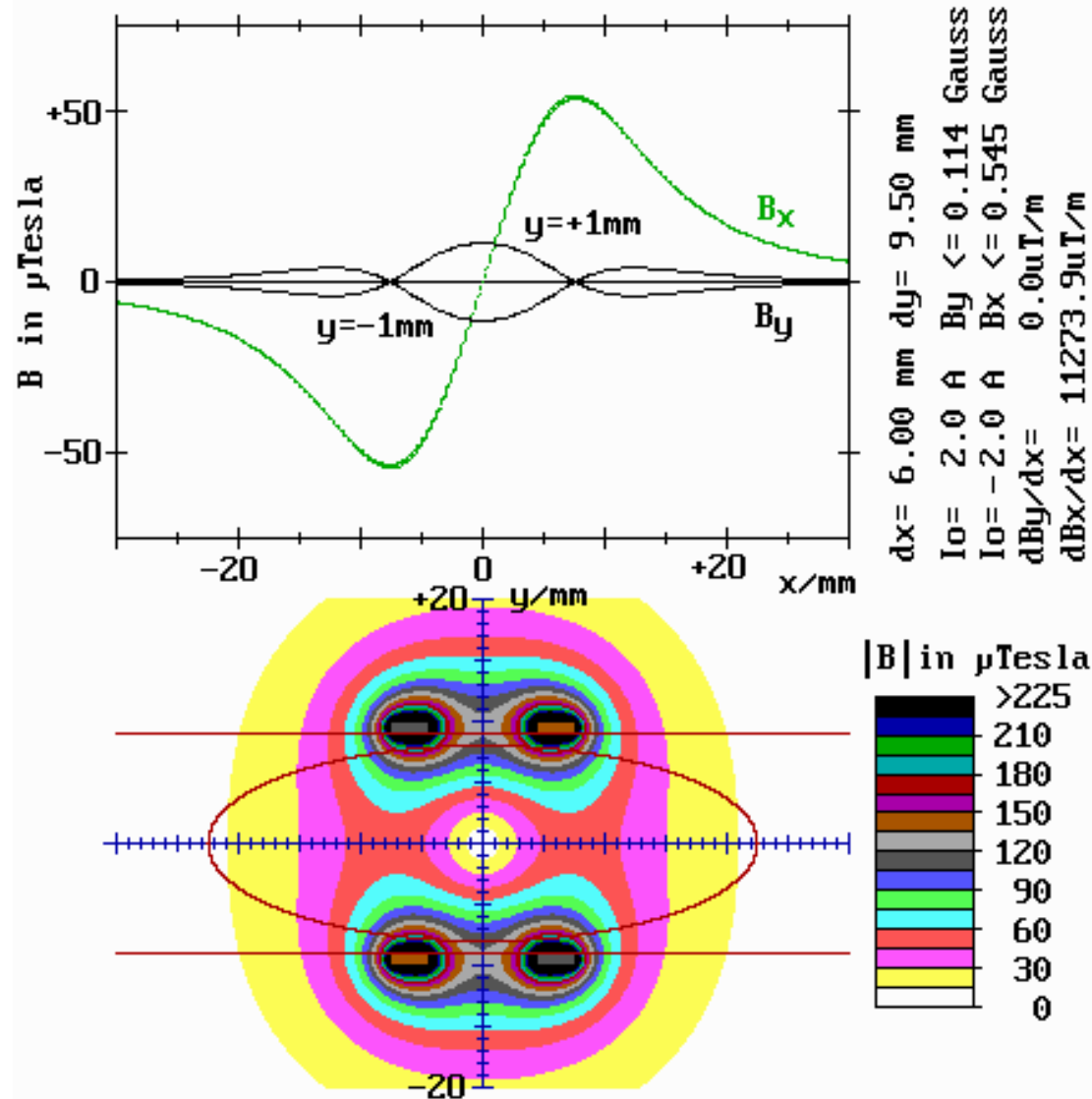
successful active compensation





$dx = 6.00 \text{ mm}$ $dy = 9.50 \text{ mm}$
 $I_0 = 1.5 \text{ A}$ $B_y \leq 0.557 \text{ Gauss}$
 $I_0 = 1.5 \text{ A}$ $B_x \leq 0.060 \text{ Gauss}$
 $dB_y/dx = 4184.7 \mu\text{T/m}$
 $dB_x/dx = -0.00 \mu\text{T/m}$





IDs can reduce the horizontal aperture injection efficiency is much smaller than 90 %

U125 – the planar undulator:

- perfect compensation of static field components has not removed these problems
- the $3Q_x + 2Q_y = 67$ -resonance should not be driven by the dynamic field components – in lowest order driven by decapoles - related to the horizontal correctors on the sextupole magnets

UE112 – APPLE II-type undulator:

- in the elliptical mode the passive shimming works and has to be improved – compensation of dynamic field components by the active system
- in the linear mode active compensation very successful – will be implemented as feedforward system

Non-linear lenses created with the 32 wires of the active compensation system:

- will be used to assess impact of non-linear fields on beam dynamics
- compare observations with theory