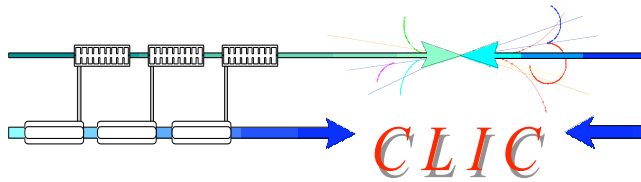


# Non-linear modeling of storage and damping rings using symplectic integrators

**Yannis PAPAPHILIPPOU**

**May 26th-28th, 2008**



# Outline

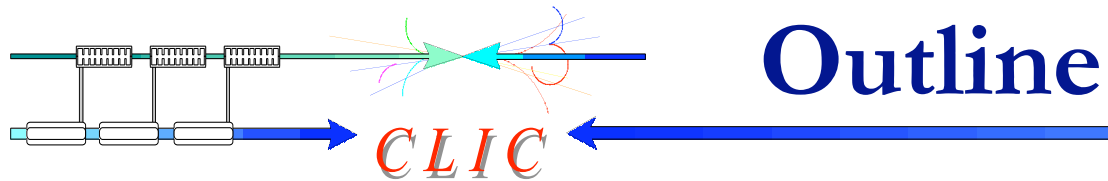


## ■ Contributors:

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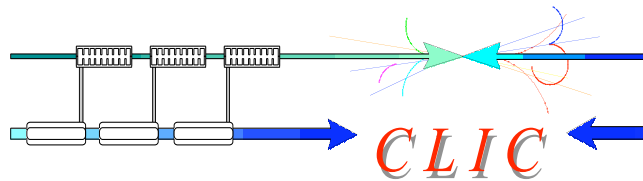
## ■ Acknowledgements

- H. Braun (CERN), L. Nadolski (Soleil), P. Robutel (IMCEE)



# Outline

- Symplectic integration
  - The SABA2 integrator
  - Application to the ESRF storage ring ideal lattice
- Compact Linear Collider (CLIC) damping rings
  - Design challenges
  - Sextupole scheme
  - Tune scans
  - Wiggler effect
  - Effect of radiation damping



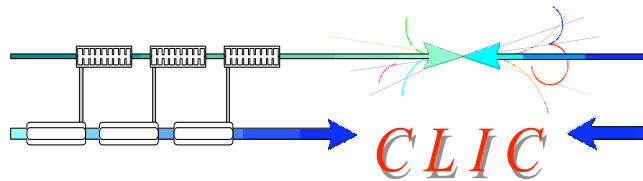
# Symplectic integration



Laskar and Robutel *Cel. Mech Dyn Astr.* 80, 39, 2001

- Symplectic integrators with positive steps for Hamiltonian systems  $H = A + \epsilon B$  with both  $A$  and  $B$  integrable
- Consider Hamiltonian system  $H(\vec{p}, \vec{q})$ , with  $N$  degrees of freedom
- A trajectory of the system in phase space is described by  $\vec{x}(t) = (x_1(t), \dots, x_{2N}(t))$ ,  $x_i = p_i$ ,  $x_{i+N} = q_i$ ,  $i = 1, \dots, N$
- Hamilton's equations of motion take the form
 
$$\frac{d\vec{x}}{dt} = \{H, \vec{x}\} = L_H \vec{x},$$
 with the usual Poisson brackets  $\{f, g\} = \sum_{i=1}^N \left( \frac{\partial f}{\partial p_i} \frac{\partial g}{\partial q_i} - \frac{\partial f}{\partial q_i} \frac{\partial g}{\partial p_i} \right)$ .
- The solution is formally written as

$$\vec{x}(t) = \sum_{n \geq 0} \frac{t^n}{n!} L_H^n \vec{x}(0) = e^{tL_H} \vec{x}(0).$$



# SABA<sub>2</sub> integrator



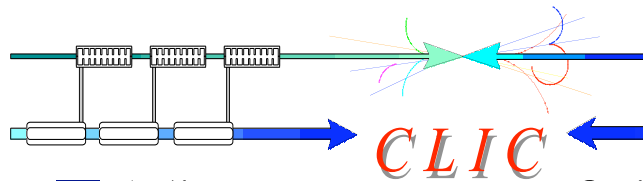
- A symplectic integrator of order  $n$  from  $t$  to  $t + \tau$  consists of approximating the operator  $e^{\tau L_H} = e^{\tau(L_A + L_{\epsilon B})}$  by products of  $e^{c_i \tau L_A}$  and  $e^{d_i \tau L_{\epsilon B}}$ ,  $i = 1, \dots, n$  which integrate exactly  $A$  and  $B$  over the time-spans  $c_i \tau$  and  $d_i \tau$
- The constants  $c_i$  and  $d_i$  are chosen for reducing the error

- The SABA<sub>2</sub> integrator is written as

$$\text{SABA}_2 = e^{c_1 \tau L_A} e^{d_1 \tau L_{\epsilon B}} e^{c_2 \tau L_A} e^{d_1 \tau L_{\epsilon B}} e^{c_1 \tau L_A},$$

with  $c_1 = \frac{1}{2} \left( 1 - \frac{1}{\sqrt{3}} \right)$ ,  $c_2 = \frac{1}{\sqrt{3}}$ ,  $d_1 = \frac{1}{2}$ .

- When  $\{\{A, B\}, B\}$  is integrable, e.g. when  $A$  is quadratic in momenta and  $B$  depends only in positions, the accuracy of the integrator is improved by two small negative steps
- $$\text{SABA}_2 C = e^{-\tau^3 \epsilon^2 \frac{c}{2} L_{\{\{A, B\}, B\}}} (\text{SABA}_2) e^{-\tau^3 \epsilon^2 \frac{c}{2} L_{\{\{A, B\}, B\}}}$$
- with  $c = (2 - \sqrt{3})/24$

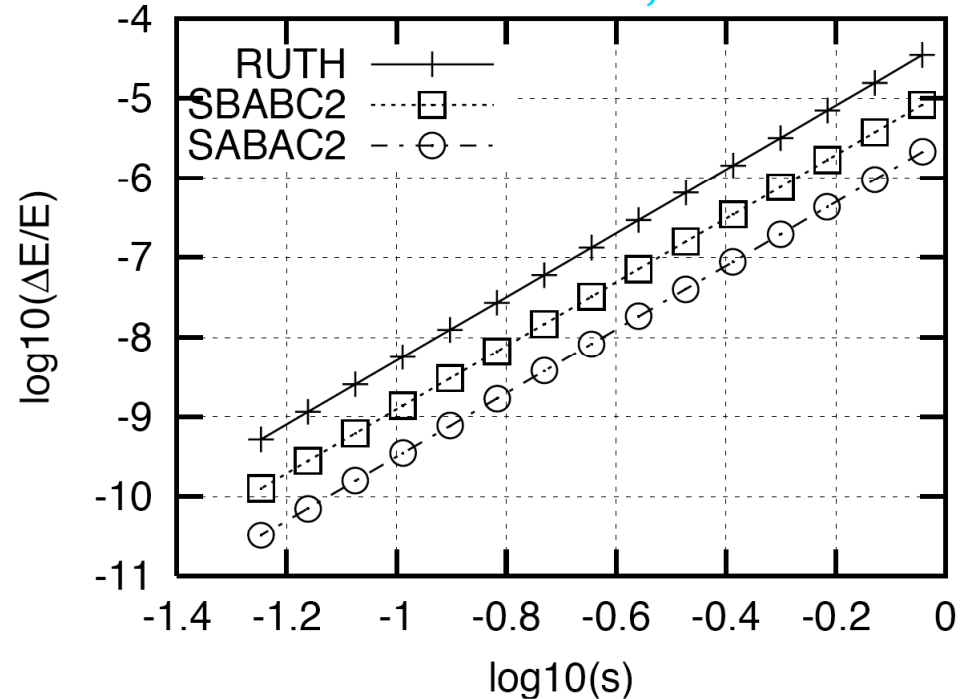


# Performance of SABA<sub>2</sub>



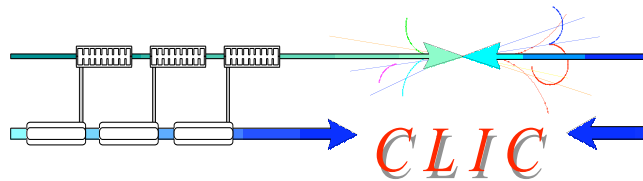
- The accuracy of the SABA<sub>2</sub>C was proved an order of magnitude more precise than the Forest-Ruth 4th order integrator

Nadolski and Laskar, EPAC 2002



- Note finally that the usual “drift-kick” scheme corresponds to the 2nd order integrator of this class

$$\text{SABA}_1 = e^{\frac{\tau}{2} L_A} e^{\tau L_{\epsilon B}} e^{\frac{\tau}{2} L_A},$$



# SABA<sub>2</sub>C for accelerators



- The accelerator Hamiltonian in the small angle, “hard-edge” approximation is written as  $H(x, y, l, p_x, p_y, \delta; s) = H_0 + V$ ,

with the unperturbed part  $H_0 = (1 + h x) \frac{p_x^2 + p_y^2}{2(1 + \delta)}$ ,

and the perturbation  $V(x, y) = \sum_{n \geq 1} \sum_{j=0}^n a_{n,j} x^j y^{n-j}$

- The unperturbed part of the Hamiltonian can be integrated

$$e^{sL_A} : \begin{cases} x^f &= \frac{1}{h} \left\{ (1 + hx^i) \left( \cos \phi + \frac{p_x^i}{p_y^i} \sin \phi \right)^2 - 1 \right\} \\ y^f &= y^i + \frac{1 + hx^i}{h} \left\{ \frac{p_x^{i2} + p_y^{i2}}{p_y^{i2}} \phi + \frac{p_y^{i2} - p_x^{i2}}{2p_y^{i2}} \sin(2\phi) + 2 \frac{p_x^i}{p_y^i} \sin^2 \phi \right\} \\ p_x^f &= p_y^i \frac{p_x^i - p_y^i \tan \phi}{p_y^i + p_x^i \tan \phi} \\ p_y^f &= p_y^i \end{cases} \quad \text{with } \phi = \frac{p_y^i h s}{2(1 + \delta)}$$

- The perturbation part of the Hamiltonian can be integrated

$$e^{sL_B} : \begin{cases} x^f = x^i & , & p_x^f = p_x^i - \left. \frac{\partial V}{\partial x} \right|_i s \\ y^f = y^i & , & p_y^f = p_y^i - \left. \frac{\partial V}{\partial y} \right|_i s \end{cases} \text{ with } \begin{cases} \left. \frac{\partial V}{\partial x} \right|_i = \sum_{n \geq 1} \sum_{j=1}^n j a_{n,j} (x^i)^{j-1} (y^i)^{n-j} \\ \left. \frac{\partial V}{\partial y} \right|_i = \sum_{n \geq 1} \sum_{j=0}^n (n-j) a_{n,j} (x^i)^j (y^i)^{n-j-1} \end{cases}$$

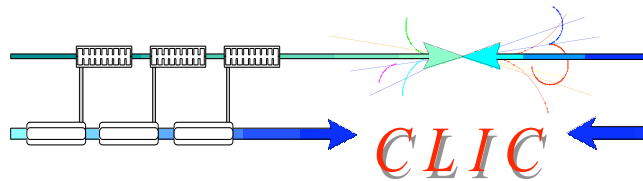
- The corrector is expressed as

$$C = \{\{A, B\}, B\} = \frac{1 + hx}{1 + \delta} \left[ \left( \frac{\partial V}{\partial x} \right)^2 + \left( \frac{\partial V}{\partial y} \right)^2 \right],$$

and the operator for the corrector is written as

$$e^{sL_C} : \begin{cases} x^f = x^i \\ y^f = y^i \\ p_x^f = p_x^i - \frac{1}{1 + \delta} \left\{ h \left[ \left. \frac{\partial V}{\partial x} \right|_i^2 + \left. \frac{\partial V}{\partial y} \right|_i^2 \right] + 2(1 + hx^i) \left[ \left. \frac{\partial V}{\partial x} \right|_i \left. \frac{\partial^2 V}{\partial x^2} \right|_i + \left. \frac{\partial V}{\partial y} \right|_i \left. \frac{\partial^2 V}{\partial x \partial y} \right|_i \right] \right\} s \\ p_y^f = p_y^i - \frac{2(1 + hx^i)}{1 + \delta} \left\{ \left. \frac{\partial V}{\partial x} \right|_i \left. \frac{\partial^2 V}{\partial x \partial y} \right|_i + \left. \frac{\partial V}{\partial y} \right|_i \left. \frac{\partial^2 V}{\partial y^2} \right|_i \right\} s \end{cases} .$$

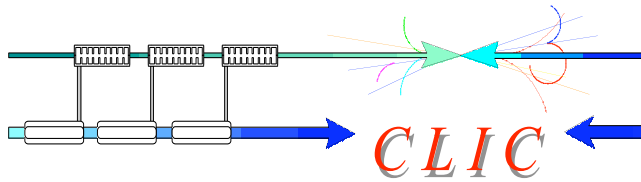




# Application to the ESRF



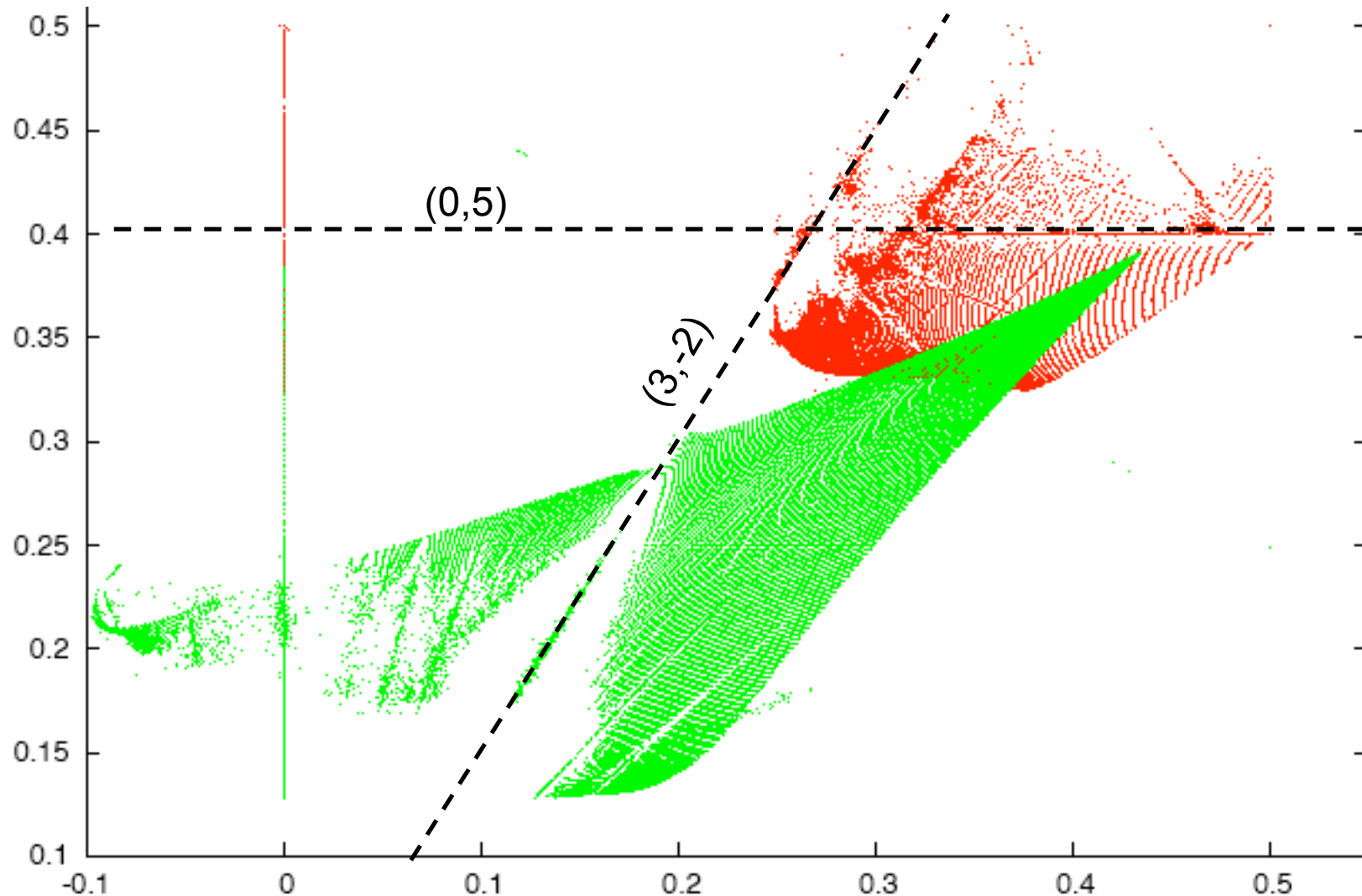
- Consider the old ESRF “ideal” lattice, i.e. perfectly symmetric (periodicity of 16) with the only non-linearity coming from the sextupoles
- Integrate the equations of motions with three different methods
  - “Drift-Kick” method by splitting the 0.4m sextupoles in a drift+kick+drift
  - Splitting the sextupoles in  $10 \times (\text{drift+kick}) + \text{drift}$
  - Using the  $\text{SABA}_2\text{C}$  symplectic integrator
- Produce frequency maps by using Laskar’s NAFF algorithm and compare



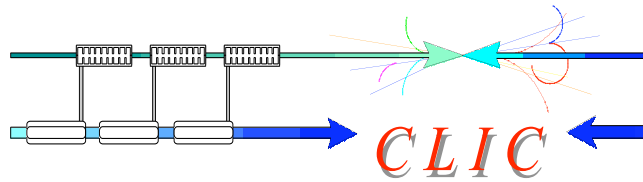
# Frequency map I



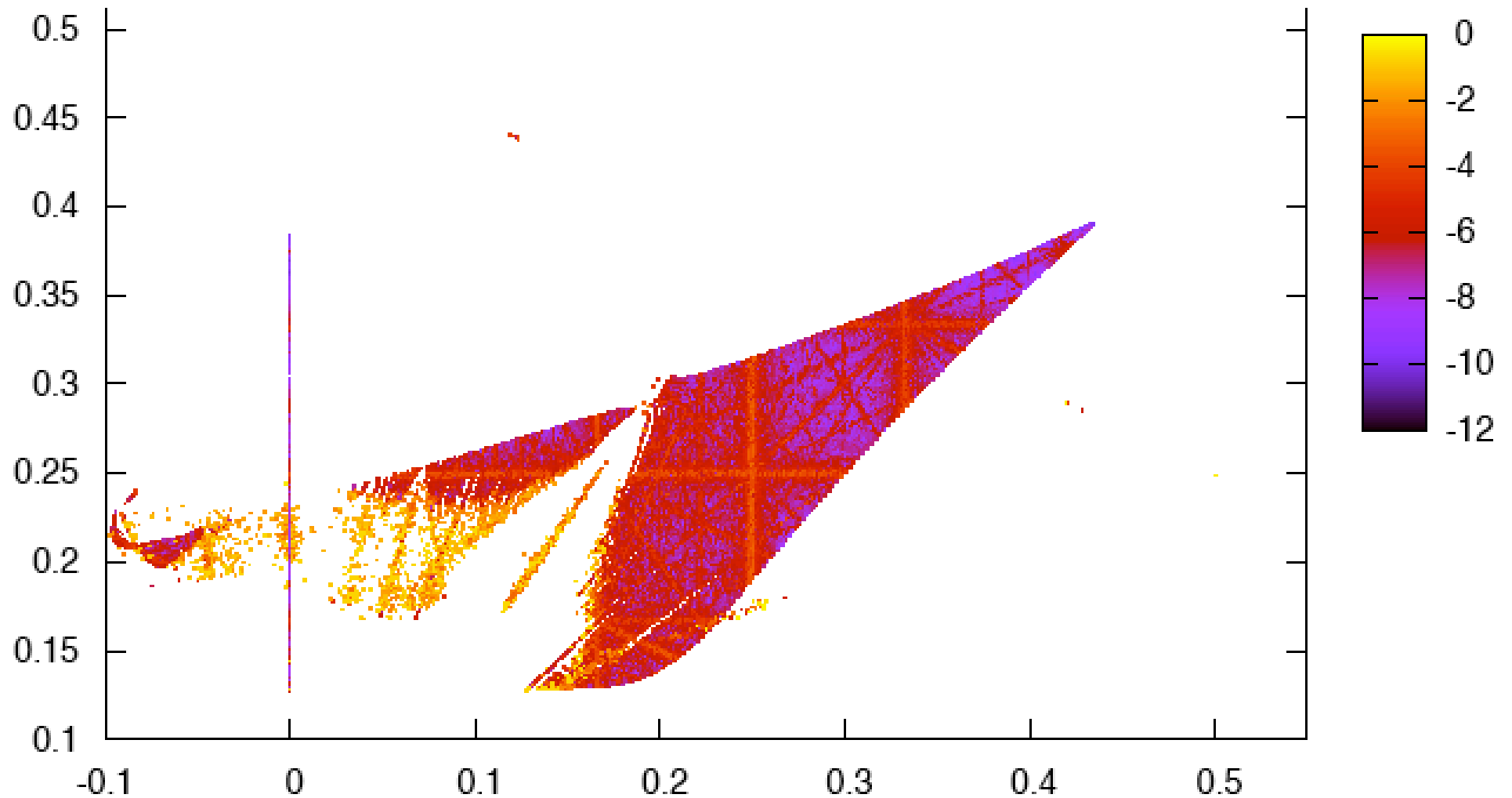
- Comparison between frequency maps produced by “drift-kick” 1 kick versus 10 kicks



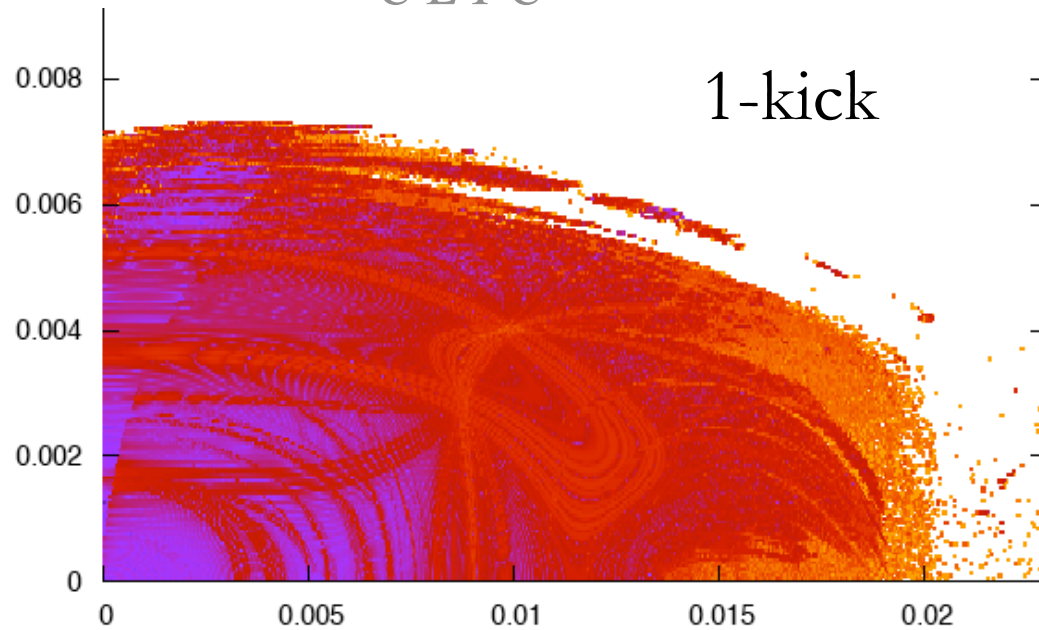
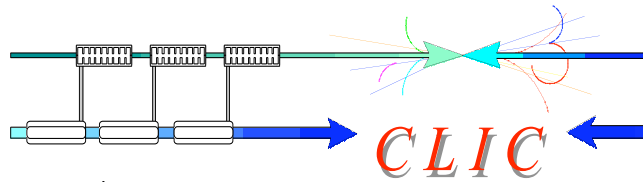
# Frequency map II



- Frequency map using the  $SABA_2C$  symplectic integrator reproduces the “10-kick” case



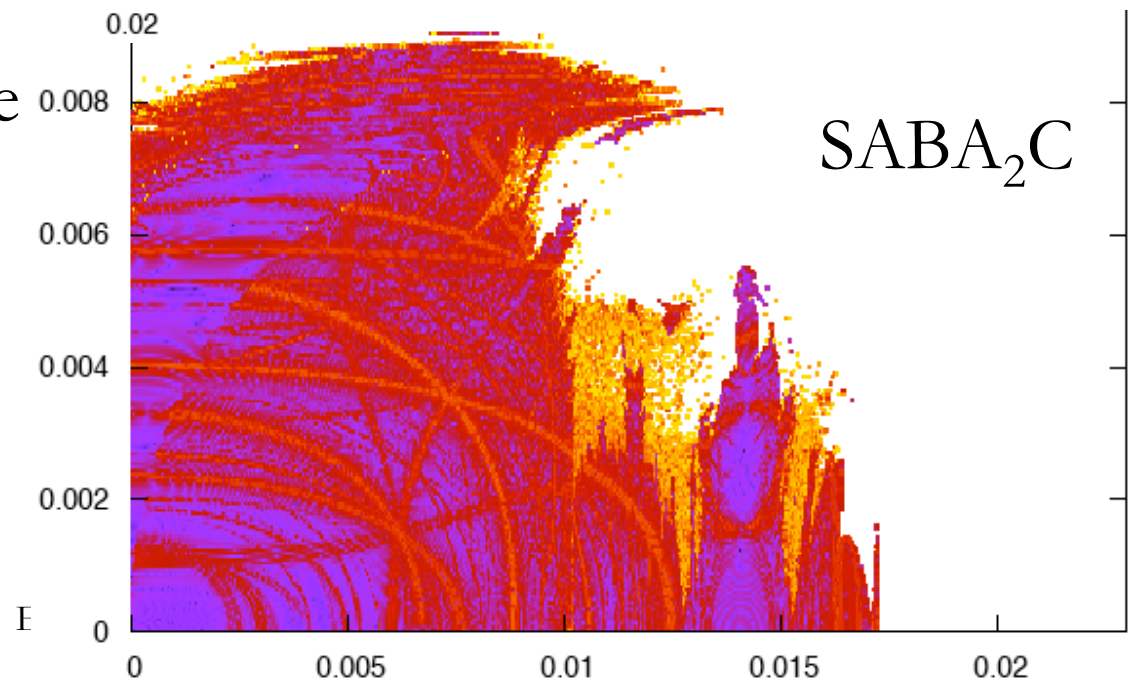
# Diffusion maps

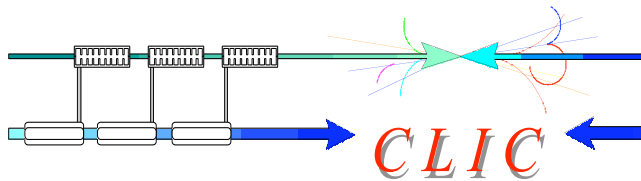


■ Colour coding following the logarithm of the diffusion vector amplitude

$$D|_{t=\tau} = \nu|_{t \in (0, \tau/2]} - \nu|_{t \in (\tau/2, \tau]}$$

- Diffusion map using the SABA<sub>2</sub>C symplectic integrator shows lower horizontal and slightly higher vertical DA than 1-kick integrator

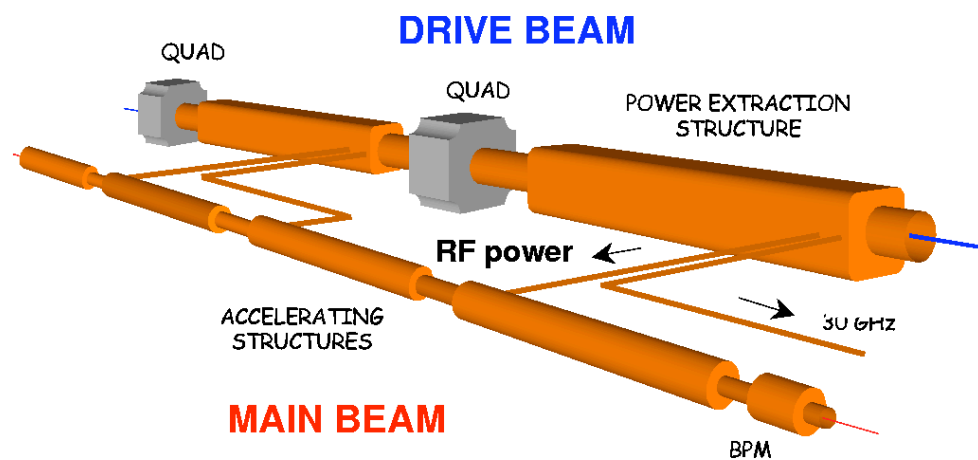
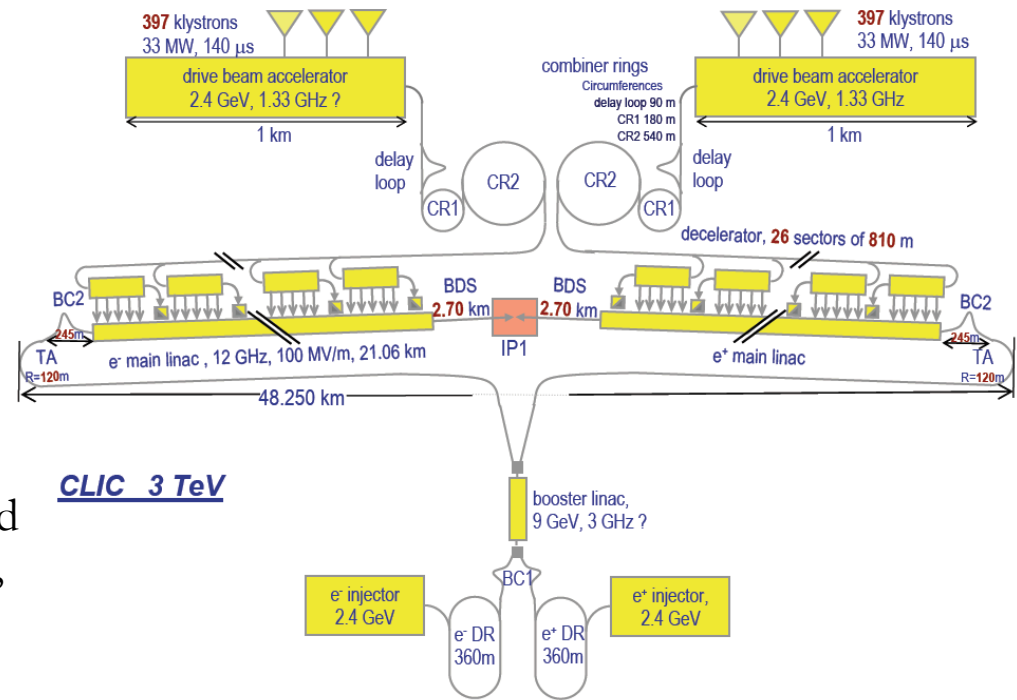




# The CLIC Project

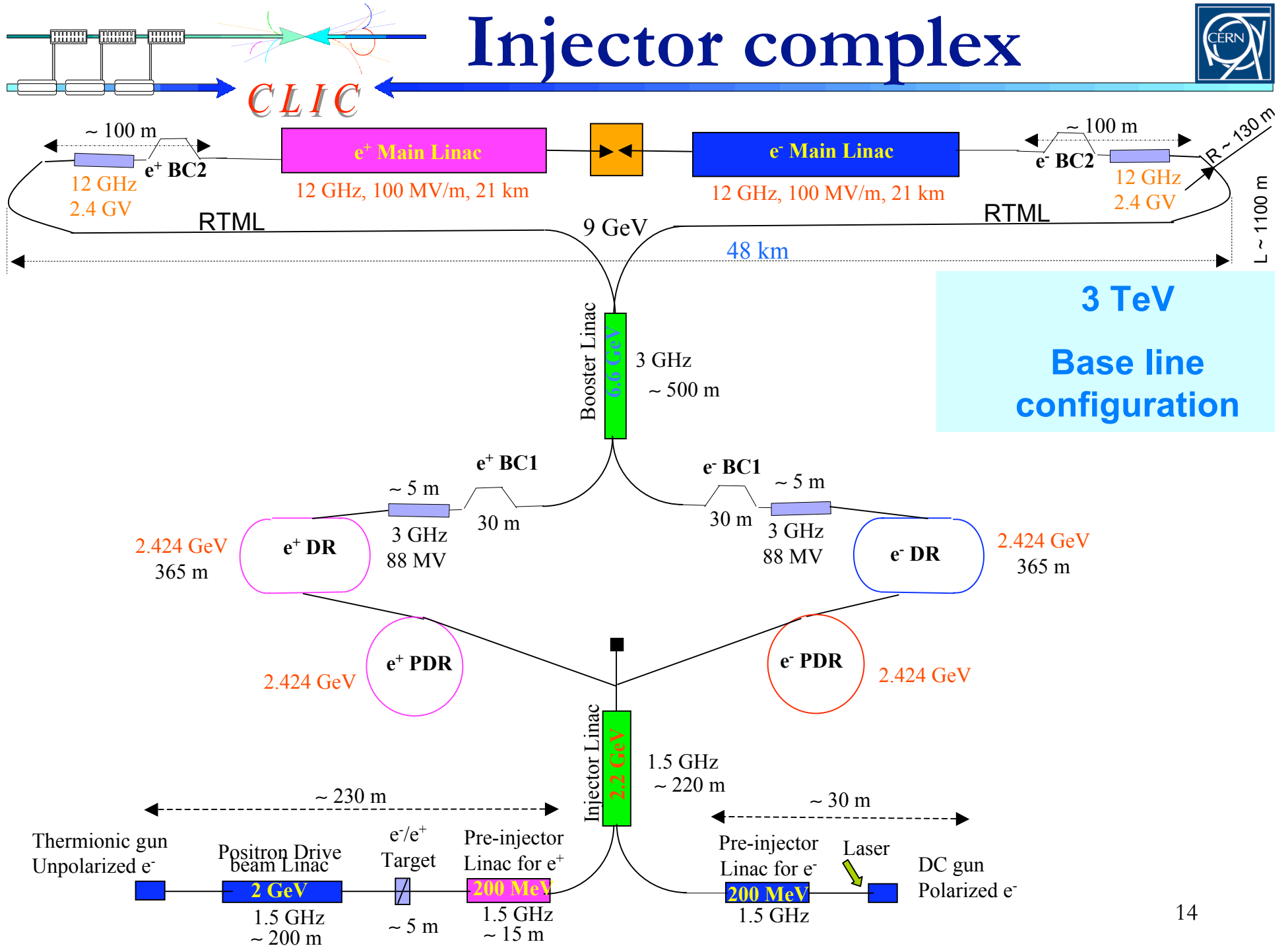


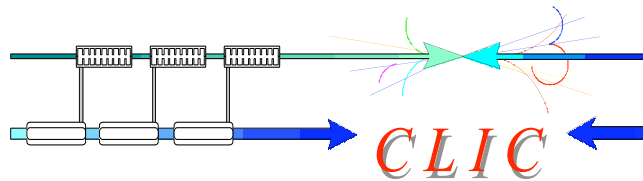
- **Compact Linear Collider** : multi-TeV e-p collider for high energy physics beyond the LHC
- Center-of-mass energy from 0.5 to **3 TeV**
- RF gradient and frequencies are **very high**
  - **100 MV/m** in room temperature accelerating structures at **12 GHz**
- **Two-beam-acceleration concept**
  - High current “**drive**” beam, decelerated in power extraction structures (**PETS**), generates RF power for main beam.
- Challenges:
  - Efficient generation of drive beam
  - PETS generating the required power
  - 12 GHz RF structures for the high gradient
  - Generation/preservation of small emittance beam
  - Focusing to nanometer beam size
  - Precise alignment of the different components





# Injector complex



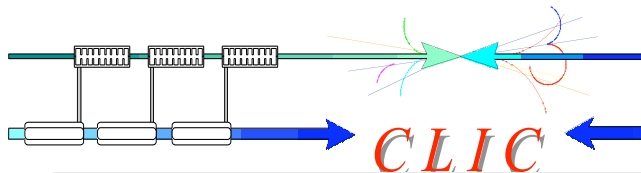


# Damping ring design goals

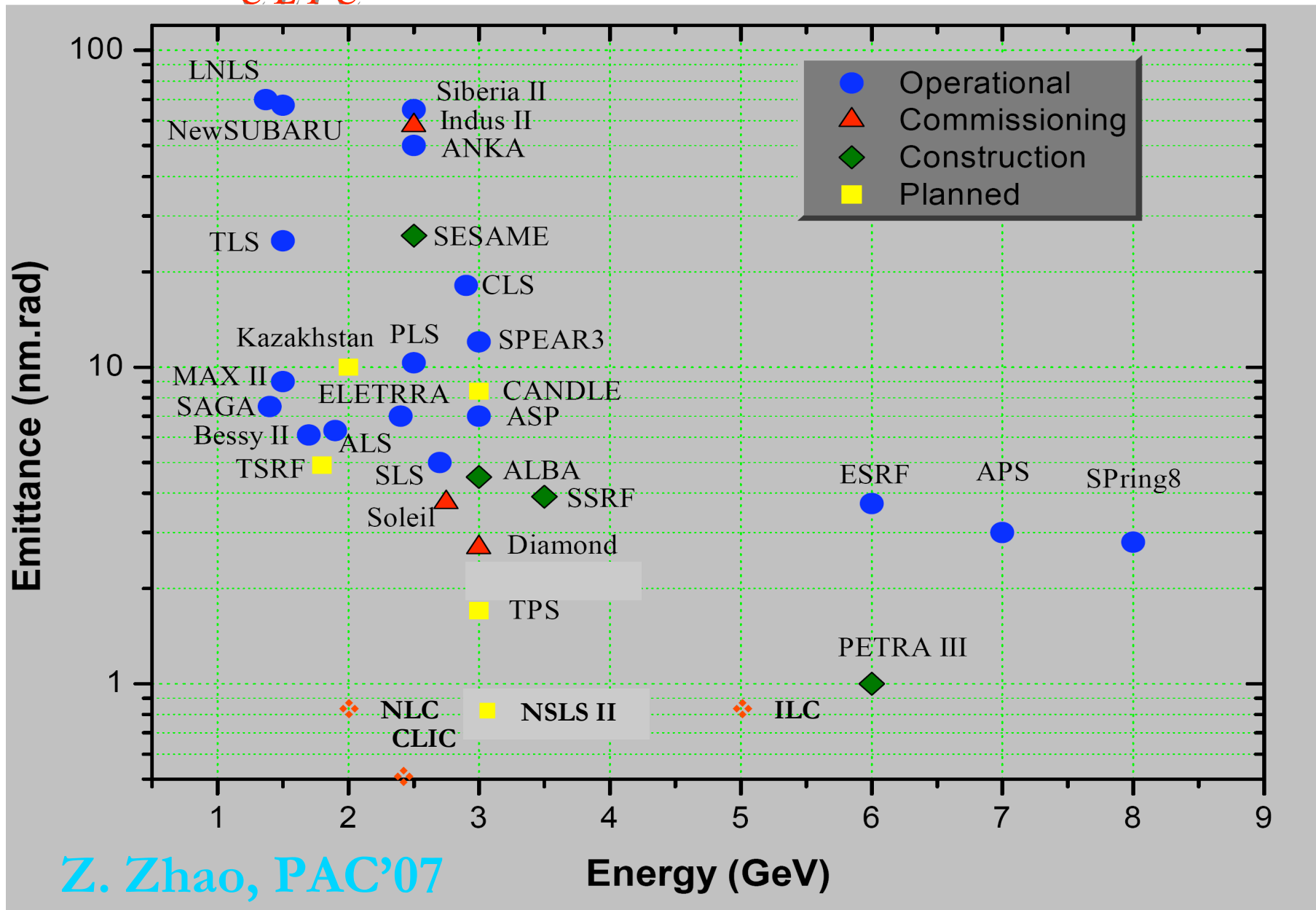


- Ultra-low emittance and high beam polarisation impossible to be produced by conventional particle source:
  - Ring to damp the beam size to desired values through synchrotron radiation
- Intra-beam scattering due to high bunch current blows-up the beam
  - Equilibrium “IBS dominated” emittance should be reached fast to match collider high repetition rate
- Other collective effects (e.g.  $e^-$ -cloud) may increase beam losses
- Starting parameter dictated by design criteria of the collider (e.g. luminosity), injected beam characteristics or compatibility with the downstream system parameters (e.g. bunch compressors)

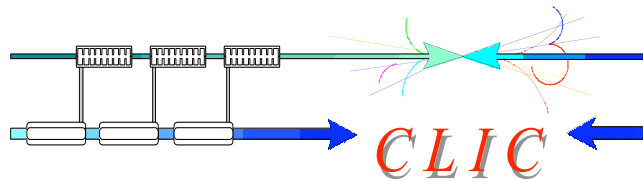
PARAMETER	CLIC
bunch population ( $10^9$ )	4.1
bunch spacing [ns]	0.5
number of bunches/train	312
number of trains	1
Repetition rate [Hz]	50
Extracted hor. normalized emittance [nm]	<680
Extracted ver. normalized emittance [nm]	< 20
Extracted long. normalized emittance [eV m]	<5000
Injected hor. normalized emittance [ $\mu\text{m}$ ]	63
Injected ver. normalized emittance [ $\mu\text{m}$ ]	1.5
Injected long. normalized emittance [keV m]	1240



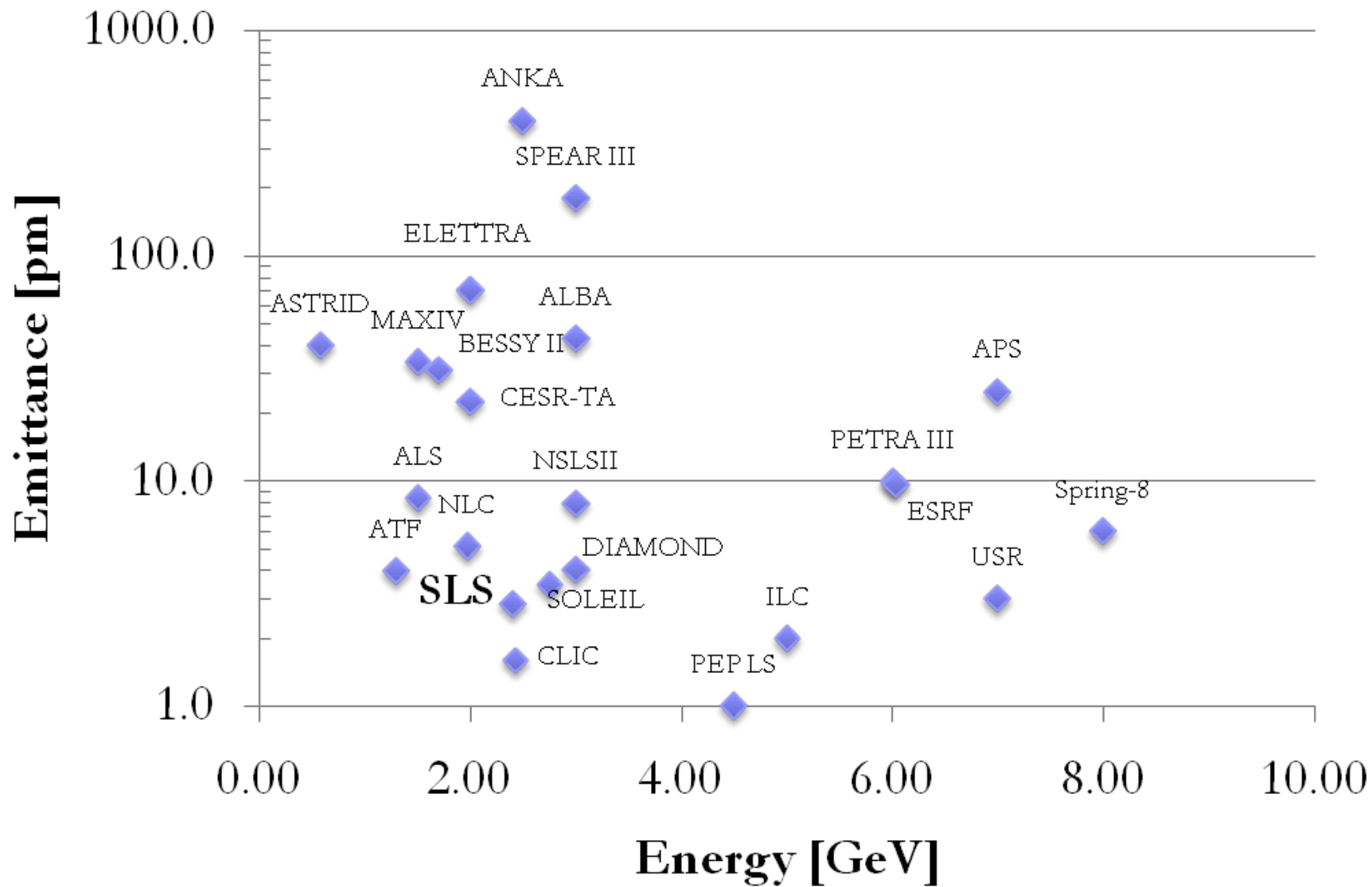
# Horizontal emittance vs. energy





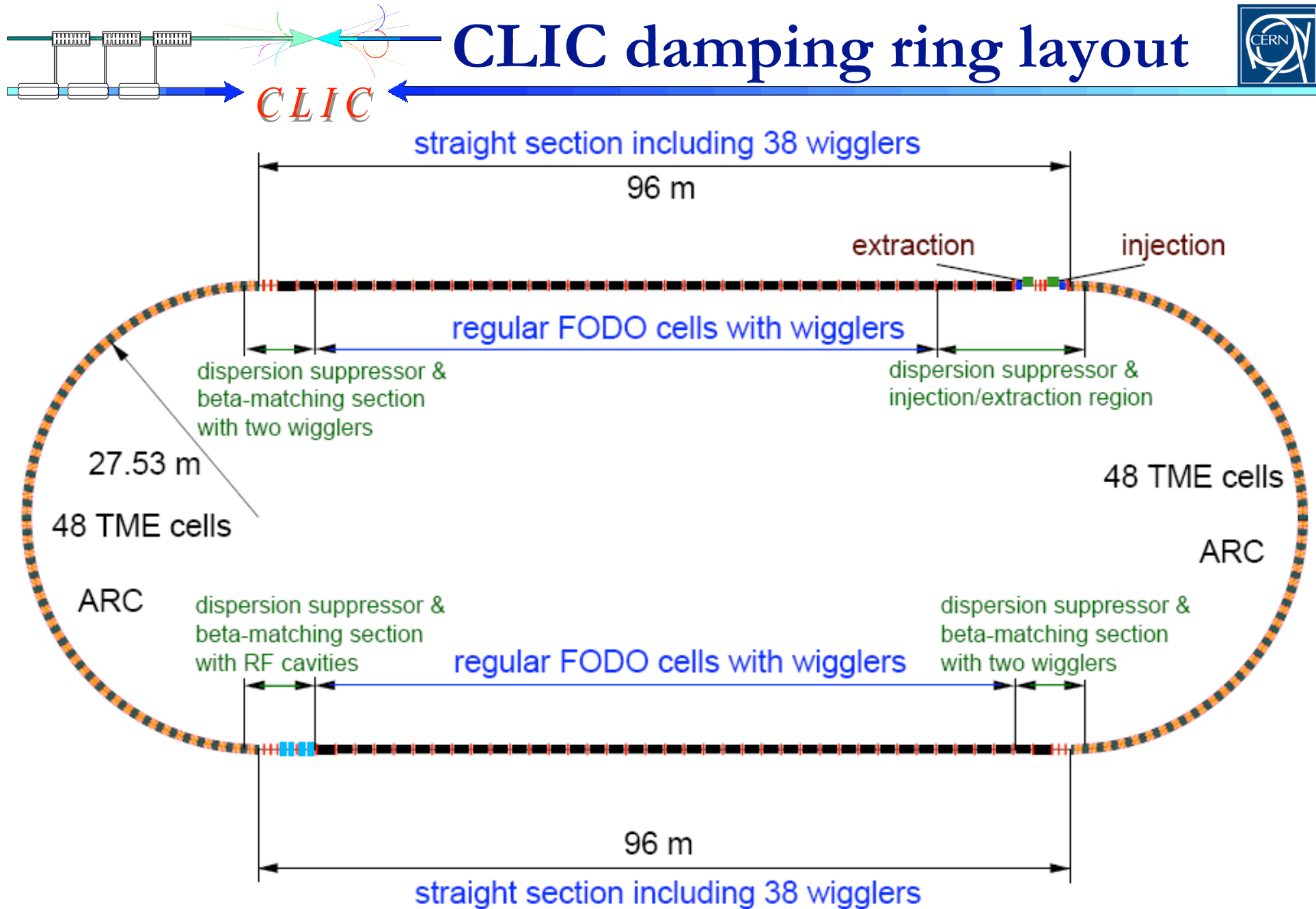


# Vertical emittance vs. energy

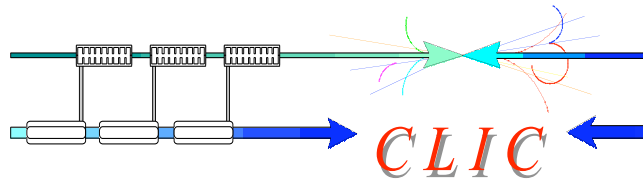




# CLIC damping ring layout

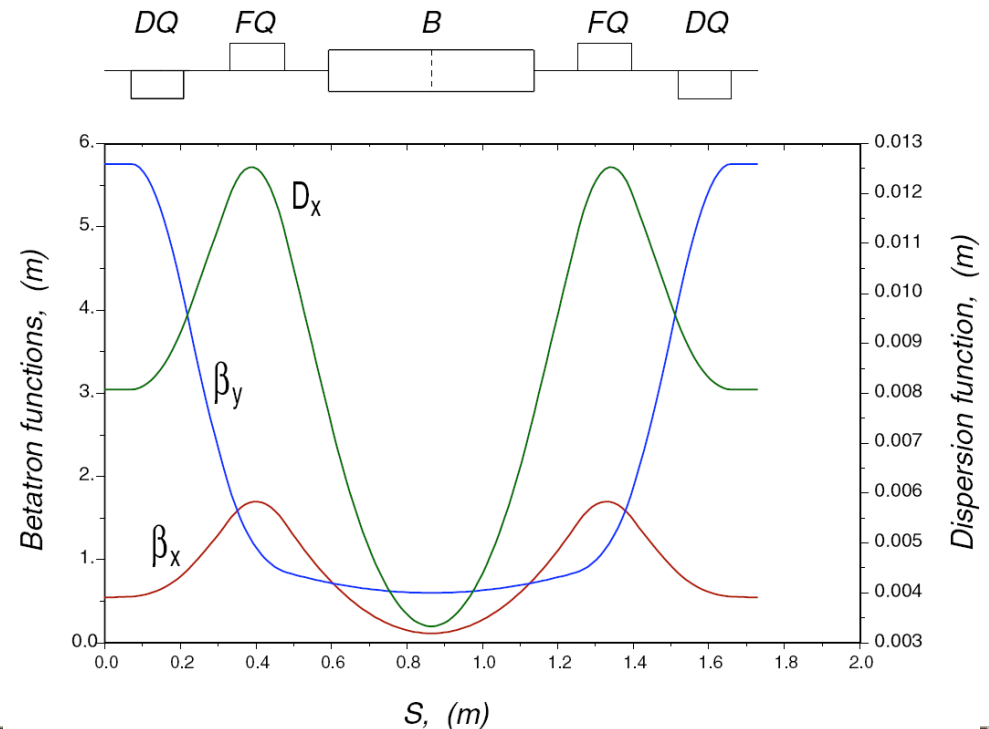


# TME arc cell

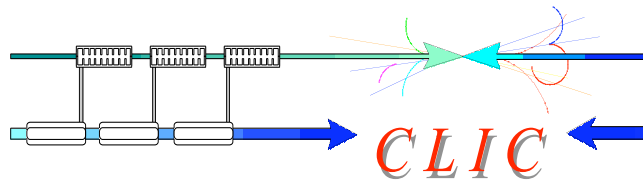


- TME cell chosen for compactness and efficient emittance minimisation over Multiple Bend Structures (or achromats) used in light sources
- Large phase advance necessary to achieve optimum equilibrium emittance
- Very low dispersion
- Strong sextupoles needed to correct chromaticity
- Impact in dynamic aperture

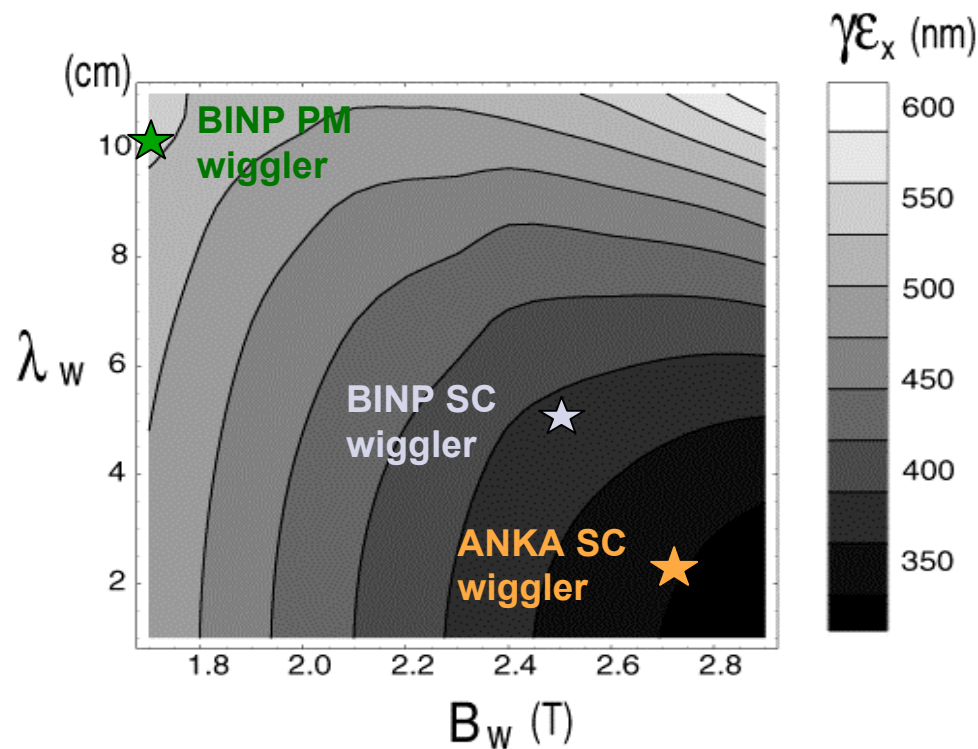
26/05/2008



Energy	2.42 GeV
Field of the bending magnet, $B_a$	0.932 T
Length of the bending magnet	0.545 m
Bending angle	$2\pi/100$
Bending radius	8.67 m
Length of the cell, $L_{TME}$	1.73 m
Horizontal phase advance, $\mu_x$	$210^\circ$
Vertical phase advance, $\mu_y$	$90^\circ$
Emittance detuning factor, $\epsilon_r$	1.8
Horizontal chromaticity, $\partial\nu_x/\partial\delta$	-0.84
Vertical chromaticity, $\partial\nu_y/\partial\delta$	-1.18
Average horizontal beta function, $\langle\beta_x\rangle$	0.847 m
Average vertical beta function, $\langle\beta_y\rangle$	2.22 m
Average horizontal dispersion, $\langle D_x\rangle$	0.0085 m
Relative horizontal beta function, $\beta_r = \beta^*/\beta_m^*$	$0.113/0.07 = 1.6$
Relative horizontal dispersion, $D_r = D^*/D_m^*$	$0.00333/0.00143 = 2.33$

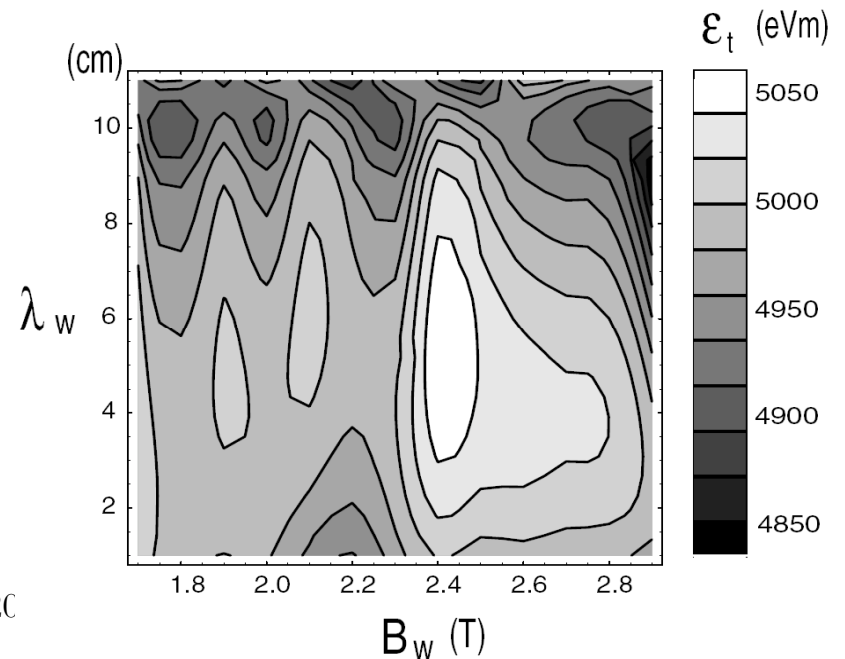


# Wigglers' effect with IBS



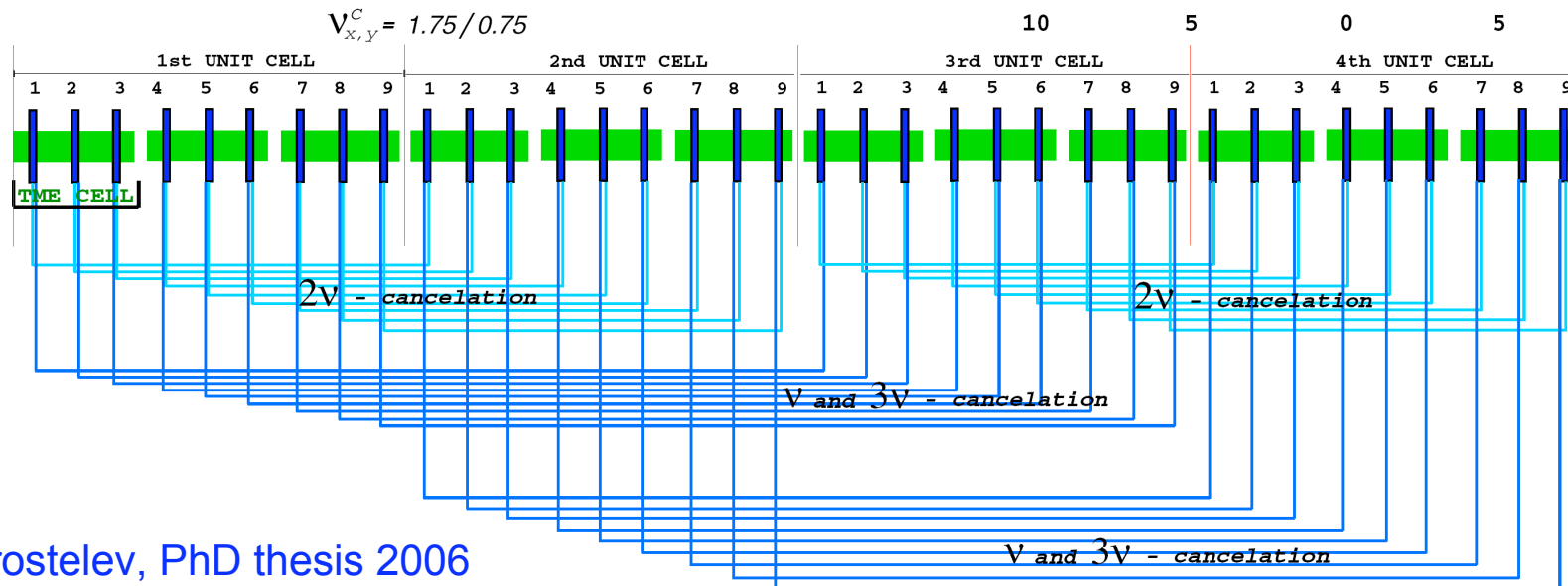
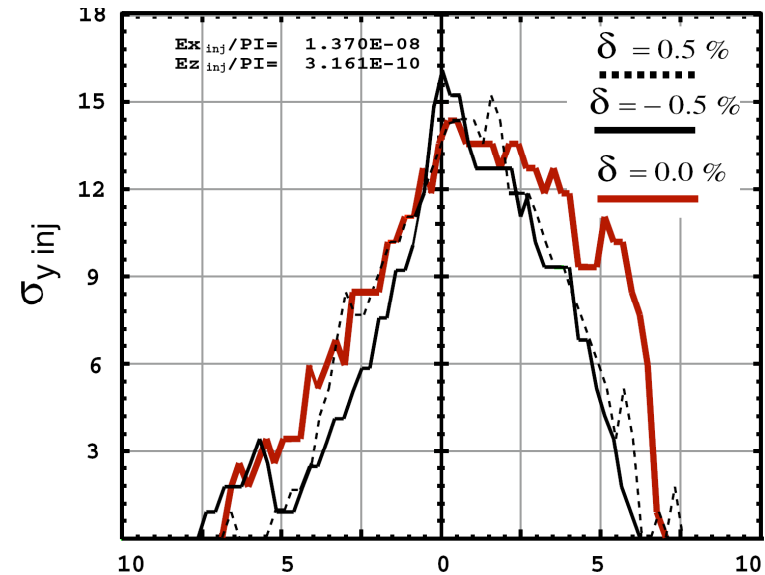
- For higher wiggler field and smaller period the transverse emittance computed with IBS gets smaller
- The longitudinal emittance has a different optimum but it can be controlled with the RF voltage

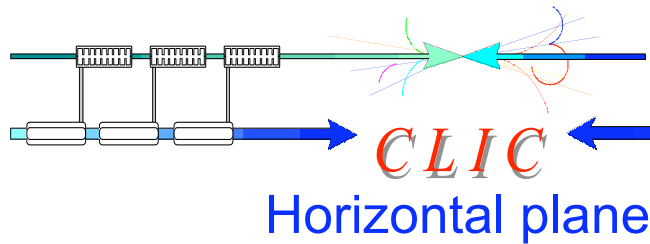
- The choice of the wiggler parameters is finally dictated by their technological feasibility.
  - Normal conducting wiggler of 1.7T can be extrapolated by existing designs
  - Super-conducting options have to be designed, built and tested





- Two sextupole schemes
  - 2 and 9 families of sextupoles
  - For 2nd scheme sextupoles are separated by a  $-I$  transformer (2nd order achromat)
- Dynamic aperture is  $9\sigma_x$  in the horizontal and  $14\sigma_y$  in the vertical plane (comfortable for injection)

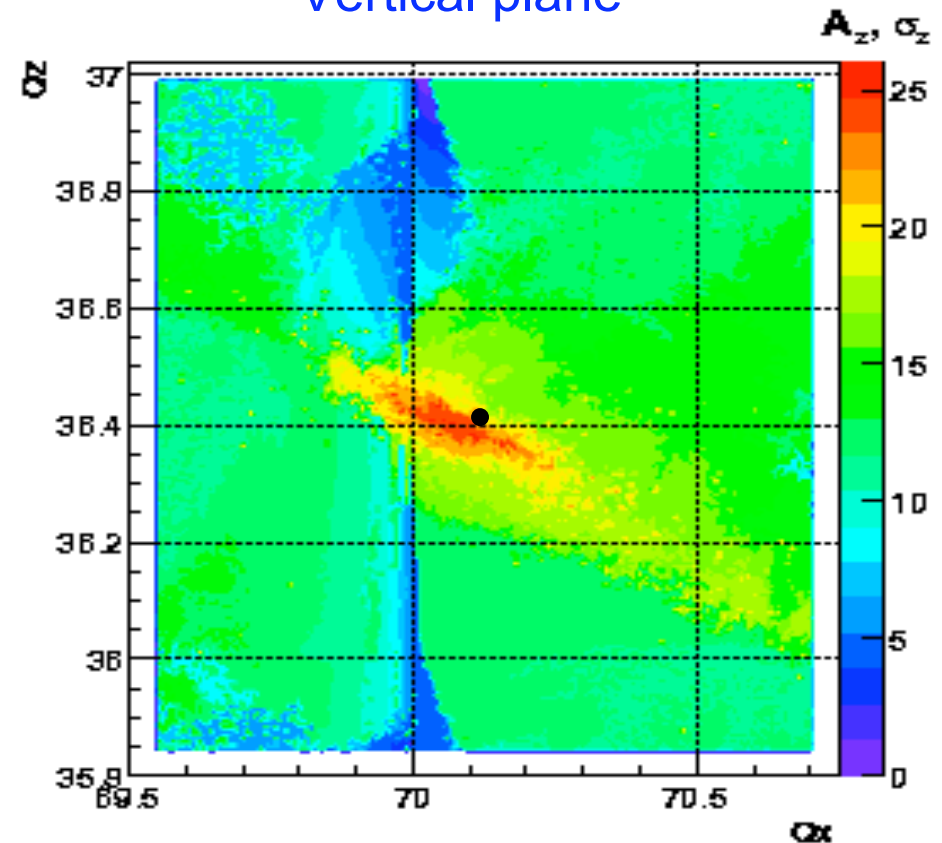
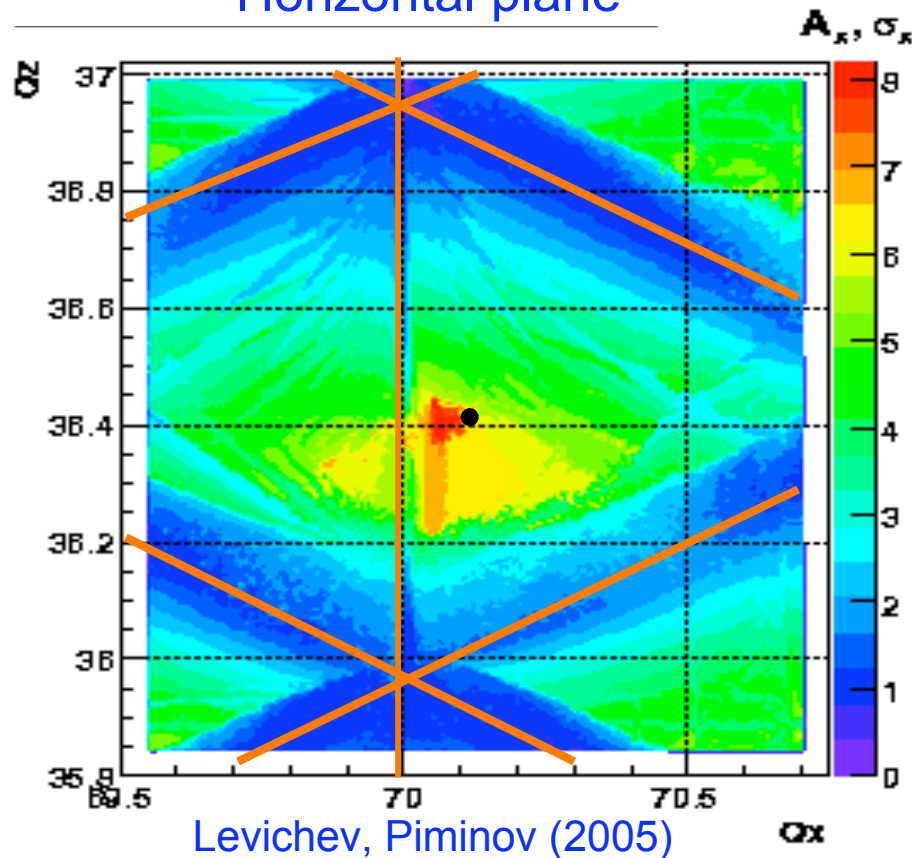




# CLIC DR betatron tunes scan



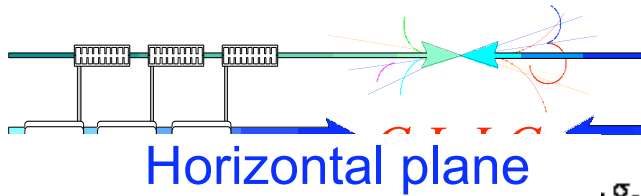
Vertical plane



- Optimising the CLIC DR tune by scanning the tune space for maximum horizontal and vertical dynamic aperture
- DA limited by  $(1, \pm 2)$  and integer resonance line

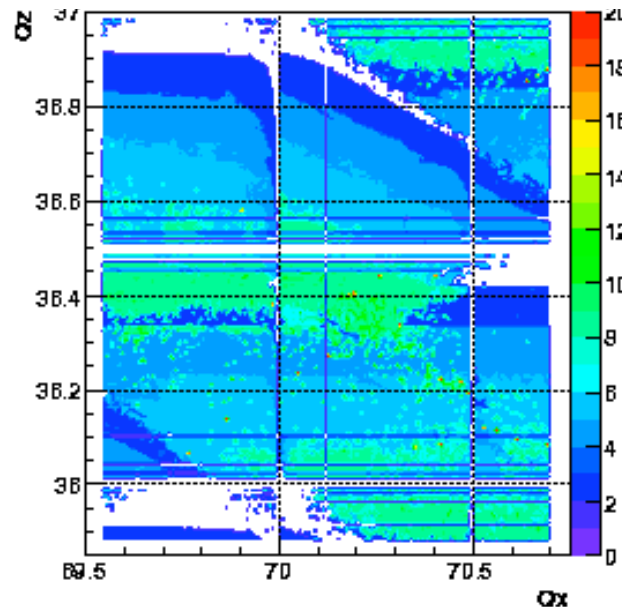
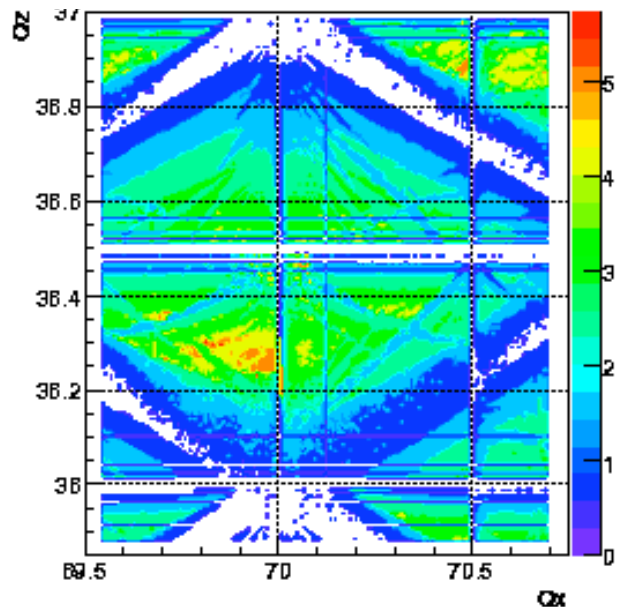
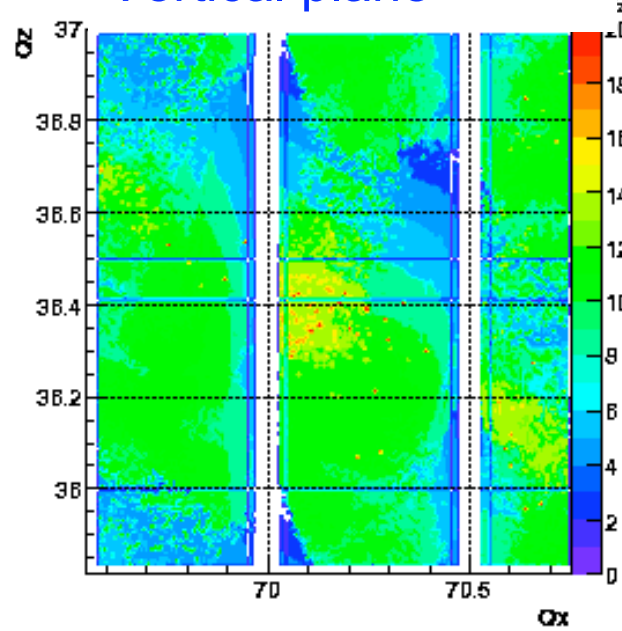
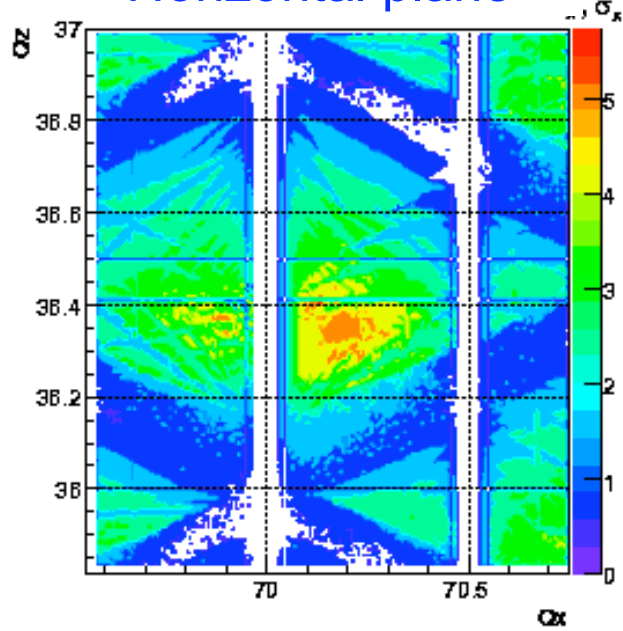
# Effect of broken periodicity

Levichev, Piminov (2005)

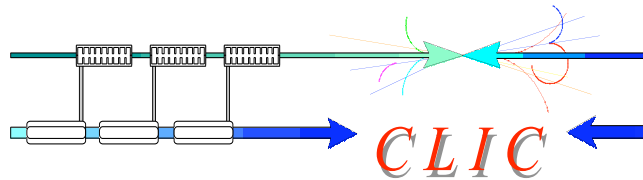


Horizontal plane

Vertical plane

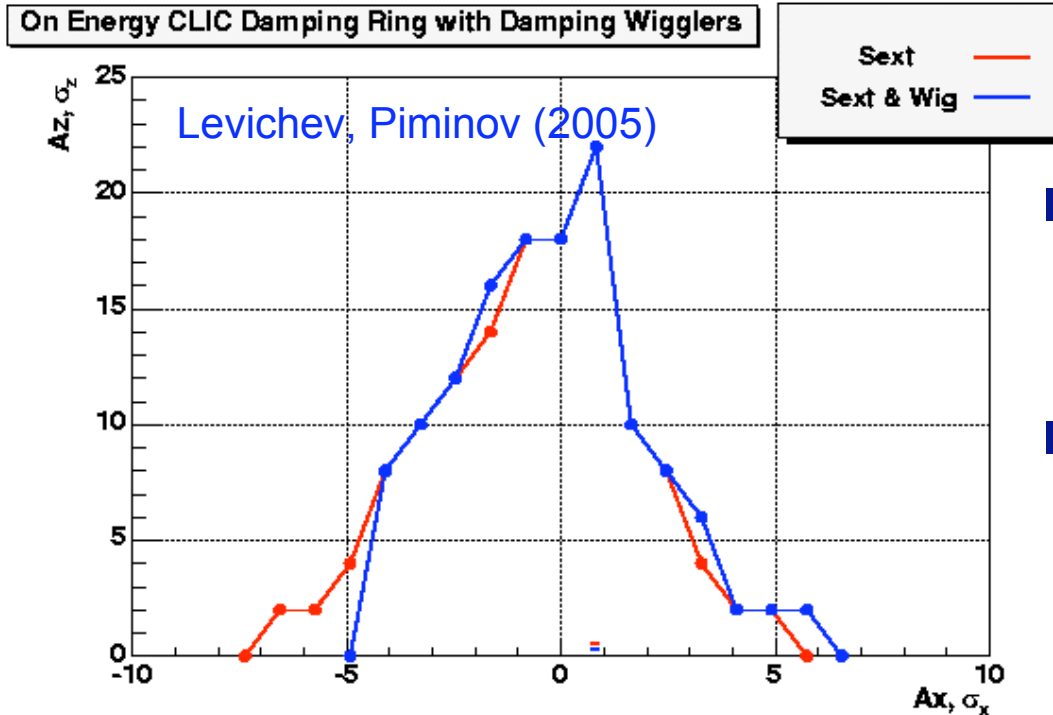
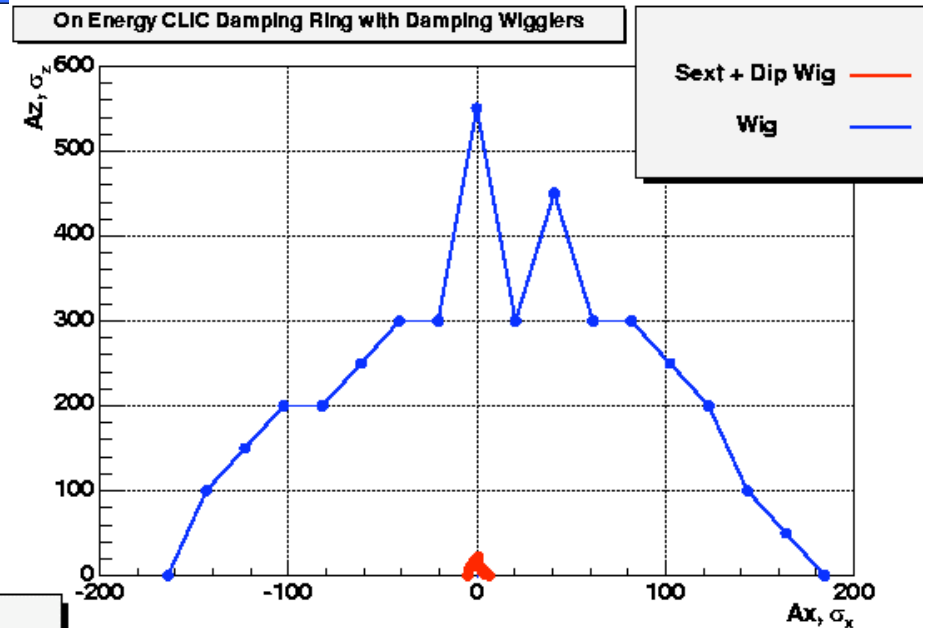


- With horizontal or vertical beta beating of 5%, appearance of large amount of non-systematic resonances, shrinking the DA and the optimal tune areas



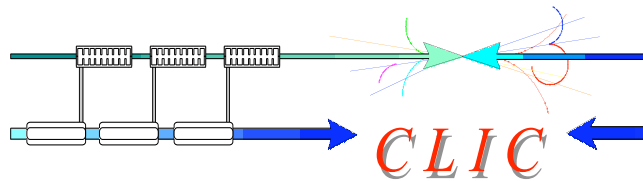
# DA for Damping wigglers

- Particles through 3D wiggler field tracked with symplectic integrator (Verlet scheme)
- Linear optics distortion corrected with quadrupole magnets in the dispersion suppressor



- Longitudinal field variation contributes to an octupole-like tune-spread
- Effect of wiggler in DA quite small

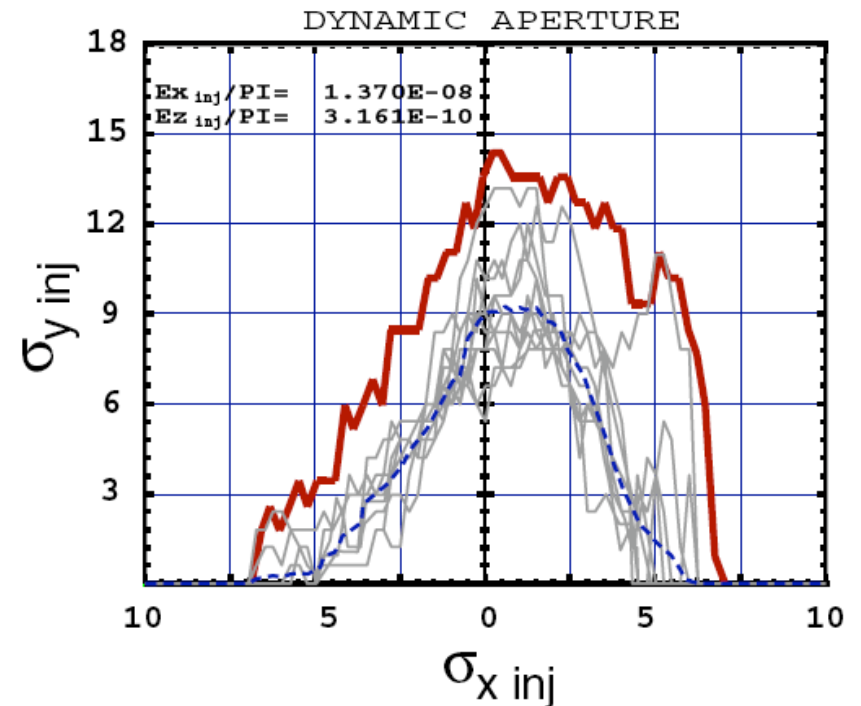




# Effect of COD and coupling

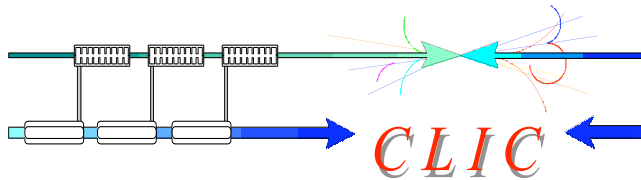
- Several alignment errors considered introducing closed orbit distortion and dispersion variation
- Correction with dispersion free steering (orbit and dispersion correction)
- Skew quadrupole correctors for correcting dispersion in the arc and emittance minimisation
- Even after correction, reduction of the DA, especially in the vertical plane

Korostelev, Zimmermann (2006)



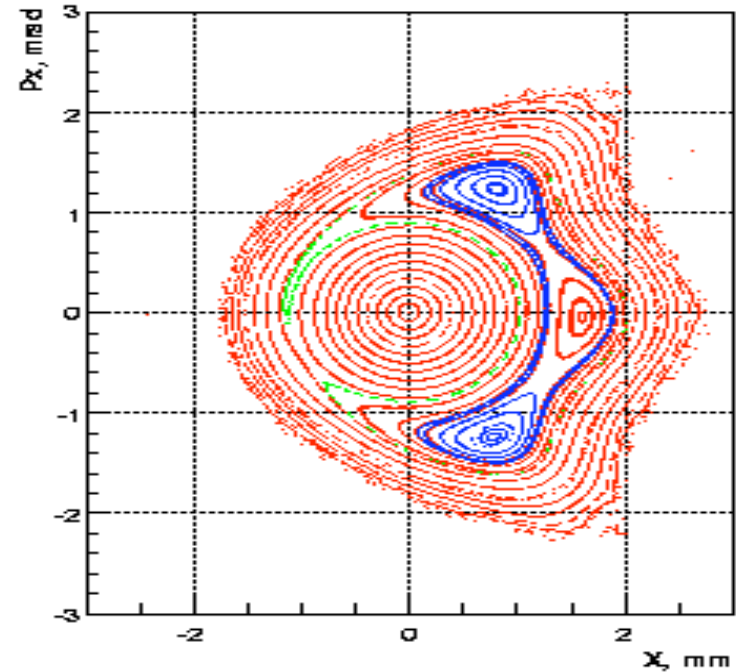
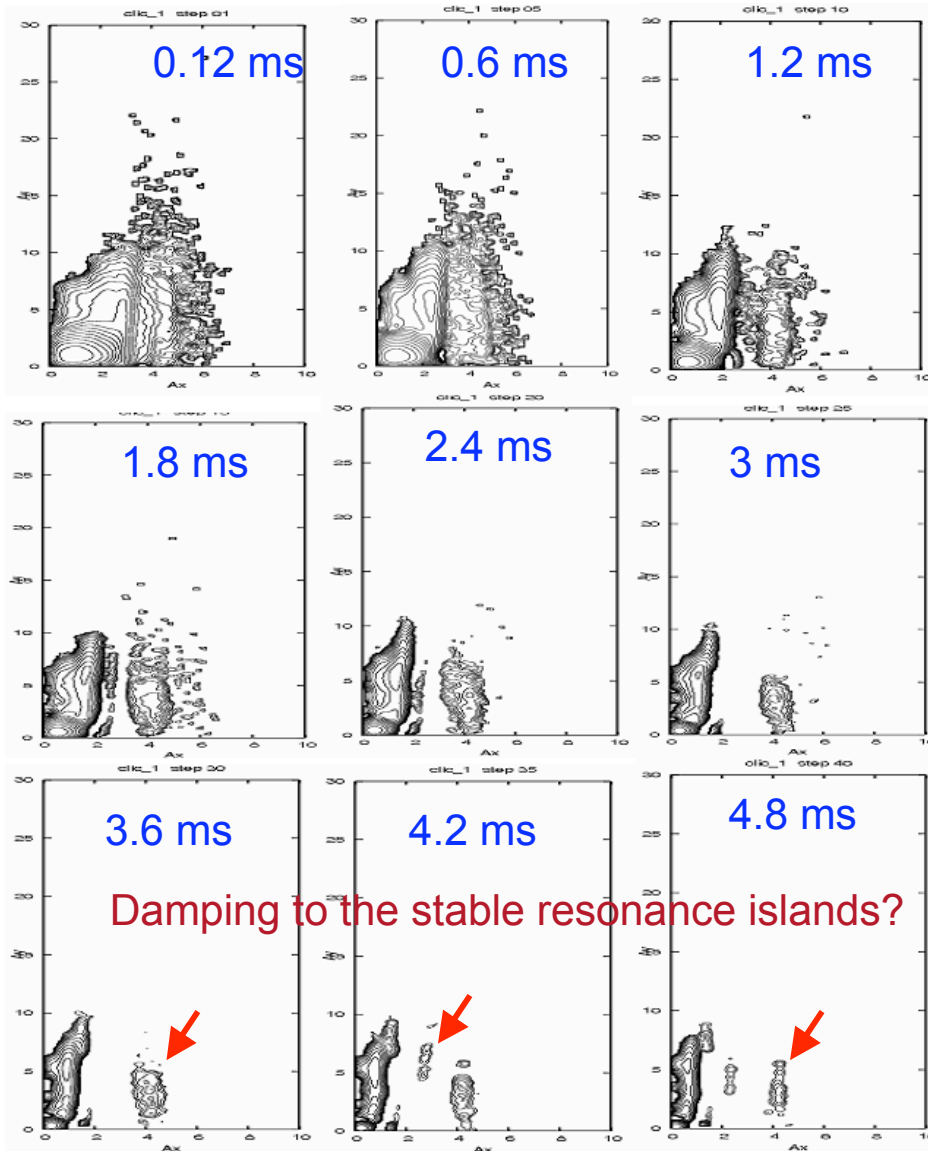
Imperfections	Simbol	1 r.m.s.
Quadrupole misalignment	$\langle \Delta Y_{\text{quad}} \rangle, \langle \Delta X_{\text{quad}} \rangle$	90 $\mu\text{m}$ .
Sextupole misalignment	$\langle \Delta Y_{\text{sext}} \rangle, \langle \Delta X_{\text{sext}} \rangle$	40 $\mu\text{m}$
Quadrupole rotation	$\langle \Delta \Theta_{\text{quad}} \rangle$	100 $\mu\text{rad}$
Dipole rotation	$\langle \Delta \Theta_{\text{dipole arc}} \rangle$	100 $\mu\text{rad}$ .
BPMs resolution	$\langle R_{\text{BPM}} \rangle$	2 $\mu\text{m}$ .

# Effect of radiation damping

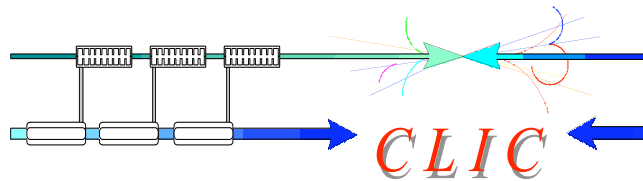


$Q_x=70.1277$   $Q_z=35.4152$

Levichev (2007)



- Including radiation damping and excitation shows that 0.7% of the particles are lost during the damping
- Certain particles seem to damp away from the beam core, on resonance islands



# Perspectives

- Optimise the TME cell for realistic magnet parameters
- Reiterate sextupole optimisation and non-linear dynamics including magnet and wiggler field errors
- Include space effect: in fact the space charge tune-shift at injection is negligible but when the beam shrinks it becomes quite large

$$\Delta\nu_y = \frac{N_{bp} r_0}{(2\pi)^{3/2} \gamma^3 \sigma_s} \oint \frac{\beta_y}{\sigma_y (\sigma_x + \sigma_y)} ds \approx 0.15$$

and should be taken into account at least in the tune optimisation

- Include effect of radiation damping, excitation and IBS in the non-linear optimisation process
- Use symplectic integrators + resonance analysis (frequency and diffusion maps)